

**REGIONE
PUGLIA**



CUP: E75G19000040005

**PIANO DEGLI INTERVENTI AIP 2020-2023 DI CUI ALLA DELIBERA N.6 DEL 22/02/2021
CON COPERTURA FINANZIARIA " FONDI DERIVANTI DA PROVENTI TARIFFARI"**

**PROGETTO DEFINITIVO
POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E DEL RECAPITO FINALE
A SERVIZIO DELL'AGGLOMERATO DEL COMUNE DI SQUINZANO (LE)**

**Acquedotto Pugliese S.p.A.
Direzione Ingegneria**

**Il Responsabile del Procedimento
Ing. Matteo MORELLO**

**Il Direttore
Ing. Gaetano BARBONE**



Ingegneria Ambientale s.r.l.
www.ingegneriambientale.com
info@ingegneriambientale.com

Ing. Franco NACCI

Ing. Stefano SANSONE



Geotek plus s.r.l.
www.geotek-rilievi.com
info@geotek-rilievi.com

PROGETTAZIONE

**Il Progettista
Prof. Ing. Matteo Ranieri**

**Il Coordinatore della Sicurezza in
fase di progettazione
Prof. Ing. Matteo Ranieri**



UNING s.r.l.
info@uning.it



Ingegneria s.r.l.
ingegneria@uning.it

Elaborato

R.37.2

**TABULATI DI CALCOLO STRUTTURALE
– EDIFICIO ALLOGGIO SOFFIANTI –**

Codice Intervento P1370

**Codice SAP
210000023391**

**Prot. N. 27346
Data 23/04/2021**

Scala:

00	MAG.2021	Emesso per Progetto DEFINITIVO			
N. Rev.	Data	Descrizione	Disegnato	Controllato	Approvato



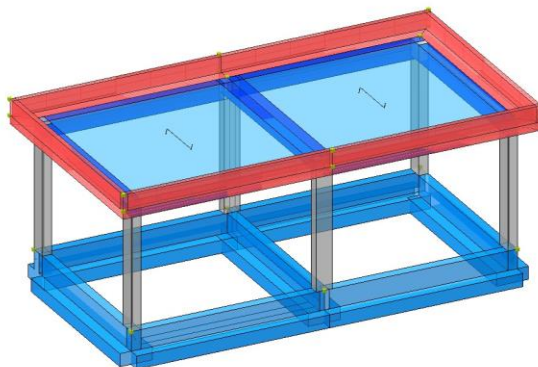


Immagine del modello di calcolo

Vita nominale, classi d'uso e periodo di riferimento

La costruzione in oggetto è definita dalla seguente tipologia (p.to 2.4 delle NT):

Vita della struttura	
Tipo	Opere ordinarie (50-100)
Vita nominale VN [anni]	50.0
Classe d'uso	III
Coefficiente d'uso CU	1.500
Periodo di riferimento VR [anni]	75.000
Probabilità di superamento PVR allo Stato limite di esercizio - SLD	63.0%
Probabilità di superamento PVR allo Stato limite ultimo - SLV	10.0%
Periodo di ritorno TR SLD [anni]	75.4
Periodo di ritorno TR SLV [anni]	711.8

Materiali impiegati e resistenze di calcolo

Materiali		
C35/45		
Peso specifico	daN/m ³	2500.00
Modulo di Young E	MPa	3.41E04
Modulo di Poisson ν		0.13
Coefficiente di dilatazione termica λ	1/°C	1e-05

Caratteristiche dei materiali delle parti in calcestruzzo armato		
Classe calcestruzzo		Cl. C35/45
Resistenza cubica R_{ck}	MPa	45.00
Resistenza di calcolo f_{cd}	MPa	21.16
Resistenza a trazione di calcolo f_{ctd}	MPa	1.56
Resistenza cilindrica f_{ck}	MPa	37.35
Resistenza a trazione media f_{ctm}	MPa	3.35
Classe acciaio barre longitudinali		Acciaio barre B450C
Resistenza allo snervamento f_{yk}	MPa	≥ 450.00
Resistenza alla rottura barre f_{tk}	MPa	≥ 540.00
Classe acciaio staffe		Acciaio barre B450C
Resistenza allo snervamento f_{yk}	MPa	≥ 450.00
Resistenza alla rottura barre f_{tk}	MPa	≥ 540.00

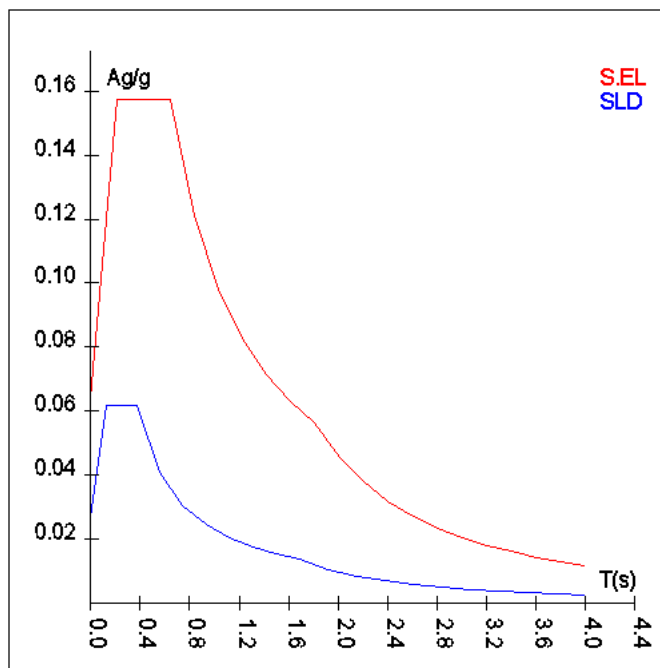
Spettri di risposta

Spettro: **SpettroNT_ 2018 (q=1)**

Il calcolo degli spettri e del fattore di comportamento sono stati calcolati per la seguente tipologia di terreno e struttura.

Vita della struttura	
Tipo	Opere ordinarie (50-100)
Vita nominale VN [anni]	50.0
Classe d'uso	III
Coefficiente d'uso CU	1.500
Periodo di riferimento VR [anni]	75.000
Probabilità di superamento PVR allo Stato limite di esercizio - SLD	63.0%
Probabilità di superamento PVR allo Stato limite ultimo - SLV	10.0%
Periodo di ritorno TR SLD [anni]	75.4
Periodo di ritorno TR SLV [anni]	711.8
Parametri del sito	
Comune	Squinzano (LE)
Longitudine	18.0569
Latitudine	40.4431
Id reticolo del sito	34591-34590-34368-34367
Valori di riferimento del sito	
Accelerazione orizzontale massima del sito Ag/g - SLD (TR=75.4)	0.0223
Fattore di amplificazione dello spettro Fo - SLD (TR=75.4)	2.3026
Periodo di riferimento di inizio del tratto a velocità costante T°C [s] - SLD (TR=75.4)	0.255
Accelerazione orizzontale massima del sito Ag/g - SLV (TR=711.8)	0.0530
Fattore di amplificazione dello spettro Fo - SLV (TR=711.8)	2.4727
Periodo di riferimento di inizio del tratto a velocità costante T°C [s] - SLV (TR=711.8)	0.514
Coefficiente Amplificazione Topografica St	1.000
Categoria terreno	B
Stato limite SLV	
Coefficiente di amplificazione stratigrafica Ss	1.20
Periodo di inizio del tratto ad accelerazione costante dello spettro TB [s]	0.22
Periodo di inizio del tratto a velocità costante dello spettro TC [s]	0.65
Periodo di inizio del tratto a spostamento costante dello spettro TD [s]	1.81
Stato limite SLD	
Coefficiente di amplificazione stratigrafica Ss	1.20
Periodo di inizio del tratto ad accelerazione costante dello spettro TB [s]	0.12
Periodo di inizio del tratto a velocità costante dello spettro TC [s]	0.37
Periodo di inizio del tratto a spostamento costante dello spettro TD [s]	1.69
Spettro Elastico	
Smorzamento viscoso %	5.0

T El. [s]	Sd El.[a/g]	T SLD [s]	Sd SLD[a/g]
0.00000	0.06360	0.00000	0.02671
0.21544	0.15728	0.12297	0.06150
0.64632	0.15728	0.36892	0.06150
0.84060	0.12093	0.55751	0.04070
1.03489	0.09822	0.74609	0.03041
1.22917	0.08270	0.93468	0.02428
1.42345	0.07141	1.12327	0.02020
1.61773	0.06284	1.31186	0.01730
1.81201	0.05610	1.50045	0.01512
2.01092	0.04555	1.68904	0.01343
2.20983	0.03772	1.92013	0.01039
2.40874	0.03175	2.15123	0.00828
2.60765	0.02709	2.38232	0.00675
2.80655	0.02338	2.61342	0.00561
3.00546	0.02039	2.84452	0.00474
3.20437	0.01794	3.07561	0.00405
3.40328	0.01590	3.30671	0.00350
3.60218	0.01420	3.53781	0.00306
3.80109	0.01275	3.76890	0.00270
4.00000	0.01151	4.00000	0.00240



Percentuali Spostamento masse impalcati

Posizione	% Spostamento direzione X	% Spostamento direzione Y
1	0	-5
2	5	0
3	0	5
4	-5	0

Combinazioni del Sisma in X e Y e Verticale

Comb.	Pos. SismaX	Pos. SismaY	Fx	Fy	Fz
1	1	2	1	0.3	0.3
2	1	2	0.3	1	0.3
3	1	2	0.3	0.3	1
4	1	4	1	0.3	0.3
5	1	4	0.3	1	0.3
6	1	4	0.3	0.3	1
7	3	2	1	0.3	0.3
8	3	2	0.3	1	0.3
9	3	2	0.3	0.3	1
10	3	4	1	0.3	0.3
11	3	4	0.3	1	0.3
12	3	4	0.3	0.3	1

Comb. Numero di combinazione dei sismi
 Pos. SismaX Posizione in cui viene scelto il sisma in direzione X
 Pos. SismaY Posizione in cui viene scelto il sisma in direzione Y
 Fx Fattore con cui il sisma X partecipa
 Fy Fattore con cui il sisma Y partecipa
 Fz Fattore con cui il sisma Verticale partecipa (quando richiesto)

Ogni combinazione genera al massimo 8 sotto-combinazioni in base a tutte le combinazioni possibili dei segni di Fx ed Fy ed Fz.

Azioni sulla struttura

Descrizione	Tipo
Peso Proprio	Automatica
QP Solai	Automatica
QFissi Solai	Automatica
QV Solai	Automatica
QV SolaiPsi0	Automatica
QV SolaiPsi1	Automatica

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021
Pagina 4 di 103

Descrizione	Tipo
QV SolaiPsi2	Automatica
Neve	Utente
Muri esterni	Utente
permanenti	Utente
ACCIDENTALI COPERTURA	Utente

Scenario di calcolo

Scenario : ScenarioNT_2018 A2_SLV_SLD_STR_GEO
Combinazione n° 1: Solo Permanenti
 Tipo: STR+GEO
 Spettro: n.a.
 Fattore sisma: n.a.
 Angolo ingresso sisma [°]: n.a.
 Kmod: 0.60

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1.3	Si	n.a.	n.a.
QP Solai	1.3	Si	n.a.	n.a.
QFissi Solai	1.5	Si	n.a.	n.a.
QV Solai	1	No	n.a.	n.a.
QV SolaiPsi0	1	No	n.a.	n.a.
QV SolaiPsi1	1	No	n.a.	n.a.
QV SolaiPsi2	1	No	n.a.	n.a.
Neve	1.5	No	n.a.	n.a.
Muri esterni	1.5	Si	n.a.	n.a.
permanenti	1.5	Si	n.a.	n.a.
ACCIDENTALI COPERTURA	1	No	n.a.	n.a.

Combinazione n° 2: AD QVSolai
 Tipo: STR+GEO
 Spettro: n.a.
 Fattore sisma: n.a.
 Angolo ingresso sisma [°]: n.a.
 Kmod: 0.90

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1.3	Si	n.a.	n.a.
QP Solai	1.3	Si	n.a.	n.a.
QFissi Solai	1.5	Si	n.a.	n.a.
QV Solai	1.5	Si	n.a.	n.a.
QV SolaiPsi0	1	No	n.a.	n.a.
QV SolaiPsi1	1	No	n.a.	n.a.
QV SolaiPsi2	1	No	n.a.	n.a.
Neve	0.75	Si	n.a.	n.a.
Muri esterni	1.5	Si	n.a.	n.a.
permanenti	1.5	Si	n.a.	n.a.
ACCIDENTALI COPERTURA	1.5	Si	n.a.	n.a.

Combinazione n° 3: Neve
 Tipo: STR+GEO
 Spettro: n.a.
 Fattore sisma: n.a.
 Angolo ingresso sisma [°]: n.a.
 Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1.3	Si	n.a.	n.a.
QP Solai	1.3	Si	n.a.	n.a.
QFissi Solai	1.5	Si	n.a.	n.a.
QV Solai	1.5	No	n.a.	n.a.
QV SolaiPsi0	1	No	n.a.	n.a.
QV SolaiPsi1	1	Si	n.a.	n.a.
QV SolaiPsi2	1	No	n.a.	n.a.
Neve	1.5	Si	n.a.	n.a.
Muri esterni	1.5	Si	n.a.	n.a.
permanenti	1.5	Si	n.a.	n.a.
ACCIDENTALI COPERTURA	1.5	Si	n.a.	n.a.

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021
Pagina 5 di 103

Combinazione n° 4: **SISMAX1_SLV**
Tipo: Modale STR+GEO
Spettro: SpettroNT_2018
Fattore sisma: 1.00
Angolo ingresso sisma [°]: 0
Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	Si	1
QP Solai	1	Si	Si	1
QFissi Solai	1	Si	Si	1
QV Solai	1	No	No	1
QV SolaiPsi0	1	No	No	1
QV SolaiPsi1	1	No	No	1
QV SolaiPsi2	1	Si	Si	1
Neve	1	No	No	1
Muri esterni	1	Si	Si	1
permanenti	1	Si	Si	1
ACCIDENTALI COPERTURA	1	No	Si	1

Combinazione n° 5: **SISMAY1_SLV**
Tipo: Modale STR+GEO
Spettro: SpettroNT_2018
Fattore sisma: 1.00
Angolo ingresso sisma [°]: 90
Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	Si	1
QP Solai	1	Si	Si	1
QFissi Solai	1	Si	Si	1
QV Solai	1	No	No	1
QV SolaiPsi0	1	No	No	1
QV SolaiPsi1	1	No	No	1
QV SolaiPsi2	1	Si	Si	1
Neve	1	Si	No	1
Muri esterni	1	Si	Si	1
permanenti	1	Si	Si	1
ACCIDENTALI COPERTURA	1	No	Si	1

Combinazione n° 6: **AD QVSolai**
Tipo: SLE Rara
Spettro: n.a.
Fattore sisma: n.a.
Angolo ingresso sisma [°]: n.a.
Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	n.a.	n.a.
QP Solai	1	Si	n.a.	n.a.
QFissi Solai	1	Si	n.a.	n.a.
QV Solai	1	Si	n.a.	n.a.
QV SolaiPsi0	1	No	n.a.	n.a.
QV SolaiPsi1	1	No	n.a.	n.a.
QV SolaiPsi2	1	No	n.a.	n.a.
Neve	0.5	Si	n.a.	n.a.
Muri esterni	1	Si	n.a.	n.a.
permanenti	1	No	n.a.	n.a.
ACCIDENTALI COPERTURA	1	Si	n.a.	n.a.

Combinazione n° 7: **AD QVSolai**
Tipo: SLE Freq.
Spettro: n.a.
Fattore sisma: n.a.
Angolo ingresso sisma [°]: n.a.
Kmod: 1.00

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021
Pagina 6 di 103

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	n.a.	n.a.
QP Solai	1	Si	n.a.	n.a.
QFissi Solai	1	Si	n.a.	n.a.
QV Solai	1	No	n.a.	n.a.
QV SolaiPsi0	1	No	n.a.	n.a.
QV SolaiPsi1	1	Si	n.a.	n.a.
QV SolaiPsi2	1	No	n.a.	n.a.
Neve	0.2	Si	n.a.	n.a.
Muri esterni	1	Si	n.a.	n.a.
permanenti	1	Si	n.a.	n.a.
ACCIDENTALI COPERTURA	0.5	No	n.a.	n.a.

Combinazione n° 8: Quasi P1
 Tipo: SLE Q.Perm.
 Spettro: n.a.
 Fattore sisma: n.a.
 Angolo ingresso sisma [°]: n.a.
 Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	n.a.	n.a.
QP Solai	1	Si	n.a.	n.a.
QFissi Solai	1	Si	n.a.	n.a.
QV Solai	1	No	n.a.	n.a.
QV SolaiPsi0	1	No	n.a.	n.a.
QV SolaiPsi1	1	No	n.a.	n.a.
QV SolaiPsi2	1	Si	n.a.	n.a.
Neve	1	No	n.a.	n.a.
Muri esterni	1	Si	n.a.	n.a.
permanenti	1	Si	n.a.	n.a.
ACCIDENTALI COPERTURA	0.5	No	n.a.	n.a.

Combinazione n° 9: SISMAX_SLD
 Tipo: Modale SLE
 Spettro: SpettroNT_ 2018
 Fattore sisma: 1.00
 Angolo ingresso sisma [°]: 0
 Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	Si	1
QP Solai	1	Si	Si	1
QFissi Solai	1	Si	Si	1
QV Solai	1	No	No	1
QV SolaiPsi0	1	No	No	1
QV SolaiPsi1	1	No	No	1
QV SolaiPsi2	1	Si	Si	1
Neve	1	No	No	1
Muri esterni	1	Si	Si	1
permanenti	1	Si	Si	1
ACCIDENTALI COPERTURA	0.5	No	Si	1

Combinazione n° 10: SISMAX_SLD
 Tipo: Modale SLE
 Spettro: SpettroNT_ 2018
 Fattore sisma: 1.00
 Angolo ingresso sisma [°]: 90
 Kmod: 1.00

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
Peso Proprio	1	Si	Si	1
QP Solai	1	Si	Si	1
QFissi Solai	1	Si	Si	1
QV Solai	1	No	No	1
QV SolaiPsi0	1	No	No	1
QV SolaiPsi1	1	No	No	1
QV SolaiPsi2	1	Si	Si	1
Neve	1	No	No	1
Muri esterni	1	Si	Si	1
permanenti	1	Si	Si	1

Condizione di carico	Fattore di combinazione	Attiva	Massa	Fattore massa
ACCIDENTALI COPERTURA	0.5	No	Si	1

Criteri di verifica

CLS_Pilastri_ND		
Generici		
Resistenza caratteristica R_{ck}	MPa	45.00
Tensione caratteristica snervamento acciaio barre f_{yk}	MPa	450.00
Tensione caratteristica snervamento acciaio staffe f_{yk}	MPa	450.00
Deformazione unitaria ϵ_{c0}		0.002
Deformazione ultima ϵ_{cu}		0.0035
ϵ_{fu} (solo incrudimento)		0.002
Modulo elastico E acciaio	MPa	2.10E05
Copriferro di calcolo	mm	56.00
Copriferro di disegno	mm	50.00
Coefficiente di sicurezza γ_{Cl}		1.5
Coefficiente di sicurezza γ_{Acc}		1.15
Riduzione f_{cd} calcestruzzo		0.85
Usa staffe minime di normativa in assenza di sisma		Si
Usa staffe minime di normativa in presenza di sisma		No
Generici N.T.		
Inclinazione bielle compresse $\cotg(\theta)$		1.00
Modello acciaio		Incrudente
Incrudimento E_y/E_0		0.000
Elemento esistente		No
Sforzo normale ammissibile v_{max} (CDA)		0.550
Sforzo normale ammissibile v_{max} (CDB)		0.650
Generici D.M. 96 T.A.		
Tensione ammissibile σ_c	MPa	13.50
Tensione ammissibile σ_c in trazione	MPa	4.02
Tensione ammissibile σ_c acciaio	MPa	260.00
Tensione tangenziale ammissibile τ_{c0}	MPa	0.80
Tensione tangenziale massima τ_{c1}	MPa	2.26
Coefficiente di omogeneizzazione n		15
Coefficiente di omogeneizzazione n in trazione		0.5
Sezione interamente reagente		No
Fessurazioni		
Verifica a decompressione		No
Verifica formazione fessure		No
Verifica aperture fessure		Si
Classe di esposizione		XC4
Tipo armatura		Poco sensibile
Combinazione Rara		No
Combinazione QP		Si
W ammissibile Combinazione QP	mm	0.200
Combinazione Freq.		Si
W ammissibile Combinazione Freq.	mm	0.300
Valore caratteristico apertura fessure $w_k(*w_m)$		1
Resistenza media a trazione f_{ctm}	MPa	33.52
Coefficiente di breve o lunga durata k_t		0.40
Coefficiente di aderenza k_1		0.80
Tensioni ammissibili di esercizio		
Verifica Combinazione Rara		Si
Tensione ammissibile σ_{Cl}	MPa	22.41
Tensione ammissibile $\sigma_{Acciaio}$	MPa	360.00
Verifica Combinazione QP		Si
Tensione ammissibile σ_{Cl}	MPa	16.81
Tensione ammissibile $\sigma_{Acciaio}$	MPa	360.00
Verifica Combinazione Freq.		No
Coefficienti di omogeneizzazione		
Acciaio - Cl s compresso		15
Cl s tesoro - Cl s compresso		0.5
Armatura pilastri		
Massimo numero di ferri in ogni spigolo		1
Diametro ferri di spigolo	mm	16
Diametro ferri laterali	mm	16
Diametro staffe	mm	8
Numero braccia staffe lato lungo		4

Minima percentuale armatura rispetto al Cls	%	1.00
Massima percentuale armatura rispetto al Cls	%	4.00
Verifica pilastri		
Verifica a carico di punta		No
Verifica a pressoflessione deviata		No
Verifica come pareti		No
Verifica Duttibilità N.T. 2018		
Verifica di duttilità		NO
Fattore confinamento minimo		1.000
Calcolo Fattore confinamento		SI
Verifica N.T. pilastri		
Verifica pilastri tozzi		NO
Gerarchia Flessione-Taglio		NO
Verifica a taglio pilastri		
Effetto spinotto		SI
Traslazione momento		SI
Considera la resistenza a taglio VRDns		NO
Verifica a taglio pilastri DM 3274/DM96		
Coefficiente di amplificazione γ_{Rd}		1.2
Sforzo normale ammissibile v_{max}		0.8
Effetto della pressoflessione		SI
Verifica a taglio N.T. pilastri		
γ_{Rd} (CDA) Pressoflessione		1.3
γ_{Rd} (CDB) Pressoflessione		1.3
γ_{Rd} (CDA) Taglio		1.3
γ_{Rd} (CDB) Taglio		1.1
Verifica Nodi secondo EC8		SI
Stampa pilastri		
Informazioni sollecitazioni di verifica		No
Verifica per tutte le combinazioni di carico		SI
Fattori di amplificazione		No
Gerarchia delle resistenze pilastri		
Direzione Y		No
Direzione Z		No

CLS_TraviAlte_ND		
Generici		
Resistenza caratteristica R_{ck}	MPa	45.00
Tensione caratteristica snervamento acciaio barre f_{yk}	MPa	450.00
Tensione caratteristica snervamento acciaio staffe f_{yk}	MPa	450.00
Deformazione unitaria ϵ_{c0}		0.002
Deformazione ultima ϵ_{cu}		0.0035
ϵ_{fu} (solo incrudimento)		0.002
Modulo elastico E acciaio	MPa	2.10E05
Copriferro di calcolo	mm	56.00
Copriferro di disegno	mm	50.00
Coefficiente di sicurezza γ_{Cl}		1.5
Coefficiente di sicurezza γ_{Acc}		1.15
Riduzione f_{cd} calcestruzzo		0.85
Usa staffe minime di normativa in assenza di sisma		SI
Usa staffe minime di normativa in presenza di sisma		No
Generici N.T.		
Inclinazione bielle compresse $\cotg(\theta)$		1.00
Modello acciaio		Incrudente
Incrudimento E_y/E_0		0.000
Elemento esistente		No
Generici D.M. 96 T.A.		
Tensione ammissibile σ_c	MPa	13.50
Tensione ammissibile σ_c in trazione	MPa	4.02
Tensione ammissibile σ_c acciaio	MPa	260.00
Tensione tangenziale ammissibile τ_{c0}	MPa	0.80
Tensione tangenziale massima τ_{c1}	MPa	2.26
Coefficiente di omogeneizzazione n		15
Coefficiente di omogeneizzazione n in trazione		0.5
Sezione interamente reagente		No
Fessurazioni		
Verifica a decompressione		No
Verifica formazione fessure		No
Verifica aperture fessure		SI
Classe di esposizione		XC4
Tipo armatura		Poco sensibile

Combinazione Rara		No
Combinazione QP		Si
W ammissibile Combinazione QP	mm	0.200
Combinazione Freq.		Si
W ammissibile Combinazione Freq.	mm	0.300
Valore caratteristico apertura fessure wk(*wm)		1
Resistenza media a trazione fctm	MPa	33.52
Coefficiente di breve o lunga durata kt		0.40
Coefficiente di aderenza k1		0.80
Tensioni ammissibili di esercizio		
Verifica Combinazione Rara		Si
Tensione ammissibile σClS	MPa	22.41
Tensione ammissibile σAcciaio	MPa	360.00
Verifica Combinazione QP		Si
Tensione ammissibile σClS	MPa	16.81
Tensione ammissibile σAcciaio	MPa	360.00
Verifica Combinazione Freq.		No
Coefficienti di omogeneizzazione		
Acciaio - Cls compresso		15
Cls teso - Cls compresso		0.5
Armatura travi		
Numero di bracci delle staffe		2
Numero minimo di ferri superiori		2
Numero minimo di ferri inferiori		2
Numero minimo di ferri di parete		1
Numero reggistaffe superiori		0
Numero reggistaffe intermedi		0
Numero reggistaffe inferiori		0
Diametro ferri superiori	mm	16
Diametro ferri inferiori	mm	16
Diametro staffe	mm	8
Percentuale armatura rispetto alla base per verifica a taglio	%	100.00
Minima percentuale armatura compressa rispetto alla tesa	%	50.00
Minima percentuale armatura rispetto al Cls	%	0.31
Massima percentuale armatura rispetto al Cls	%	1.55
Calcolo travi		
Traslazione momento		No
Verifica travi		
Verifica a torsione		No
Verifica a pressoflessione retta		No
Trave a spessore		No
Verifica N.T. travi		
Trave tozza		No
Gerarchia Flessione-Taglio		No
Escludi dalla gerarchia trave-pilastro		No
Verifica a taglio DM 3274 travi		
Coefficiente di sovra resistenza γRd		1.2
Includi effetto della pressoflessione nel taglio		Si
Verifica a taglio N.T. travi		
Includi effetto spinotto nel taglio		Si
Considera la resistenza a taglio VRDns		NO
Coefficiente di sovra resistenza γRd (CDA)		1.2
Coefficiente di sovra resistenza γRd (CDB)		1.1
Verifica Duttività N.T. 2018		
Verifica di duttilità		NO
Fattore confinamento minimo		1.000
Calcolo Fattore confinamento		NO
Verifica a taglio D.M. 96 T.A. travi		
Percentuale taglio alle staffe	%	60
Percentuale taglio ferri parete	%	40
Stampa travi		
Stampa informazioni relative all'asse neutro		Si

CLS_Muri_ND		
Generici		
Resistenza caratteristica Rck	MPa	45.00
Tensione caratteristica snervamento acciaio barre fyk	MPa	450.00
Tensione caratteristica snervamento acciaio staffe fyk	MPa	450.00
Deformazione unitaria εc0		0.002
Deformazione ultima εcu		0.0035
εfu (solo incrudimento)		0.002

Modulo elastico E acciaio	MPa	2.10E05
Copri ferro di calcolo	mm	60.00
Copri ferro di disegno	mm	40.00
Coefficiente di sicurezza γ_{Cl}		1.5
Coefficiente di sicurezza γ_{Acc}		1.15
Riduzione fcd calcestruzzo		0.85
Usa staffe minime di normativa in assenza di sisma		Si
Usa staffe minime di normativa in presenza di sisma		No
Generici N.T.		
Inclinazione bielle compresse $\cotg(\theta)$		1.00
Modello acciaio		Incrudente
Incrudimento E_y/E_0		0.000
Elemento esistente		No
Generici D.M. 96 T.A.		
Tensione ammissibile σ_c	MPa	13.50
Tensione ammissibile σ_c in trazione	MPa	4.02
Tensione ammissibile σ_c acciaio	MPa	260.00
Tensione tangenziale ammissibile τ_{c0}	MPa	0.80
Tensione tangenziale massima τ_{c1}	MPa	2.26
Coefficiente di omogeneizzazione n		15
Coefficiente di omogeneizzazione n in trazione		0.5
Sezione interamente reagente		No
Fessurazioni		
Verifica a decompressione		No
Verifica formazione fessure		No
Verifica aperture fessure		Si
Classe di esposizione		XC4
Tipo armatura		Poco sensibile
Combinazione Rara		No
Combinazione QP		Si
W ammissibile Combinazione QP	mm	0.200
Combinazione Freq.		Si
W ammissibile Combinazione Freq.	mm	0.300
Valore caratteristico apertura fessure $w_k(*w_m)$		1
Resistenza media a trazione f_{ctm}	MPa	33.52
Coefficiente di breve o lunga durata k_t		0.40
Coefficiente di aderenza k_1		0.80
Tensioni ammissibili di esercizio		
Verifica Combinazione Rara		Si
Tensione ammissibile σ_{Cl}	MPa	22.41
Tensione ammissibile $\sigma_{Acciaio}$	MPa	360.00
Verifica Combinazione QP		Si
Tensione ammissibile σ_{Cl}	MPa	16.81
Tensione ammissibile $\sigma_{Acciaio}$	MPa	360.00
Verifica Combinazione Freq.		No
Coefficienti di omogeneizzazione		
Acciaio - Cls compresso		15
Cls teso - Cls compresso		0.5
Armatura muri		
Minima percentuale armatura rispetto al Cls in direzione X	%	0.1
Minima percentuale armatura rispetto al Cls in direzione Y	%	0.1
Massima percentuale armatura rispetto al Cls in direzione X	%	2
Massima percentuale armatura rispetto al Cls in direzione Y	%	2
Verifica muri		
Step incremento armatura	cmq	0.01
Verifica muri come pareti		No

CLS_TraviFondazione_ND		
Generici		
Resistenza caratteristica R_{ck}	MPa	45.00
Tensione caratteristica snervamento acciaio barre f_{yk}	MPa	450.00
Tensione caratteristica snervamento acciaio staffe f_{yk}	MPa	450.00
Deformazione unitaria ϵ_{c0}		0.002
Deformazione ultima ϵ_{cu}		0.0035
ϵ_{fu} (solo incrudimento)		0.002
Modulo elastico E acciaio	MPa	2.10E05
Copri ferro di calcolo	mm	56.00
Copri ferro di disegno	mm	50.00
Coefficiente di sicurezza γ_{Cl}		1.5
Coefficiente di sicurezza γ_{Acc}		1.15
Riduzione fcd calcestruzzo		0.85

Usa staffe minime di normativa in assenza di sisma		Si
Usa staffe minime di normativa in presenza di sisma		No
Generici N.T.		
Inclinazione bielle compresse $\cotg(\theta)$		1.00
Modello acciaio		Incrudente
Incrudimento E_y/E_0		0.000
Elemento esistente		No
Generici D.M. 96 T.A.		
Tensione ammissibile σ_c	MPa	13.50
Tensione ammissibile σ_c in trazione	MPa	4.02
Tensione ammissibile σ_c acciaio	MPa	260.00
Tensione tangenziale ammissibile τ_{c0}	MPa	0.80
Tensione tangenziale massima τ_{c1}	MPa	2.26
Coefficiente di omogeneizzazione n		15
Coefficiente di omogeneizzazione n in trazione		0.5
Sezione interamente reagente		No
Fessurazioni		
Verifica a decompressione		No
Verifica formazione fessure		No
Verifica aperture fessure		Si
Classe di esposizione		XA2
Tipo armatura		Poco sensibile
Combinazione Rara		No
Combinazione QP		Si
W ammissibile Combinazione QP	mm	0.200
Combinazione Freq.		Si
W ammissibile Combinazione Freq.	mm	0.300
Valore caratteristico apertura fessure $w_k(*w_m)$		1
Resistenza media a trazione f_{ctm}	MPa	33.52
Coefficiente di breve o lunga durata k_t		0.40
Coefficiente di aderenza k_1		0.80
Tensioni ammissibili di esercizio		
Verifica Combinazione Rara		Si
Tensione ammissibile σ_{Cl}	MPa	22.41
Tensione ammissibile $\sigma_{Acciaio}$	MPa	360.00
Verifica Combinazione QP		Si
Tensione ammissibile σ_{Cl}	MPa	16.81
Tensione ammissibile $\sigma_{Acciaio}$	MPa	360.00
Verifica Combinazione Freq.		No
Coefficienti di omogeneizzazione		
Acciaio - Cls compresso		15
Clis tesoro - Cls compresso		0.5
Armatura travi		
Numero di bracci delle staffe		2
Numero minimo di ferri superiori		2
Numero minimo di ferri inferiori		2
Numero minimo di ferri di parete		1
Numero reggistaffe superiori		0
Numero reggistaffe intermedi		4
Numero reggistaffe inferiori		2
Diametro ferri superiori	mm	16
Diametro ferri inferiori	mm	16
Diametro staffe	mm	8
Percentuale armatura rispetto alla base per verifica a taglio	%	100.00
Minima percentuale armatura compressa rispetto alla tesa	%	50.00
Minima percentuale armatura rispetto al Cls	%	0.20
Massima percentuale armatura rispetto al Cls	%	1.55
Calcolo travi		
Traslazione momento		Si
Verifica travi		
Verifica a torsione		No
Verifica a pressoflessione retta		No
Trave a spessore		No
Verifica N.T. travi		
Trave tozza		No
Gerarchia Flessione-Taglio		No
Escludi dalla gerarchia trave-pilastro		No
Verifica a taglio DM 3274 travi		
Coefficiente di sovra resistenza γ_{Rd}		1.2
Includi effetto della pressoflessione nel taglio		Si
Verifica a taglio N.T. travi		
Includi effetto spinotto nel taglio		Si

Considera la resistenza a taglio VRDns		NO
Coefficiente di sovra resistenza γ_{Rd} (CDA)		1.2
Coefficiente di sovra resistenza γ_{Rd} (CDB)		1.1
Verifica Duttività N.T. 2018		
Verifica di duttilità		NO
Fattore confinamento minimo		1.000
Calcolo Fattore confinamento		NO
Verifica a taglio D.M. 96 T.A. travi		
Percentuale taglio alle staffe	%	60
Percentuale taglio ferri parete	%	40
Stampa travi		
Stampa informazioni relative all'asse neutro		Si

Risultati Analisi Dinamica - Statistiche matrice di rigidezza

Scenario di calcolo: **ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO**

Minimo della diagonale	1.629375e+07
Massimo della diagonale	7.966715e+12
Rapporto Max/Min	4.889429e+05
Media della diagonale	1.985562e+11
Densità	2.141118e+00

Dati generali

Nome struttura	
Fattore rigidezza assiale pilastri	10
Numero di frequenze	15
% Filtro masse libere	0.1
% Coefficiente di smorzamento viscoso	5
Spostamenti modali con segno	Si
Deformabilità a taglio delle aste	Si
Spostamento ammissibile impalcati	0.0050*h

Impalcati

N°	Quota m	Rigido m	Incr.Soll.Pil	Inc.Soll.Par.
0	0.000	No	1.000	1.000
1	3.500	Si	1.000	1.000
2	4.000	Si	1.000	1.000

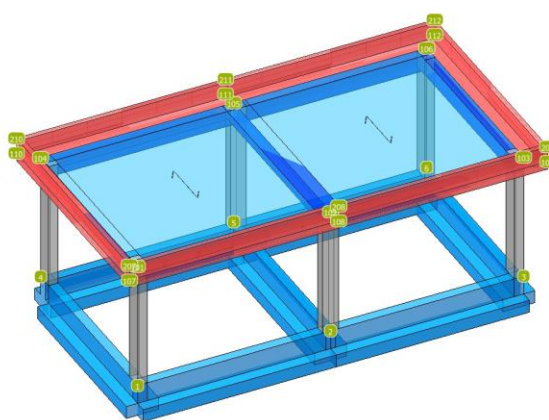
Percentuali Spostamento masse impalcati

Posizione	% Spostamento direzione X	% Spostamento direzione Y
1	0	-5
2	5	0
3	0	5
4	-5	0

Nodi - Geometria e vincoli

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
	Coordinate [m]			Vincoli						
1	0.000	0.500	0.000	1	1	0	0	0	1	0
2	6.000	0.500	0.000	1	1	0	0	0	1	0
3	12.000	0.500	0.000	1	1	0	0	0	1	0
4	0.000	6.500	0.000	1	1	0	0	0	1	0
5	6.000	6.500	0.000	1	1	0	0	0	1	0
6	12.000	6.500	0.000	1	1	0	0	0	1	0
101	0.000	0.500	4.000	0	0	0	0	0	0	1
102	6.000	0.500	4.000	0	0	0	0	0	0	1
103	12.000	0.500	4.000	0	0	0	0	0	0	1
104	0.000	6.500	4.000	0	0	0	0	0	0	1
105	6.000	6.500	4.000	0	0	0	0	0	0	1
106	12.000	6.500	4.000	0	0	0	0	0	0	1
107	-0.500	0.000	4.000	0	0	0	0	0	0	1
108	6.000	0.000	4.000	0	0	0	0	0	0	1
109	12.500	0.000	4.000	0	0	0	0	0	0	1

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
110	-0.500	7.000	4.000	0	0	0	0	0	0	1
111	6.000	7.000	4.000	0	0	0	0	0	0	1
112	12.500	7.000	4.000	0	0	0	0	0	0	1
207	-0.500	0.000	4.500	0	0	0	0	0	0	2
208	6.000	0.000	4.500	0	0	0	0	0	0	2
209	12.500	0.000	4.500	0	0	0	0	0	0	2
210	-0.500	7.000	4.500	0	0	0	0	0	0	2
211	6.000	7.000	4.500	0	0	0	0	0	0	2
212	12.500	7.000	4.500	0	0	0	0	0	0	2



Input - Aste - Tabella sezioni tipo

Tipo	Nome	Base	Altezza	Larg.mag.
R		m	m	m
	50x30	0.50	0.30	0.00
	70x25	0.70	0.25	0.00
	30x50	0.30	0.50	0.00

Tipo	Nome	Alt. sup.	Base sup.	Alt. inf.	Base inf.	Larg.mag.
T		m	m	m	m	m
	Sezione T 0	0.60	0.30	0.40	1.00	1.00

Aste - Geometria e vincoli

	Ni	Nf	Vin c.	Sez.	Mat.	Crit.pr .	Rot °	f.f.	xi	yi	zi	xf	yf	zf	Tipo	L2	L3
									m							m	
1	1	101	I-I	30x50	C35/45	CLS_Pil astri_N D	0.0 0	1010	0.00	0.00	0.00	0.00	0.00	0.00	Pila .	4.00	4.00
2	2	102	I-I	50x30	C35/45	CLS_Pil astri_N D	0.0 0	2020	0.00	0.00	0.00	0.00	0.00	0.00	Pila .	4.00	4.00
3	3	103	I-I	30x50	C35/45	CLS_Pil astri_N D	0.0 0	3030	0.00	0.00	0.00	0.00	0.00	0.00	Pila .	4.00	4.00
4	4	104	I-I	30x50	C35/45	CLS_Pil astri_N D	0.0 0	7070	0.00	0.00	0.00	0.00	0.00	0.00	Pila .	4.00	4.00

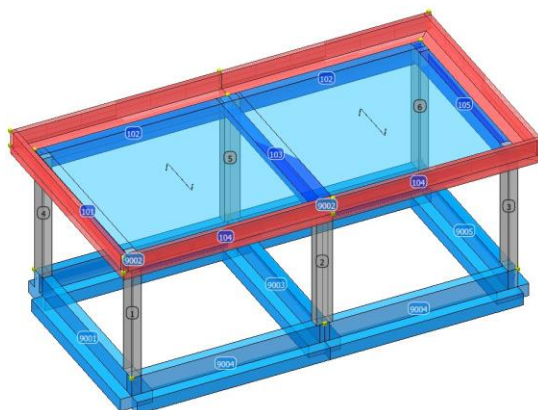
**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 14 di 103

	Ni	Nf	Vin c.	Sez.	Mat.	Crit.pr .	Rot .	f.f.	xi	yi	zi	xf	yf	zf	Tipo	L2	L3
5	5	105	I-I	50x30	C35/45	CLS_Pil astri_N D	0.0 0	8080	0.00	0.00	0.00	0.00	0.00	0.00	Pila .	4.00	4.00
6	6	106	I-I	30x50	C35/45	CLS_Pil astri_N D	0.0 0	9090	0.00	0.00	0.00	0.00	0.00	0.00	Pila .	4.00	4.00
101	101	104	I-I	30x50	C35/45	CLS_Tra viAlte_ ND	0.0 0	9197	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	6.00	6.00
102	104	105	I-I	30x50	C35/45	CLS_Tra viAlte_ ND	0.0 0	9798	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	6.00	6.00
102	105	106	I-I	30x50	C35/45	CLS_Tra viAlte_ ND	0.0 0	9899	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	6.00	6.00
103	105	102	I-I	70x25	C35/45	CLS_Tra viSpess ore ND	0.0 0	8882	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	6.00	6.00
104	102	101	I-I	30x50	C35/45	CLS_Tra viAlte_ ND	0.0 0	9291	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	6.00	6.00
104	103	102	I-I	30x50	C35/45	CLS_Tra viAlte_ ND	0.0 0	9392	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	6.00	6.00
105	106	103	I-I	30x50	C35/45	CLS_Tra viAlte_ ND	0.0 0	8882	0.00	0.00	0.00	0.00	0.00	0.00	Trav e	6.00	6.00
9001	1	4	I-I	Sezione T 0	C35/45	CLS_Tra viFonda zione_R ett ND	0.0 0	8282	0.00	0.00	0.00	0.00	0.00	0.00	Fond .	6.00	6.00
9002	4	5	I-I	Sezione T 0	C35/45	CLS_Tra viFonda zione_R ett ND	0.0 0	9798	0.00	0.00	0.00	0.00	0.00	0.00	Fond .	6.00	6.00
9002	5	6	I-I	Sezione T 0	C35/45	CLS_Tra viFonda zione_R ett ND	0.0 0	9899	0.00	0.00	0.00	0.00	0.00	0.00	Fond .	6.00	6.00
9003	5	2	I-I	Sezione T 0	C35/45	CLS_Tra viFonda zione_R ett ND	0.0 0	8282	0.00	0.00	0.00	0.00	0.00	0.00	Fond .	6.00	6.00
9004	2	1	I-I	Sezione T 0	C35/45	CLS_Tra viFonda zione_R ett ND	0.0 0	9291	0.00	0.00	0.00	0.00	0.00	0.00	Fond .	6.00	6.00
9004	3	2	I-I	Sezione T 0	C35/45	CLS_Tra viFonda zione_R ett ND	0.0 0	9392	0.00	0.00	0.00	0.00	0.00	0.00	Fond .	6.00	6.00
9005	6	3	I-I	Sezione T 0	C35/45	CLS_Tra viFonda zione_R ett ND	0.0 0	8282	0.00	0.00	0.00	0.00	0.00	0.00	Fond .	6.00	6.00



Aste - Carichi

Descrizione carichi aste

UnifG	Uniforme globale
UnifL	Uniforme locale
VarG	Variabile lineare globale
VarL	Variabile lineare locale
PolG	Poligonale globale
Termico	Distorsione termica
Torcente	Carico torcente
Precomp.	Carico da precompressione
POLL	Poligonale locale

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					m	car. dist. kN/m coppie torc. kN			m	car. dist. kN/m coppie torc. kN		
Pilastro 1												
30x50	1	101	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	4.00	0.00	0.00	3.75
Pilastro 2												
50x30	2	102	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	4.00	0.00	0.00	3.75
Pilastro 3												
30x50	3	103	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	4.00	0.00	0.00	3.75
Pilastro 4												
30x50	4	104	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	4.00	0.00	0.00	3.75
Pilastro 5												
50x30	5	105	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	4.00	0.00	0.00	3.75
Pilastro 6												
30x50	6	106	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	4.00	0.00	0.00	3.75
Trave 101												
30x50	101	104	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	6.00	0.00	0.00	3.75
Trave 102												
30x50	104	105	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	6.00	0.00	0.00	3.75
30x50	104	105	QP Solai	PolG	0.15	0.00	0.00	8.83	6.00	0.00	0.00	8.84
30x50	104	105	QFissi Solai	PolG	0.15	0.00	0.00	7.12	6.00	0.00	0.00	7.13
30x50	104	105	QV Solai	PolG	0.15	0.00	0.00	1.42	6.00	0.00	0.00	1.43
30x50	104	105	Neve	PolG	0.15	0.00	0.00	1.71	6.00	0.00	0.00	1.71
30x50	105	106	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	6.00	0.00	0.00	3.75
30x50	105	106	QP Solai	PolG	0.00	0.00	0.00	8.83	5.85	0.00	0.00	8.84
30x50	105	106	QFissi Solai	PolG	0.00	0.00	0.00	7.12	5.85	0.00	0.00	7.13
30x50	105	106	QV Solai	PolG	0.00	0.00	0.00	1.42	5.85	0.00	0.00	1.43
30x50	105	106	Neve	PolG	0.00	0.00	0.00	1.71	5.85	0.00	0.00	1.71
Trave 103												
70x25	105	102	Peso Proprio	UnifG	0.00	0.00	0.00	4.38	6.00	0.00	0.00	4.38
Trave 104												
30x50	102	101	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	6.00	0.00	0.00	3.75

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

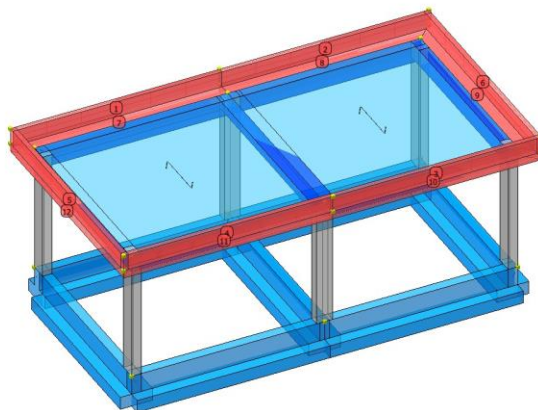
Maggio 2021

Pagina 16 di 103

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
30x50	102	101	QP Solai	PolG	0.00	0.00	0.00	8.84	5.85	0.00	0.00	8.83
30x50	102	101	QFissi Solai	PolG	0.00	0.00	0.00	7.13	5.85	0.00	0.00	7.12
30x50	102	101	QV Solai	PolG	0.00	0.00	0.00	1.43	5.85	0.00	0.00	1.42
30x50	102	101	Neve	PolG	0.00	0.00	0.00	1.71	5.85	0.00	0.00	1.71
30x50	103	102	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	6.00	0.00	0.00	3.75
30x50	103	102	QP Solai	PolG	0.15	0.00	0.00	8.84	6.00	0.00	0.00	8.83
30x50	103	102	QFissi Solai	PolG	0.15	0.00	0.00	7.13	6.00	0.00	0.00	7.12
30x50	103	102	QV Solai	PolG	0.15	0.00	0.00	1.43	6.00	0.00	0.00	1.42
30x50	103	102	Neve	PolG	0.15	0.00	0.00	1.71	6.00	0.00	0.00	1.71
Trave 105												
30x50	106	103	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	6.00	0.00	0.00	3.75
Fondazione 9001												
Sezione T 0	1	4	Peso Proprio	UnifG	0.00	0.00	0.00	14.50	5.50	0.00	0.00	14.50
Sezione T 0	1	4	Muri esterni	UnifG	0.00	0.00	0.00	10.00	5.50	0.00	0.00	10.00
Fondazione 9002												
Sezione T 0	4	5	Peso Proprio	UnifG	0.00	0.00	0.00	14.50	6.00	0.00	0.00	14.50
Sezione T 0	4	5	Muri esterni	UnifG	0.00	0.00	0.00	10.00	6.00	0.00	0.00	10.00
Sezione T 0	5	6	Peso Proprio	UnifG	0.00	0.00	0.00	14.50	6.00	0.00	0.00	14.50
Sezione T 0	5	6	Muri esterni	UnifG	0.00	0.00	0.00	10.00	6.00	0.00	0.00	10.00
Fondazione 9003												
Sezione T 0	5	2	Peso Proprio	UnifG	0.00	0.00	0.00	14.50	5.70	0.00	0.00	14.50
Fondazione 9004												
Sezione T 0	2	1	Peso Proprio	UnifG	0.00	0.00	0.00	14.50	6.00	0.00	0.00	14.50
Sezione T 0	2	1	Muri esterni	UnifG	0.00	0.00	0.00	10.00	6.00	0.00	0.00	10.00
Sezione T 0	3	2	Peso Proprio	UnifG	0.00	0.00	0.00	14.50	6.00	0.00	0.00	14.50
Sezione T 0	3	2	Muri esterni	UnifG	0.00	0.00	0.00	10.00	6.00	0.00	0.00	10.00
Fondazione 9005												
Sezione T 0	6	3	Peso Proprio	UnifG	0.00	0.00	0.00	14.50	5.50	0.00	0.00	14.50
Sezione T 0	6	3	Muri esterni	UnifG	0.00	0.00	0.00	10.00	5.50	0.00	0.00	10.00

Pareti - geometria e vincoli

Parete	Nodi	Tipo	Materiale	Criterio	N.P.	N.P.X	N.P.Y	Spess.
								m
1	110-111-211-210	Discreto	C35/45	CLS Muri ND	12			0.15
2	111-112-212-211	Discreto	C35/45	CLS Muri ND	12			0.15
3	109-108-208-209	Discreto	C35/45	CLS Muri ND	12			0.15
4	108-107-207-208	Discreto	C35/45	CLS Muri ND	12			0.15
5	107-110-210-207	Discreto	C35/45	CLS Muri ND	12			0.15
6	209-212-112-109	Discreto	C35/45	CLS Muri ND	12			0.15
7	105-111-110-104	Discreto	C35/45	CLS Muri ND	36	6	6	0.25
8	106-112-111-105	Discreto	C35/45	CLS Muri ND	36	6	6	0.25
9	109-112-106-103	Discreto	C35/45	CLS Muri ND	36	6	6	0.25
10	108-109-103-102	Discreto	C35/45	CLS Muri ND	36	6	6	0.25
11	107-108-102-101	Discreto	C35/45	CLS Muri ND	36	6	6	0.25
12	107-101-104-110	Discreto	C35/45	CLS Muri ND	36	6	6	0.25



Muri - Carichi

Shell	Indice dello shell
Cond.	Condizione di carico
Tipo	Tipologia di spinta
γ	Peso specifico: terreno o acqua
Q	Valore del carico uniforme
Vert.1	Valore del carico nel primo vertice ⁽¹⁾
Vert.2	Valore del carico nel secondo vertice ⁽¹⁾
Vert.3	Valore del carico nel terzo vertice ⁽¹⁾
Vert.4	Valore del carico nel quarto vertice ⁽¹⁾
Hw	Altezza del pelo libero dell'acqua

⁽¹⁾: Per shell con numero di vertici maggiori 4, per carichi trapezoidali, il valore del carico nei vertici e' stampato a gruppi di 4 secondo l'ordine con cui i vertici sono stati definiti

She 11	Cond.	Tipo	Q	Vert.1	Vert.2	Vert.3	Vert.4	Hw	γ
			kN/m ²	kN/m ²	kN/m ²	kN/m ²	kN/m ²	m	daN/m ³
1	Peso Proprio	Peso Proprio kN	12.19						
2	Peso Proprio	Peso Proprio kN	12.19						
3	Peso Proprio	Peso Proprio kN	12.19						
4	Peso Proprio	Peso Proprio kN	12.19						
5	Peso Proprio	Peso Proprio kN	13.13						
6	Peso Proprio	Peso Proprio kN	13.13						
7	Peso Proprio	Peso Proprio kN	19.53						
7	Neve	Uniforme GLOBZ	0.60						
7	permanenti	Uniforme GLOBZ	2.00						
7	ACCIDENTALI COPERTURA	Uniforme GLOBZ	0.50						
8	Peso Proprio	Peso Proprio kN	19.53						
8	Neve	Uniforme GLOBZ	0.60						
8	permanenti	Uniforme GLOBZ	2.00						
8	ACCIDENTALI COPERTURA	Uniforme GLOBZ	0.50						
9	Peso Proprio	Peso Proprio kN	20.31						
9	Neve	Uniforme GLOBZ	0.60						
9	permanenti	Uniforme GLOBZ	2.00						
9	ACCIDENTALI COPERTURA	Uniforme GLOBZ	0.50						
10	Peso Proprio	Peso Proprio kN	19.53						
10	Neve	Uniforme GLOBZ	0.60						
10	permanenti	Uniforme GLOBZ	2.00						

She 11	Cond.	Tipo	Q	Vert.1	Vert.2	Vert.3	Vert.4	Hw	γ
10	ACCIDENTALI COPERTURA	Uniforme_GLOBZ	0.50						
11	Peso Proprio	Peso Proprio kN	19.53						
11	Neve	Uniforme_GLOBZ	0.60						
11	permanenti	Uniforme_GLOBZ	2.00						
11	ACCIDENTALI COPERTURA	Uniforme_GLOBZ	0.50						
12	Peso Proprio	Peso Proprio kN	20.31						
12	Neve	Uniforme_GLOBZ	0.60						
12	permanenti	Uniforme_GLOBZ	2.00						
12	ACCIDENTALI COPERTURA	Uniforme_GLOBZ	0.50						

Tabella solai tipo

Sol.N°	Descrizione	Spessore	QP	QF	QVar.	ψ_0	ψ_1	ψ_2	Luce netta	Def	%QX	%QY
		m	daN/m ²	daN/m ²	daN/m ²							
1	Tetti e Coperture	0.25	310.00	250.00	50.00	0.00	0.00	0.00	No	No	100	0

Dati solai

Solaio n°	Nodi	Tipo
1	105-102-103-106	Tetti e Coperture
2	104-101-102-105	Tetti e Coperture

Risultati Analisi Dinamica - Baricentri masse e masse

Scenario di calcolo: **ScenarioNT_2018 A2_SLV_SLD_STR_GEO**

Piano	Rigido	Massa	X	Y	Z
		kN	m	m	m
0	No	0.00	0.00	0.00	0.00
1	Si	796.75	5.96	3.15	4.01
2	Si	24.22	7.47	3.15	4.44

Piano	Rigido	Massa	X	Y	Z
		kN	m	m	m
0	No	0.00	0.00	0.00	0.00
1	Si	796.75	6.61	3.50	4.01
2	Si	24.22	8.12	3.50	4.44

Piano	Rigido	Massa	X	Y	Z
		kN	m	m	m
0	No	0.00	0.00	0.00	0.00
1	Si	796.75	5.96	3.85	4.01
2	Si	24.22	7.47	3.85	4.44

Piano	Rigido	Massa	X	Y	Z
		kN	m	m	m
0	No	0.00	0.00	0.00	0.00
1	Si	796.75	5.31	3.50	4.01
2	Si	24.22	6.82	3.50	4.44

Taglianti di piano

Scenario di calcolo: **ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO**

Scenario di calcolo: **ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO**

I taglianti sono dati per combinazioni di calcolo C-S-Pm con C=Combinazione(1,2,...) S=Sisma(I,II) Pm=posizione masse(1,2,...). Le azioni, complessive, sono riferite al sistema di riferimento globale.

$\Theta = F_z \cdot dr / (F_h \cdot H)$ con:

Fz Forza verticale

dr Spostamento medio del piano rispetto al piano inferiore

Fh Tagliante

H Altezza del piano

dx spostamento medio di piano in direzione X

dy spostamento medio di piano in direzione Y

dr $((dx_s - dx_i)^2 + (dy_s - dy_i)^2)^{0.5}$ s=impalcato superiore i=impalcato inferiore

Nel caso di combinazioni sismiche l'aliquota dovuta al sisma di dx e dy è valutata secondo le indicazioni in 7.3.3, moltiplicando lo spostamento per μ_d

Combinazione: 4-I-1 (SISMAX1 SLV)

Piano	Fx	Fy	Fz	dx	dy	Θ
	kN	kN	kN	mm	mm	
0	-138.06	-0.00	856.46	0.00	0.00	--
1	138.06	0.00	-766.46	0.03	0.00	0.000042
2	-2.95	-0.00	0.00	0.87	0.03	0.000000

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kN	kN	kN	kN	kN	kN	kN	kN
0	-138.06	-0.00	0.00	0.00	0.00	0.00	-138.06	-0.00
1	138.06	0.00	0.00	0.00	0.00	0.00	138.06	0.00
2	0.00	0.00	0.00	0.00	-2.95	-0.00	-2.95	-0.00

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	--	--	--
1	--	--	--
2	--	--	--

Combinazione: 4-I-2 (SISMAX1 SLV)

Piano	Fx	Fy	Fz	dx	dy	Θ
	kN	kN	kN	mm	mm	
0	-139.36	0.55	857.71	0.00	0.00	--
1	139.36	-0.55	-767.71	0.03	0.00	0.000042
2	-3.67	0.01	0.03	0.88	0.02	0.000000

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kN	kN	kN	kN	kN	kN	kN	kN
0	-139.36	0.55	0.00	0.00	0.00	0.00	-139.36	0.55
1	139.36	-0.55	0.00	0.00	0.00	0.00	139.36	-0.55
2	0.00	0.00	0.00	0.00	-3.67	0.01	-3.67	0.01

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--

Combinazione: 4-I-3 (SISMAX1 SLV)

Piano	Fx	Fy	Fz	dx	dy	Θ
	kN	kN	kN	mm	mm	
0	-138.45	0.00	856.46	0.00	0.00	--
1	138.45	-0.00	-766.46	0.03	0.00	0.000042
2	-4.78	0.00	0.00	0.87	0.03	0.000000

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kN	kN	kN	kN	kN	kN	kN	kN
0	-138.45	0.00	0.00	0.00	0.00	0.00	-138.45	0.00
1	138.45	-0.00	0.00	0.00	0.00	0.00	138.45	-0.00
2	0.00	0.00	0.00	0.00	-4.78	0.00	-4.78	0.00

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	--	--	--
1	--	--	--
2	--	--	--

Combinazione: 4-I-4 (SISMAX1 SLV)

Piano	Fx	Fy	Fz	dx	dy	Θ
	kN	kN	kN	mm	mm	
0	-139.35	-0.56	855.21	0.00	0.00	--
1	139.35	0.56	-765.21	0.03	0.00	0.000042
2	-4.47	-0.01	-0.03	0.88	0.04	0.000011

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kN	kN	kN	kN	kN	kN	kN	kN
0	-139.35	-0.56	0.00	0.00	0.00	0.00	-139.35	-0.56
1	139.35	0.56	0.00	0.00	0.00	0.00	139.35	0.56
2	0.00	0.00	0.00	0.00	-4.47	-0.01	-4.47	-0.01

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	0.00	0.00	100.00

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--

Combinazione: 5-I-1 (SISMAY1 SLV)

Piano	Fx	Fy	Fz	dx	dy	Θ
	kN	kN	kN	mm	mm	
0	0.00	-137.18	905.91	0.00	0.00	--
1	-0.00	137.18	-815.91	-0.00	0.04	0.000059
2	0.00	-3.46	-0.07	-0.00	0.99	0.000036

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kN	kN	kN	kN	kN	kN	kN	kN
0	0.00	-137.18	0.00	0.00	0.00	0.00	0.00	-137.18
1	-0.00	137.18	0.00	0.00	0.00	0.00	-0.00	137.18
2	0.00	0.00	0.00	0.00	0.00	-3.46	0.00	-3.46

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	--	--	--
1	--	--	--
2	--	--	--

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	0.00	0.00	100.00

Combinazione: 5-I-2 (SISMAY1 SLV)

Piano	Fx	Fy	Fz	dx	dy	Θ
	kN	kN	kN	mm	mm	
0	-1.87	-134.77	908.62	0.00	0.00	--
1	1.87	134.77	-818.62	0.00	0.04	0.000059
2	-0.01	-3.15	0.02	0.00	0.97	0.000000

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kN	kN	kN	kN	kN	kN	kN	kN
0	-1.87	-134.77	0.00	0.00	0.00	0.00	-1.87	-134.77
1	1.87	134.77	0.00	0.00	0.00	0.00	1.87	134.77
2	0.00	0.00	0.00	0.00	-0.01	-3.15	-0.01	-3.15

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	0.00	0.00	100.00

Combinazione: 5-I-3 (SISMAY1 SLV)

Piano	Fx	Fy	Fz	dx	dy	Θ
	kN	kN	kN	mm	mm	
0	-0.00	-137.12	911.34	0.00	0.00	--
1	0.00	137.12	-821.34	0.00	0.04	0.000059
2	0.00	-3.31	0.11	0.00	0.99	0.000000

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kN	kN	kN	kN	kN	kN	kN	kN
0	-0.00	-137.12	0.00	0.00	0.00	0.00	-0.00	-137.12
1	0.00	137.12	0.00	0.00	0.00	0.00	0.00	137.12
2	0.00	0.00	0.00	0.00	0.00	-3.31	0.00	-3.31

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	--	--	--
1	--	--	--
2	--	--	--

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	0.00	0.00	100.00

Combinazione: 5-I-4 (SISMAY1 SLV)

Piano	Fx	Fy	Fz	dx	dy	Θ
	kN	kN	kN	mm	mm	
0	1.87	-134.76	908.62	0.00	0.00	--
1	-1.87	134.76	-818.62	-0.00	0.04	0.000059
2	0.01	-3.46	0.02	-0.00	0.97	0.000000

Piano	FxPil/Isol.	FyPil/Isol.	FxPar	FyPar	FxShell	FyShell	FxTot	FyTot
	kN	kN	kN	kN	kN	kN	kN	kN
0	1.87	-134.76	0.00	0.00	0.00	0.00	1.87	-134.76
1	-1.87	134.76	0.00	0.00	0.00	0.00	-1.87	134.76
2	0.00	0.00	0.00	0.00	0.01	-3.46	0.01	-3.46

Percentuali assorbite in direzione X

Piano	%Pil/Isol. FX	%Par. FX	%Shell. FX
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	--	--	--

Percentuali assorbite in direzione Y

Piano	%Pil/Isol. FY	%Par. FY	%Shell. FY
0	100.00	0.00	0.00
1	100.00	0.00	0.00
2	0.00	0.00	100.00

Centri di rigidezza e Centri di massa

Centri rigidezze

Piano	Kx	Ky	Kxy	K ϕ	X	Y	r ² /ls ² >=1
	kN/m	kN/m	kN/m	kN*m/rad	m	m	
1	5.838290E04	6.314293E04	5.478758E-08	2.820192E06	6.00	3.51	2.459
2	5.748045E04	5.961494E04	7.993437E-08	2.811293E06	6.00	3.51	2.596

Ellissi delle rigidezze

Piano	K ξ	K η	alfa	r ξ	r η
	kN/m	kN/m	°	m	m
1	5.838290E04	6.314293E04	0.00	6.68	6.95
2	5.748045E04	5.961494E04	0.00	6.87	6.99

Baricentri masse per posizione masse

Piano	Pos.Masse	X	Y	Peso Sism.
		m	m	kN
0	1	0.00	0.00	0.00
0	2	0.00	0.00	0.00
0	3	0.00	0.00	0.00
0	4	0.00	0.00	0.00
1	1	5.96	3.15	796.75
1	2	6.61	3.50	796.75
1	3	5.96	3.85	796.75
1	4	5.31	3.50	796.75
2	1	7.47	3.15	24.22
2	2	8.12	3.50	24.22
2	3	7.47	3.85	24.22
2	4	6.82	3.50	24.22

Verifica Degli Spostamenti Relativi

Scenario di calcolo: **ScenarioNT_2018 A2_SLV_SLD_STR_GEO**

Interp.	Comb.	η_{Xv}	η_{Xh}	η_{Yv}	η_{Yh}	Nodo1	Nodo2	η	η_{Amm}	Cs
		mm	mm	mm	mm			mm	mm	
0-1	(9+10)-V-3	0.00	0.41	0.08	1.19	1	101	1.27	20.00	16
0-1	(9+10)-V-4	0.00	0.19	0.08	0.97	2	102	1.04	20.00	19
0-1	(9+10)-II-4	0.00	0.41	0.08	1.19	3	103	1.27	20.00	16
0-1	(9+10)-V-3	0.00	0.16	0.08	1.19	4	104	1.27	20.00	16
0-1	(9+10)-V-4	0.00	0.37	0.08	0.97	5	105	1.04	20.00	19
0-1	(9+10)-II-4	0.00	0.16	0.08	1.19	6	106	1.27	20.00	16
1-2	(9+10)-X-4	0.10	0.02	0.03	0.02	107	207	0.12	2.50	21
1-2	(9+10)-V-4	0.00	0.01	0.05	0.09	108	208	0.14	2.50	17
1-2	(9+10)-VII-3	0.10	0.02	0.03	0.02	109	209	0.12	2.50	21
1-2	(9+10)-IV-3	0.10	0.02	0.02	0.03	110	210	0.12	2.50	21
1-2	(9+10)-V-4	0.00	0.00	0.07	0.09	111	211	0.16	2.50	15
1-2	(9+10)-I-4	0.10	0.02	0.02	0.03	112	212	0.12	2.50	21
Minimo										
1-2	(9+10)-V-4	0.00	0.00	0.07	0.09	111	211	0.16	2.50	15

Periodi di vibrazione e Masse modali

Scenario di calcolo: **ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO**

Posizione masse 1

Numero di Frequenze calcolate =15, filtrate=8

N	T	Coeff. Partecipazione		Masse Modali		Percentuali	
	s			kgm*g			
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.2548	-0.001	90.569	0.00	80441.50	0.00	97.98
2(2)	0.2490	90.751	0.001	80764.84	0.00	98.38	0.00
3(3)	0.1916	-9.951	0.000	971.09	0.00	1.18	0.00
4(4)	0.0728	0.000	-9.523	0.00	889.37	0.00	1.08
5(5)	0.0689	4.458	0.000	194.91	0.00	0.24	0.00
6(6)	0.0654	0.000	-7.011	0.00	481.99	0.00	0.59
7(7)	0.0625	3.417	0.001	114.47	0.00	0.14	0.00
8(10)	0.0392	-0.001	-4.571	0.00	204.94	0.00	0.25
Somma delle Masse Modali [kgm*g]				82045.31	82017.79		
Masse strutturali libere [kgm*g]				82096.40	82096.40		
Percentuale				99.94	99.90	99.94	99.90

Masse e coefficienti di partecipazione rotazionali:

N	T(s)	Coeff. Partecipazione		Masse Modali		Percentuali	
				kgm*g			
1(1)	0.2548		7.819		599.47		0.03
2(2)	0.2490		81.532		65189.70		3.17
3(3)	0.1916		447.712		1965706.97		95.45
4(4)	0.0728		-1.055		10.91		0.00
5(5)	0.0689		-28.551		7994.21		0.39
6(6)	0.0654		-0.779		5.95		0.00
7(7)	0.0625		34.880		11930.60		0.58
8(10)	0.0392		-1.294		16.41		0.00

Posizione masse 2

Numero di Frequenze calcolate =15, filtrate=8

N	T	Coeff. Partecipazione		Masse Modali		Percentuali	
	s			kgm*g			
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.2575	1.368	89.395	18.34	78369.87	0.02	95.46
2(2)	0.2480	91.279	-1.482	81708.37	21.54	99.53	0.03
3(3)	0.1890	-0.816	-14.404	6.54	2034.57	0.01	2.48
4(4)	0.0731	2.436	9.071	58.18	806.86	0.07	0.98
5(5)	0.0714	-3.140	6.137	96.66	369.36	0.12	0.45
6(6)	0.0636	-3.389	2.781	112.66	75.82	0.14	0.09
7(7)	0.0622	-2.186	-3.670	46.86	132.11	0.06	0.16
8(10)	0.0403	-0.607	-4.053	3.62	161.11	0.00	0.20
Somma delle Masse Modali [kgm*g]				82051.23	81971.23		
Masse strutturali libere [kgm*g]				82096.40	82096.40		
Percentuale				99.94	99.85	99.94	99.85

Masse e coefficienti di partecipazione rotazionali:

N	T(s)	Coeff. Partecipazione		Masse Modali		Percentuali	
				kgm*g			
1(1)	0.2575		137.717		185992.22		9.00
2(2)	0.2480		1.510		22.35		0.00
3(3)	0.1890		434.605		1852296.17		89.63
4(4)	0.0731		23.335		5339.91		0.26
5(5)	0.0714		12.926		1638.62		0.08
6(6)	0.0636		-22.611		5013.73		0.24
7(7)	0.0622		29.513		8541.94		0.41
8(10)	0.0403		-8.909		778.36		0.04

Posizione masse 3

Numero di Frequenze calcolate =15, filtrate=8

N	T s	Coeff. Partecipazione		Masse Modali kgm*g		Percentuali	
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.2548	0.000	90.550	0.00	80407.58	0.00	97.94
2(2)	0.2487	90.915	-0.000	81057.41	0.00	98.73	0.00
3(3)	0.1919	8.267	-0.000	670.14	0.00	0.82	0.00
4(4)	0.0742	0.000	9.942	0.00	969.27	0.00	1.18
5(5)	0.0705	-4.696	0.001	216.24	0.00	0.26	0.00
6(6)	0.0641	0.000	6.645	0.00	433.02	0.00	0.53
7(7)	0.0609	-3.208	0.000	100.93	0.00	0.12	0.00
8(10)	0.0388	0.000	-4.405	0.00	190.32	0.00	0.23
Somma delle Masse Modali [kgm*g]				82044.73	82000.19		
Masse strutturali libere [kgm*g]				82096.40	82096.40		
Percentuale				99.94	99.88	99.94	99.88

Masse e coefficienti di partecipazione rotazionali:

N	T(s)	Coeff. Partecipazione		Masse Modali kgm*g		Percentuali	
1(1)	0.2548		7.818		599.37		0.03
2(2)	0.2487		-73.834		53460.89		2.60
3(3)	0.1919		448.943		1976526.79		95.98
4(4)	0.0742		1.098		11.83		0.00
5(5)	0.0705		-34.594		11735.94		0.57
6(6)	0.0641		0.733		5.28		0.00
7(7)	0.0609		30.365		9041.80		0.44
8(10)	0.0388		-1.268		15.77		0.00

Posizione masse 4

Numero di Frequenze calcolate =15, filtrate=8

N	T s	Coeff. Partecipazione		Masse Modali kgm*g		Percentuali	
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.2576	-1.367	89.388	18.33	78357.43	0.02	95.45
2(2)	0.2480	91.278	1.482	81706.56	21.55	99.53	0.03
3(3)	0.1892	-0.820	14.444	6.59	2045.83	0.01	2.49
4(4)	0.0730	-2.467	9.029	59.67	799.50	0.07	0.97
5(5)	0.0713	-3.137	-6.198	96.49	376.68	0.12	0.46
6(6)	0.0636	3.403	2.766	113.57	75.02	0.14	0.09
7(7)	0.0622	-2.169	3.691	46.15	133.60	0.06	0.16
8(10)	0.0404	0.412	-4.268	1.67	178.67	0.00	0.22
Somma delle Masse Modali [kgm*g]				82049.03	81988.27		
Masse strutturali libere [kgm*g]				82096.40	82096.40		
Percentuale				99.94	99.87	99.94	99.87

Masse e coefficienti di partecipazione rotazionali:

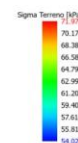
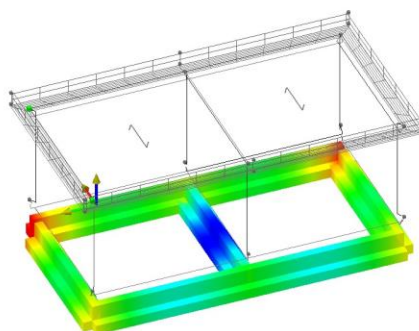
N	T(s)	Coeff. Partecipazione		Masse Modali kgm*g		Percentuali	
1(1)	0.2576		-122.548		147277.18		7.18
2(2)	0.2480		1.782		31.15		0.00
3(3)	0.1892		437.489		1876956.95		91.47
4(4)	0.0730		-21.291		4445.24		0.22
5(5)	0.0713		11.723		1347.67		0.07
6(6)	0.0636		23.050		5210.15		0.25
7(7)	0.0622		30.435		9083.67		0.44
8(10)	0.0404		6.872		463.10		0.02

Risultati Analisi Dinamica - Massime tensioni sul terreno aste per combinazione

Scenario di calcolo: **ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO**

Combinazione	Asta	N.in.	N.fin.	SigmaMax kPa	SigmaMin
1	9002	5	6	71.1	51.8
2	9002	5	6	74.1	54.2
3	9002	5	6	73.9	53.9
4-I-1	9002	5	6	60.5	37.4
4-I-2	9002	5	6	59.3	37.4
4-I-3	9002	5	6	58.0	37.4
4-I-4	9002	5	6	59.2	37.4
4-II-1	9002	4	5	60.5	37.4
4-II-2	9002	4	5	59.2	37.4
4-II-3	9002	4	5	58.0	37.4
4-II-4	9002	4	5	59.3	37.4
5-I-1	9002	4	5	69.4	35.0
5-I-2	9002	5	6	71.6	33.3
5-I-3	9002	5	6	69.6	35.1
5-I-4	9002	4	5	71.6	33.2
5-II-1	9004	3	2	64.4	37.6
5-II-2	9004	3	2	66.2	35.9
5-II-3	9004	2	1	64.3	37.5
5-II-4	9004	2	1	66.2	35.9

Tipo diagramma: Tensioni medie terreno
Combinazione corrente : Scenario ScenarioNT_2018 A2_SLV_SLD_STR_GEO - C 2
Tensioni medie terreno aste
Tensioni medie terreno platee



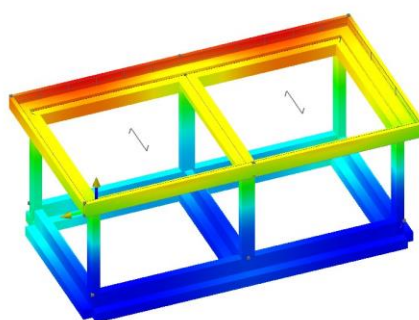
Risultati Analisi Dinamica - Spostamenti massimi - Nodi
Scenario di calcolo: ScenarioNT_2018 A2_SLV_SLD_STR_GEO

la tripletta (Cb [-SubC-Cbm]) indica la Combinazione - SottoCombinazione sismica - Posizione Masse, nel caso non sismico mancano SubC-Cbm

Nodo	Trasl. X mm	Trasl. Y mm	Trasl. Z mm	Rotaz. X °	Rotaz. Y °	Rotaz. Z °
1	0.00 (1)	0.00 (1)	-2.26 (2)	0.02 (5-II-4)	-0.01 (5-II-4)	0.00 (1)
2	0.00 (1)	0.00 (1)	-2.11 (2)	0.01 (5-II-1)	0.00 (4-I-3)	0.00 (1)
3	0.00 (1)	0.00 (1)	-2.26 (2)	0.02 (5-II-2)	0.01 (5-II-2)	0.00 (1)
4	0.00 (1)	0.00 (1)	-2.42 (2)	-0.02 (5-I-4)	-0.01 (5-I-4)	0.00 (1)
5	0.00 (1)	0.00 (1)	-2.20 (2)	-0.01 (5-I-3)	0.00 (4-I-1)	0.00 (1)
6	0.00 (1)	0.00 (1)	-2.42 (2)	-0.02 (5-I-2)	0.01 (5-I-2)	0.00 (1)
101	2.73 (4-I-1)	3.21 (5-I-4)	-2.16 (2)	-0.03 (5-I-4)	0.02 (4-I-3)	0.01 (5-II-4)
102	2.73 (4-I-1)	2.77 (5-I-1)	-2.14 (2)	0.04 (5-II-1)	-0.01 (4-II-1)	-0.01 (5-I-4)
103	-2.73 (4-II-1)	3.21 (5-I-2)	-2.16 (2)	-0.03 (5-I-2)	-0.02 (4-II-3)	-0.01 (5-I-4)
104	2.71 (4-I-3)	3.21 (5-I-4)	-2.32 (2)	0.03 (5-II-4)	0.02 (4-I-1)	-0.01 (5-I-4)
105	2.71 (4-I-3)	2.77 (5-I-1)	-2.22 (2)	-0.04 (5-I-3)	0.01 (4-I-3)	-0.01 (5-I-4)

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
106	-2.71 (4-II-3)	3.21 (5-I-2)	-2.32 (2)	0.03 (5-II-2)	-0.02 (4-II-1)	0.01 (5-II-4)
107	-2.75 (4-II-1)	3.24 (5-I-4)	-2.19 (5-II-4)	-0.02 (5-I-4)	0.02 (2)	0.01 (5-II-4)
108	2.74 (4-I-1)	2.76 (5-I-1)	-2.26 (2)	0.04 (5-II-1)	-0.01 (4-II-3)	-0.01 (5-I-4)
109	2.75 (4-I-1)	3.24 (5-I-2)	-2.19 (5-II-2)	-0.02 (5-I-2)	-0.02 (2)	-0.01 (5-II-2)
110	-2.73 (4-II-3)	3.23 (5-I-4)	-2.39 (5-I-4)	0.02 (5-II-4)	0.02 (2)	-0.01 (5-I-4)
111	2.72 (4-I-3)	2.77 (5-I-1)	-2.37 (2)	-0.04 (5-I-3)	0.01 (4-I-1)	-0.01 (5-I-4)
112	2.73 (4-I-3)	3.23 (5-I-2)	-2.39 (5-II-2)	0.02 (5-II-2)	-0.02 (2)	0.01 (5-I-2)
207	2.89 (4-I-1)	3.46 (5-I-4)	-2.19 (5-II-4)	-0.02 (5-I-4)	0.02 (2)	-0.01 (5-I-4)
208	2.80 (4-I-1)	2.97 (5-I-1)	-2.27 (2)	0.04 (5-II-1)	-0.01 (4-II-3)	-0.01 (5-I-4)
209	-2.89 (4-II-1)	3.45 (5-I-2)	-2.19 (5-II-2)	-0.02 (5-I-2)	-0.02 (2)	0.01 (5-I-2)
210	2.86 (4-I-3)	3.40 (5-I-4)	-2.39 (5-I-4)	0.02 (5-II-4)	0.02 (2)	0.01 (5-II-4)
211	2.78 (4-I-3)	3.11 (5-I-3)	-2.38 (2)	-0.04 (5-I-3)	0.01 (4-I-1)	-0.01 (5-I-4)
212	-2.86 (4-II-3)	3.40 (5-I-2)	-2.38 (5-I-2)	0.02 (5-II-2)	-0.02 (2)	-0.01 (5-II-2)

Tipo diagramma: Deformata
Combinazione corrente : Scenario ScenarioNT_2018 A2_SLV_SLD_STR_GEO - C 5-I
Posizione masse N° 1



Risultati Analisi Dinamica - Reazioni massime - Nodi

Scenario di calcolo: ScenarioNT_2018 A2_SLV_SLD_STR_GEO

Nodo	Rx	Ry	Rz	Mx	My	Mz
	kN	kN	kN	kN*m	kN*m	kN*m
1	18.03 (4-II-1)	-35.84 (5-I-4)	0	0	0	-5.86 (5-I-4)
2	-41.44 (4-I-1)	-13.94 (5-I-3)	0	0	0	-5.96 (4-II-3)
3	-18.03 (4-I-1)	-35.83 (5-I-2)	0	0	0	5.86 (5-I-2)
4	17.48 (4-II-3)	36.34 (5-II-4)	0	0	0	5.90 (5-II-4)
5	-40.92 (4-I-3)	13.78 (5-II-1)	0	0	0	5.93 (4-II-1)
6	-17.48 (4-I-3)	36.33 (5-II-2)	0	0	0	-5.90 (5-II-2)

Risultati Analisi Dinamica - Spostamenti massimi - Impalcato

Scenario di calcolo: ScenarioNT_2018 A2_SLV_SLD_STR_GEO

la tripletta (Cb [-SubC-Cbm]) indica la Combinazione - SottoCombinazione sismica - Posizione Masse, nel caso non sismico mancano SubC-Cbm

Piano	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
	mm	mm	mm			
1	2.59 (4-II-4)	2.78 (5-II-1)	-2.47 (2-1)	0.00 (1-1)	0.00 (1-1)	-0.00 (5-II-4)
2	-2.63 (4-I-4)	2.95 (5-II-2)	-2.41 (2-1)	0.00 (1-1)	0.00 (1-1)	-0.01 (5-II-4)

Risultati Analisi Dinamica - Spostamenti massimi - Impalcato (SLD)

Scenario di calcolo: ScenarioNT_2018 A2_SLV_SLD_STR_GEO

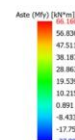
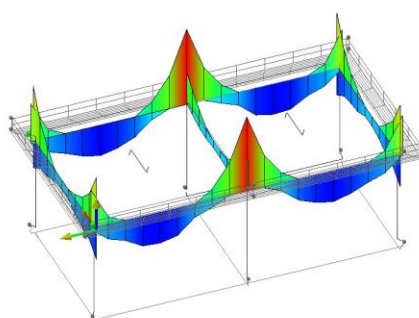
la tripletta (Cb [-SubC-Cbm]) indica la Combinazione - SottoCombinazione sismica - Posizione Masse, nel caso non sismico mancano SubC-Cbm

Piano	Trasl. X mm	Trasl. Y mm	Trasl. Z mm	Rotaz. X °	Rotaz. Y °	Rotaz. Z °
1	0.96 (9-II-4)	1.07 (10-II-1)	-1.76 (6-1)	0.00 (6-1)	0.00 (6-1)	-0.00 (10-II-4)
2	-0.97 (9-I-4)	1.14 (10-II-2)	-1.71 (6-1)	0.00 (6-1)	0.00 (6-1)	-0.00 (10-II-4)

Risultati Analisi Dinamica - Sollecitazioni massime - Involuppi - Travi
Scenario di calcolo: **ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO**

Asta	N.in. N.fin.	N kN	Ty kN	Tz kN	Mt kN*m	My kN*m	Mz kN*m
101	101	0	-3.93 (5-II-4)	-35.71 (5-II-4)	-1.81 (5-II-4)	46.38 (5-II-4)	-1.96 (5-II-4)
	104	0	3.75 (5-I-4)	35.87 (5-I-4)	1.73 (5-I-4)	46.52 (5-I-4)	-1.88 (5-I-4)
102	104	0	8.18 (2)	-51.09 (2)	3.77 (2)	33.32 (4-II-3)	4.09 (2)
	105	0	-10.55 (4-II-3)	74.00 (2)	-4.86 (4-II-3)	66.16 (4-I-3)	5.27 (4-II-3)
102	105	0	10.55 (4-I-3)	-74.00 (2)	4.86 (4-I-3)	66.16 (4-II-3)	5.27 (4-I-3)
	106	0	-8.18 (2)	51.09 (2)	-3.77 (2)	33.32 (4-I-3)	4.09 (2)
103	105	0	0.03 (5-I-4)	-17.93 (5-I-3)	0.13 (5-I-4)	28.90 (5-I-3)	0.09 (5-I-4)
	102	0	0.03 (5-I-4)	17.73 (5-II-3)	-0.13 (5-II-4)	28.26 (5-II-1)	-0.09 (5-I-4)
104	102	0	10.75 (4-II-1)	-73.73 (2)	4.96 (4-II-1)	65.80 (4-I-1)	5.37 (4-II-1)
	101	0	-8.13 (2)	51.60 (2)	-3.75 (2)	34.01 (4-II-1)	4.07 (2)
104	103	0	8.13 (2)	-51.60 (2)	3.75 (2)	34.01 (4-I-1)	4.07 (2)
	102	0	-10.75 (4-I-1)	73.73 (2)	-4.96 (4-I-1)	65.80 (4-II-1)	5.37 (4-I-1)
105	106	0	-3.75 (5-I-2)	-35.87 (5-I-2)	-1.73 (5-I-2)	46.50 (5-I-2)	-1.88 (5-I-2)
	103	0	3.93 (5-II-2)	35.70 (5-II-2)	1.81 (5-II-2)	46.37 (5-II-2)	-1.96 (5-II-2)

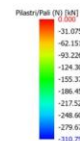
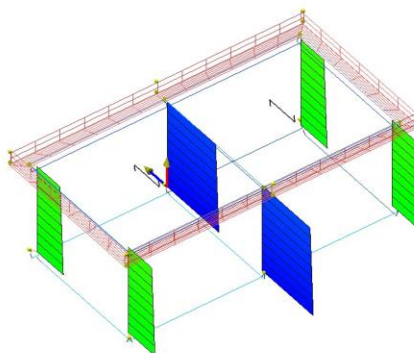
Tipo diagramma: Sollecitazioni
Combinazione corrente : Scenario ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO - C 1
Sollecitazione aste: Momento fl.Y - pilastri/pali: Sforzo Normale
Sollecitazione Muri: S I
Sollecitazione Setti: Six



Risultati Analisi Dinamica - Sollecitazioni massime - Involuppi - Pilastri
Scenario di calcolo: **ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO**

Asta	N.in. N.fin.	N kN	Ty kN	Tz kN	Mt kN*m	My kN*m	Mz kN*m
1	1	-159.79 (2)	-18.03 (4-II-1)	35.84 (5-I-4)	1.01 (5-II-4)	-81.08 (5-I-4)	-34.02 (4-II-1)
	101	-140.29 (2)	-18.03 (4-II-1)	35.84 (5-I-4)	1.01 (5-II-4)	62.27 (5-I-4)	38.08 (4-II-1)
2	2	-308.98 (2)	41.44 (4-I-1)	13.94 (5-I-3)	-1.01 (5-I-4)	-32.12 (5-I-3)	87.41 (4-I-1)
	102	-289.48 (2)	41.44 (4-I-1)	13.94 (5-I-3)	-1.01 (5-I-4)	23.63 (5-I-3)	-78.33 (4-I-1)
3	3	-159.79 (2)	18.03 (4-I-1)	35.83 (5-I-2)	-1.01 (5-I-4)	-81.06 (5-I-2)	34.02 (4-I-1)
	103	-140.29 (2)	18.03 (4-I-1)	35.83 (5-I-2)	-1.01 (5-I-4)	62.26 (5-I-2)	-38.08 (4-I-1)
4	4	-158.93 (2)	-17.48 (4-II-3)	-36.34 (5-II-4)	-1.01 (5-I-4)	82.69 (5-II-4)	33.23 (4-I-3)
	104	-139.43 (2)	-17.48 (4-II-3)	-36.34 (5-II-4)	-1.01 (5-I-4)	-62.67 (5-II-4)	37.10 (4-II-3)
5	5	-310.75 (2)	40.92 (4-I-3)	-13.78 (5-II-1)	-1.01 (5-I-4)	31.79 (5-II-1)	86.38 (4-I-3)
	105	-291.25 (2)	40.92 (4-I-3)	-13.78 (5-II-1)	-1.01 (5-I-4)	-23.31 (5-II-1)	-77.31 (4-I-3)
6	6	-158.93 (2)	17.48 (4-I-3)	-36.33 (5-II-2)	1.01 (5-II-4)	82.67 (5-II-2)	-33.23 (4-II-3)
	106	-139.43 (2)	17.48 (4-I-3)	-36.33 (5-II-2)	1.01 (5-II-4)	-62.65 (5-II-2)	-37.10 (4-I-3)

Tipo diagramma: Sollecitazioni
Combinazione corrente: Scenario ScenarioNT_2018 A2_SLV_SLD_STR_GEO - C 1
Sollecitazione aste: Momento fl.Y - pilastri/pali: Sforzo Normale
Sollecitazione Muri: S I
Sollecitazione Setti: Sxx

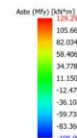
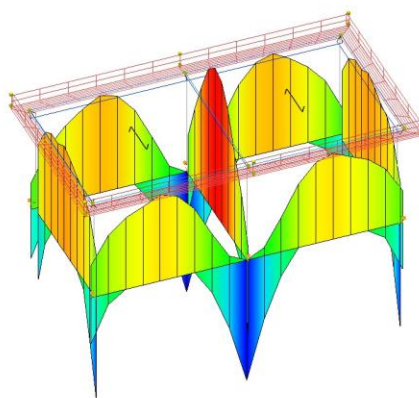


Risultati Analisi Dinamica - Sollecitazioni massime - Involuppi - Travi di fondazione
Scenario di calcolo: ScenarioNT_2018 A2_SLV_SLD_STR_GEO

Asta	N.in. N.fin.	N kN	Ty kN	Tz kN	Mt kN*m	My kN*m	Mz kN*m
9001	1	0	0	89.28 (2)	-11.37 (5-I-4)	-89.88 (5-I-4)	0
	4	0	0	-77.44 (2)	-12.75 (5-I-4)	61.89 (5-I-4)	0
9002	4	0	0	95.46 (5-I-4)	-9.85 (5-II-4)	-43.75 (4-I-3)	0
	5	0	0	-103.48 (2)	-9.55 (5-II-4)	-106.66 (4-II-3)	0
9002	5	0	0	103.48 (2)	9.55 (5-II-2)	-106.66 (4-I-3)	0
	6	0	0	-95.45 (5-I-2)	9.84 (5-II-2)	-43.75 (4-II-3)	0
9003	5	0	0	103.79 (2)	0.77 (4-I-1)	-35.34 (5-II-1)	0
	2	0	0	-115.95 (2)	-0.47 (5-I-4)	-63.84 (5-I-3)	0
9004	2	0	0	96.51 (2)	10.74 (5-I-4)	-106.99 (4-II-1)	0

Asta	N.in.	N	Ty	Tz	Mt	My	Mz
	1	0	0	-84.21 (5-II-4)	11.70 (5-I-4)	-41.15 (4-I-1)	0
9004	3	0	0	84.20 (5-II-2)	-11.69 (5-I-2)	-41.15 (4-II-1)	0
	2	0	0	-96.51 (2)	-10.73 (5-I-2)	-106.99 (4-I-1)	0
9005	6	0	0	77.44 (2)	12.75 (5-I-2)	61.88 (5-I-2)	0
	3	0	0	-89.28 (2)	11.36 (5-I-2)	-89.87 (5-I-2)	0

Tipo diagramma: Sollecitazioni
Combinazione corrente : Scenario ScenarioNT_2018 A2_SLV_SLD_STR_GEO - C 1
Sollecitazione aste: Momento fl.Y - pilastri/pali: Sforzo Normale
Sollecitazione Muri: S I
Sollecitazione Setti: Sxx



Risultati Analisi Dinamica - Sollecitazioni Massime - Muri discretizzati

Scenario di calcolo: **ScenarioNT_2018 A2_SLV_SLD_STR_GEO**

Muro	Pann.	Sxx MPa	Syy MPa	Sxy MPa	Mxx kN	Myy kN	Mxy kN
1	1	-0.13 (5-I-4)	-0.13 (5-II-4)	-0.23 (5-I-4)	-0.27 (2)	-1.21 (5-I-4)	-0.63 (5-II-3)
1	2	-0.36 (4-I-3)	-0.11 (4-I-3)	-0.10 (4-I-3)	-0.48 (5-II-3)	-0.47 (5-II-4)	-0.58 (5-II-2)
1	3	-0.33 (2)	0.08 (5-II-4)	-0.36 (2)	0.12 (4-I-1)	-0.29 (4-II-1)	-0.90 (5-II-2)
1	4	-1.23 (4-I-3)	-0.18 (4-I-3)	-0.19 (2)	-0.20 (5-I-4)	0.14 (5-II-4)	-0.88 (5-II-2)
1	5	-0.36 (2)	0.03 (5-I-4)	-0.13 (4-II-3)	0.31 (2)	0.49 (2)	-0.47 (5-II-2)
1	6	-2.06 (2)	-0.29 (2)	-0.06 (4-II-3)	0.28 (2)	0.10 (2)	-0.43 (5-II-2)
1	7	-0.26 (2)	-0.01 (4-I-1)	0.24 (4-I-3)	0.33 (2)	0.44 (2)	0.83 (5-I-2)
1	8	-1.74 (2)	-0.22 (2)	0.10 (4-I-3)	0.36 (2)	0.14 (2)	0.77 (5-I-2)
1	9	-0.06 (5-II-2)	0.07 (4-I-3)	0.58 (2)	0.20 (4-II-3)	0.46 (4-II-3)	1.52 (2)
1	10	-0.61 (4-II-3)	0.18 (4-I-3)	0.27 (2)	0.25 (4-II-3)	0.09 (4-II-3)	1.39 (2)
1	11	0.15 (3)	-0.22 (4-I-3)	0.44 (4-II-3)	-0.60 (2)	-1.00 (2)	1.01 (4-II-3)
1	12	1.98 (2)	0.39 (2)	0.23 (4-II-3)	-0.64 (2)	-0.23 (2)	0.81 (4-II-3)
2	1	0.15 (3)	-0.22 (4-II-3)	-0.44 (4-I-3)	-0.60 (2)	-1.00 (2)	-1.01 (4-I-3)
2	2	1.98 (2)	0.39 (2)	-0.23 (4-I-3)	-0.64 (2)	-0.23 (2)	-0.81 (4-I-3)
2	3	-0.06 (5-II-4)	0.07 (4-II-3)	-0.58 (2)	0.20 (4-I-3)	0.46 (4-I-3)	-1.52 (2)
2	4	-0.61 (4-II-3)	0.18 (4-II-3)	-0.27 (2)	0.25 (4-I-3)	0.09 (4-I-3)	-1.39 (2)
2	5	-0.26 (2)	-0.01 (4-II-1)	-0.24 (4-II-3)	0.33 (2)	0.44 (2)	-0.83 (5-I-4)
2	6	-1.74 (2)	-0.22 (2)	-0.10 (4-II-3)	0.36 (2)	0.14 (2)	-0.77 (5-I-4)
2	7	-0.36 (2)	0.03 (5-I-2)	0.13 (4-I-3)	0.31 (2)	0.49 (2)	0.47 (5-II-4)
2	8	-2.06 (2)	-0.29 (2)	0.06 (4-I-3)	0.28 (2)	0.10 (2)	0.43 (5-II-4)
2	9	-0.33 (2)	0.08 (5-II-2)	0.36 (2)	0.12 (4-II-1)	-0.29 (4-I-1)	0.91 (5-II-4)
2	10	-1.23 (4-II-3)	-0.18 (4-I-3)	0.19 (2)	-0.20 (5-I-2)	0.15 (5-II-2)	0.88 (5-II-4)
2	11	-0.13 (5-I-2)	-0.13 (5-II-2)	0.23 (5-I-2)	-0.27 (2)	-1.21 (5-I-2)	0.63 (5-II-3)
2	12	-0.36 (4-II-3)	-0.11 (4-II-3)	0.10 (4-II-3)	-0.48 (5-II-3)	-0.47 (5-II-2)	0.58 (5-II-4)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 30 di 103

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
3	1	-0.13(5-II-2)	-0.13(4-I-1)	-0.23(5-II-2)	-0.27(2)	-1.23(5-II-2)	-0.62(5-I-1)
3	2	-0.36(4-II-1)	-0.11(4-II-1)	-0.10(4-II-1)	-0.47(5-I-1)	-0.47(5-I-2)	-0.57(5-I-4)
3	3	-0.33(2)	0.08(5-I-2)	-0.36(2)	0.12(4-II-3)	-0.31(4-I-3)	-0.90(5-I-4)
3	4	-1.24(4-II-1)	-0.17(4-II-1)	-0.19(2)	-0.21(5-II-2)	0.14(5-I-2)	-0.86(5-I-4)
3	5	-0.37(2)	0.03(5-II-2)	-0.14(4-I-1)	0.30(2)	0.49(2)	-0.47(5-I-4)
3	6	-2.07(2)	-0.29(2)	-0.06(4-I-1)	0.28(2)	0.10(2)	-0.43(5-I-4)
3	7	-0.27(2)	-0.01(4-II-3)	0.24(4-II-1)	0.33(2)	0.44(2)	0.81(5-II-4)
3	8	-1.77(2)	-0.22(2)	0.10(4-II-1)	0.36(2)	0.14(2)	0.75(5-II-4)
3	9	-0.07(5-I-4)	0.07(4-II-1)	0.57(2)	0.20(4-I-1)	0.46(4-I-1)	1.51(2)
3	10	-0.66(4-I-1)	0.18(4-II-1)	0.26(2)	0.25(4-I-1)	0.09(4-I-1)	1.38(2)
3	11	0.12(3)	-0.23(4-II-1)	0.44(4-I-1)	-0.59(2)	-1.00(2)	1.02(4-I-1)
3	12	1.90(2)	0.38(2)	0.23(4-I-1)	-0.64(2)	-0.23(2)	0.82(4-I-1)
4	1	0.12(3)	-0.23(4-I-1)	-0.44(4-II-1)	-0.59(2)	-1.00(2)	-1.02(4-II-1)
4	2	1.90(2)	0.38(2)	-0.23(4-II-1)	-0.64(2)	-0.23(2)	-0.82(4-II-1)
4	3	-0.07(5-I-2)	0.07(4-I-1)	-0.57(2)	0.20(4-II-1)	0.46(4-II-1)	-1.51(2)
4	4	-0.66(4-II-1)	0.18(4-I-1)	-0.26(2)	0.25(4-II-1)	0.09(4-II-1)	-1.38(2)
4	5	-0.27(2)	-0.01(4-I-3)	-0.24(4-I-1)	0.33(2)	0.44(2)	-0.81(5-II-2)
4	6	-1.77(2)	-0.22(2)	-0.10(4-I-1)	0.36(2)	0.14(2)	-0.75(5-II-2)
4	7	-0.37(2)	0.03(5-II-4)	0.14(4-II-1)	0.30(2)	0.49(2)	0.47(5-I-2)
4	8	-2.07(2)	-0.29(2)	0.06(4-II-1)	0.28(2)	0.10(2)	0.43(5-I-2)
4	9	-0.33(2)	0.08(5-I-4)	0.36(2)	0.12(4-I-3)	-0.31(4-I-3)	0.90(5-I-2)
4	10	-1.24(4-I-1)	-0.17(4-I-1)	0.19(2)	-0.21(5-II-4)	0.14(5-I-4)	0.86(5-I-2)
4	11	-0.13(5-II-4)	-0.13(4-II-1)	0.23(5-II-4)	-0.27(2)	-1.23(5-II-4)	0.62(5-I-1)
4	12	-0.36(4-I-1)	-0.11(4-I-1)	0.10(4-I-1)	-0.47(5-I-1)	-0.47(5-I-4)	0.57(5-I-2)
5	1	-0.11(5-I-4)	-0.24(5-II-4)	-0.23(5-I-4)	-0.06(5-II-2)	-0.68(5-II-1)	0.43(5-II-4)
5	2	0.79(5-II-4)	0.21(5-II-4)	0.15(5-II-4)	-0.12(4-I-4)	-0.56(5-II-4)	0.43(5-II-4)
5	3	-0.18(5-I-4)	0.04(5-I-4)	-0.23(5-II-4)	-0.20(5-II-4)	-0.60(5-II-4)	-0.19(4-I-1)
5	4	-1.14(5-I-4)	-0.20(5-I-4)	-0.14(5-II-4)	-0.22(5-II-4)	0.11(4-I-2)	-0.19(4-I-1)
5	5	-0.21(3)	-0.04(5-II-4)	-0.22(5-II-4)	0.09(5-I-4)	0.13(4-I-4)	-0.53(5-II-4)
5	6	-0.91(5-I-4)	-0.15(5-I-4)	-0.09(5-II-4)	0.11(5-I-4)	-0.05(5-II-4)	-0.50(5-II-4)
5	7	-0.21(3)	-0.04(5-I-4)	0.21(5-I-4)	0.09(5-II-4)	0.13(4-I-4)	0.55(5-I-4)
5	8	-0.92(5-II-4)	-0.15(5-II-4)	0.09(5-I-4)	0.11(5-II-4)	-0.05(5-I-4)	0.52(5-I-4)
5	9	-0.18(5-II-4)	0.05(5-II-4)	0.23(5-I-4)	-0.20(5-I-4)	-0.60(5-I-4)	0.20(4-I-3)
5	10	-1.15(5-II-4)	-0.20(5-II-4)	0.14(5-I-4)	-0.22(5-I-4)	0.11(4-I-2)	0.20(4-I-3)
5	11	-0.11(5-II-4)	-0.24(5-I-4)	0.23(5-II-4)	-0.06(5-I-2)	-0.66(5-I-3)	-0.42(5-I-4)
5	12	0.79(5-I-4)	0.21(5-I-4)	-0.15(5-I-4)	-0.12(4-I-4)	-0.56(5-I-4)	-0.42(5-I-4)
6	1	0.79(5-II-2)	0.21(5-II-2)	-0.15(5-II-2)	-0.11(4-II-2)	-0.56(5-II-2)	-0.43(5-II-2)
6	2	-0.11(5-I-2)	-0.24(5-II-2)	0.23(5-I-2)	-0.06(5-II-4)	-0.68(5-II-1)	-0.43(5-II-2)
6	3	-1.14(5-I-2)	-0.20(5-I-2)	0.14(5-II-2)	-0.22(5-II-2)	0.11(4-II-4)	0.19(4-II-1)
6	4	-0.18(5-I-2)	0.05(5-I-2)	0.23(5-II-2)	-0.20(5-II-2)	-0.60(5-II-2)	0.19(4-II-1)
6	5	-0.91(5-I-2)	-0.15(5-I-2)	0.09(5-II-2)	0.11(5-I-2)	-0.05(5-II-2)	0.49(5-II-2)
6	6	-0.21(3)	-0.04(5-II-2)	0.22(5-II-2)	0.09(5-I-2)	0.12(4-I-2)	0.53(5-II-2)
6	7	-0.92(5-II-2)	-0.15(5-II-2)	-0.09(5-I-2)	0.11(5-II-2)	-0.05(5-I-2)	-0.52(5-I-2)
6	8	-0.21(3)	-0.04(5-I-2)	-0.21(5-I-2)	0.09(5-II-2)	0.12(4-I-2)	-0.55(5-I-2)
6	9	-1.15(5-II-2)	-0.20(5-II-2)	-0.14(5-I-2)	-0.22(5-I-2)	0.11(4-II-4)	-0.20(4-II-3)
6	10	-0.18(5-II-2)	0.05(5-II-2)	-0.23(5-I-2)	-0.20(5-I-2)	-0.60(5-I-2)	-0.20(4-II-3)
6	11	0.79(5-I-2)	0.21(5-I-2)	0.15(5-I-2)	-0.12(4-II-2)	-0.56(5-I-2)	0.42(5-I-2)
6	12	-0.11(5-II-2)	-0.24(5-I-2)	-0.23(5-II-2)	-0.07(5-I-4)	-0.66(5-I-3)	0.42(5-I-2)
7	1	-0.10(4-II-3)	-1.47(4-I-3)	0.34(4-II-3)	14.28(2)	17.15(4-I-3)	-6.29(4-II-3)
7	2	0.08(4-II-3)	0.34(4-II-3)	0.28(2)	-2.68(4-II-3)	-3.87(4-II-3)	-3.93(5-I-2)
7	3	0.13(2)	0.84(2)	0.08(4-I-3)	-3.36(2)	-8.96(2)	-3.58(5-I-2)
7	4	0.06(4-I-3)	1.06(2)	-0.04(4-II-2)	-3.77(2)	-11.31(2)	-2.40(5-I-2)
7	5	-0.16(4-II-3)	0.74(2)	-0.23(4-II-2)	-1.87(4-I-3)	-8.32(2)	2.56(5-II-2)
7	6	0.08(4-II-3)	-0.49(4-II-3)	-0.16(4-I-3)	8.67(5-II-4)	5.91(4-II-3)	4.25(4-I-3)
7	7	0.08(4-I-3)	-1.38(4-I-3)	0.25(4-II-3)	10.34(2)	15.90(4-I-3)	-6.75(4-II-3)
7	8	0.07(5-I-3)	0.35(4-II-3)	0.20(4-I-3)	-2.12(4-II-3)	-3.84(4-II-3)	-4.91(2)
7	9	0.15(2)	0.87(2)	0.03(4-I-2)	-2.57(2)	-8.93(2)	-3.92(5-I-2)
7	10	0.16(2)	1.09(2)	-0.04(4-II-1)	-2.71(2)	-10.97(2)	-1.73(5-I-2)
7	11	0.08(4-I-3)	0.71(4-I-3)	-0.16(4-II-3)	-1.34(4-I-3)	-7.97(2)	3.20(5-II-2)
7	12	-0.07(5-I-4)	-0.42(4-II-3)	0.12(4-II-3)	7.10(5-II-4)	5.58(4-II-3)	3.26(4-I-3)
7	13	-0.06(4-II-3)	-1.33(4-I-3)	0.15(4-II-3)	6.34(2)	14.42(4-I-3)	-6.61(4-II-3)
7	14	-0.08(2)	0.36(4-II-3)	0.10(4-I-3)	1.29(4-I-3)	-3.72(4-II-3)	-6.29(2)
7	15	-0.04(2)	0.89(2)	-0.03(4-II-1)	-1.93(2)	-8.75(2)	-3.92(5-I-2)
7	16	0.04(2)	1.10(2)	-0.04(2)	-1.65(2)	-10.47(2)	-1.44(5-I-2)
7	17	0.10(5-I-4)	0.71(4-I-3)	-0.07(4-II-2)	-1.26(5-I-4)	-7.50(2)	4.30(5-II-2)
7	18	0.07(5-I-4)	-0.35(4-II-3)	0.11(4-II-4)	4.62(5-II-4)	4.88(4-II-3)	3.10(5-II-2)
7	19	0.07(4-I-3)	-1.34(2)	0.07(4-II-3)	2.98(2)	12.96(4-I-3)	-6.58(4-II-3)
7	20	-0.10(2)	0.39(4-II-3)	-0.07(4-II-3)	1.10(4-I-3)	-3.53(4-II-3)	-6.95(2)
7	21	-0.15(2)	0.93(2)	-0.07(2)	-1.16(2)	-8.47(2)	-3.81(5-I-2)
7	22	-0.06(4-I-3)	1.12(2)	-0.04(2)	-0.66(5-II-4)	-9.96(2)	1.41(5-II-2)
7	23	0.13(2)	0.71(4-I-3)	0.02(5-II-4)	-1.26(5-I-4)	-6.84(2)	4.73(5-II-2)
7	24	0.13(5-I-4)	-0.32(4-II-3)	0.11(2)	-3.28(5-I-4)	4.07(4-II-3)	2.97(5-II-2)
7	25	0.28(2)	-1.38(2)	-0.02(5-II-2)	0.17(4-II-3)	11.60(2)	-6.49(4-II-3)
7	26	-0.12(4-II-3)	0.42(4-II-3)	-0.13(2)	1.11(2)	-3.30(4-II-3)	-7.44(2)
7	27	-0.29(2)	0.98(2)	-0.11(2)	-0.43(5-II-4)	-8.11(2)	-3.70(5-I-2)
7	28	-0.22(2)	1.13(2)	-0.04(4-I-3)	0.50(4-II-3)	-9.43(2)	1.42(5-II-2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 31 di 103

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
7	29	0.12 (4-II-3)	0.71 (4-I-3)	0.06 (2)	-1.17 (4-II-1)	-6.14 (2)	4.78 (5-II-2)
7	30	0.23 (2)	-0.31 (4-II-3)	0.13 (2)	-2.87 (5-I-4)	3.24 (4-II-3)	2.64 (5-II-2)
7	31	0.72 (2)	-1.42 (2)	-0.09 (4-II-3)	-2.53 (2)	10.27 (2)	-6.43 (2)
7	32	0.18 (4-I-3)	0.47 (4-II-3)	-0.22 (2)	1.58 (2)	-3.05 (4-II-3)	-8.28 (2)
7	33	-0.47 (2)	1.02 (2)	-0.13 (2)	0.64 (5-I-4)	-7.66 (2)	-4.16 (2)
7	34	-0.61 (2)	1.13 (2)	-0.05 (4-I-3)	1.32 (2)	-8.80 (2)	1.76 (4-II-4)
7	35	-0.34 (4-I-3)	0.69 (4-I-3)	0.11 (2)	-1.63 (4-II-3)	-5.59 (4-I-3)	5.04 (2)
7	36	0.26 (5-II-3)	-0.32 (4-II-3)	0.11 (2)	-2.77 (5-I-4)	2.42 (4-II-3)	2.54 (4-I-3)
8	1	-0.16 (4-I-1)	0.32 (4-II-3)	0.28 (4-I-3)	6.79 (5-II-2)	8.18 (4-I-3)	-3.54 (5-I-2)
8	2	0.28 (4-II-3)	0.54 (2)	-0.43 (2)	-4.59 (5-I-4)	-6.11 (5-II-4)	3.37 (2)
8	3	0.53 (2)	0.58 (2)	-0.50 (2)	-8.30 (2)	-6.79 (5-II-4)	3.77 (2)
8	4	0.54 (2)	0.43 (2)	-0.35 (2)	-8.85 (2)	-4.35 (5-II-4)	2.80 (2)
8	5	0.33 (2)	-0.42 (4-II-3)	-0.13 (4-I-3)	-6.61 (4-I-3)	3.35 (5-I-4)	0.60 (4-I-3)
8	6	-0.66 (4-II-3)	-0.95 (2)	0.78 (4-II-3)	17.94 (4-II-3)	17.44 (2)	-2.41 (4-II-3)
8	7	-0.09 (4-I-4)	-0.33 (4-I-3)	0.21 (4-I-3)	6.69 (5-II-2)	6.49 (4-I-3)	-3.11 (5-I-2)
8	8	0.37 (4-II-3)	0.52 (2)	-0.32 (2)	-3.55 (4-II-1)	-7.01 (2)	3.48 (2)
8	9	0.59 (2)	0.65 (2)	-0.47 (2)	-7.06 (2)	-6.61 (2)	4.13 (2)
8	10	0.53 (2)	0.49 (2)	-0.36 (2)	-9.23 (2)	-3.29 (5-II-4)	3.18 (2)
8	11	0.23 (2)	-0.32 (4-II-3)	-0.15 (4-I-3)	-6.18 (2)	4.72 (4-II-1)	0.86 (4-I-3)
8	12	-0.65 (4-II-3)	-0.84 (2)	0.73 (4-II-3)	13.70 (4-II-3)	17.01 (2)	-3.39 (4-II-3)
8	13	0.18 (4-I-3)	-0.29 (4-I-3)	0.17 (4-I-3)	6.39 (5-II-2)	4.58 (4-I-3)	-2.26 (5-I-2)
8	14	0.39 (4-II-3)	0.44 (2)	-0.31 (4-II-3)	-2.22 (4-II-1)	-7.91 (2)	3.37 (2)
8	15	0.54 (2)	0.61 (2)	-0.53 (2)	-6.09 (2)	-6.03 (2)	4.41 (2)
8	16	0.40 (2)	0.45 (2)	-0.47 (2)	-8.95 (2)	-2.80 (5-II-4)	3.41 (2)
8	17	0.13 (4-I-3)	-0.28 (4-II-3)	-0.21 (4-I-3)	-7.22 (2)	5.92 (4-II-1)	1.34 (4-I-3)
8	18	-0.66 (4-II-3)	-0.79 (2)	0.67 (4-II-3)	9.20 (4-II-3)	15.94 (2)	-4.37 (4-II-3)
8	19	0.25 (4-II-3)	-0.24 (4-I-3)	0.18 (4-I-3)	5.44 (5-II-2)	-3.44 (4-II-3)	-1.91 (4-I-1)
8	20	0.40 (4-II-3)	0.38 (4-II-3)	-0.33 (4-II-3)	2.25 (5-II-3)	-8.03 (2)	3.11 (4-II-3)
8	21	0.50 (2)	0.57 (2)	-0.58 (2)	-5.10 (2)	-5.47 (2)	4.68 (2)
8	22	0.32 (2)	0.46 (2)	-0.54 (2)	-8.36 (2)	-2.41 (5-II-4)	3.65 (2)
8	23	-0.16 (4-I-3)	0.22 (4-I-3)	-0.24 (4-I-3)	-7.59 (2)	6.36 (4-II-1)	1.68 (4-I-3)
8	24	-0.63 (4-II-3)	-0.68 (2)	0.70 (2)	6.23 (4-II-3)	14.20 (2)	-5.13 (4-II-3)
8	25	0.30 (4-II-3)	-0.19 (4-I-3)	0.21 (4-I-3)	4.26 (5-II-2)	-3.26 (4-II-3)	-1.83 (4-I-2)
8	26	0.40 (2)	0.31 (4-II-3)	-0.37 (4-II-3)	2.52 (5-II-3)	-7.95 (2)	3.09 (4-II-3)
8	27	0.42 (2)	0.49 (2)	-0.67 (2)	-4.19 (4-II-1)	-4.97 (2)	4.92 (2)
8	28	0.24 (2)	0.45 (2)	-0.63 (2)	-7.82 (2)	-1.97 (4-I-1)	3.91 (2)
8	29	-0.21 (4-II-3)	0.26 (4-I-3)	-0.27 (4-I-3)	-7.80 (2)	7.08 (2)	1.97 (4-I-3)
8	30	-0.57 (2)	-0.53 (2)	0.83 (2)	-4.45 (4-I-3)	12.22 (2)	-5.77 (2)
8	31	0.21 (4-II-3)	-0.15 (4-I-3)	0.24 (4-I-3)	3.07 (5-II-2)	-3.69 (4-II-3)	-1.71 (4-I-3)
8	32	0.24 (2)	0.14 (4-II-3)	-0.51 (4-II-3)	2.47 (5-II-2)	-8.18 (2)	3.02 (4-II-3)
8	33	0.23 (2)	0.29 (2)	-0.87 (2)	-3.63 (4-II-3)	-4.55 (2)	5.06 (2)
8	34	0.15 (2)	0.40 (2)	-0.74 (2)	-7.71 (2)	2.09 (4-II-3)	4.11 (2)
8	35	-0.18 (4-II-3)	0.32 (2)	-0.30 (4-I-3)	-8.33 (2)	8.24 (2)	2.23 (4-I-3)
8	36	-0.42 (2)	-0.36 (4-II-3)	1.07 (2)	-5.07 (4-I-3)	10.30 (2)	-6.40 (2)
9	1	-0.76 (5-II-2)	0.29 (2)	0.04 (3)	5.35 (5-II-2)	-0.88 (4-I-1)	-3.25 (5-II-2)
9	2	-0.78 (5-II-2)	0.11 (5-I-1)	0.04 (5-II-2)	6.51 (5-II-2)	1.43 (4-II-1)	-3.96 (5-II-2)
9	3	-0.80 (5-II-2)	0.08 (5-I-2)	0.09 (5-II-2)	7.84 (5-II-2)	2.58 (4-II-1)	-4.47 (5-II-2)
9	4	-0.86 (5-II-2)	-0.06 (5-II-2)	0.14 (5-II-2)	9.35 (5-II-2)	3.96 (4-II-1)	-5.23 (5-II-2)
9	5	-0.97 (5-II-2)	-0.17 (5-I-1)	0.21 (5-II-2)	10.99 (5-II-2)	5.62 (4-II-1)	-6.96 (5-II-2)
9	6	-1.08 (5-II-2)	0.12 (5-II-2)	0.23 (5-II-2)	12.37 (5-II-2)	6.85 (4-II-1)	-8.93 (5-II-2)
9	7	0.73 (5-I-2)	0.38 (5-II-2)	0.08 (5-II-2)	-5.05 (5-I-2)	-2.58 (5-II-2)	2.51 (5-II-2)
9	8	0.69 (5-I-2)	0.16 (5-II-2)	0.04 (3)	-5.39 (5-I-2)	-1.50 (5-II-2)	2.38 (5-II-2)
9	9	0.67 (5-I-2)	0.09 (5-II-2)	0.03 (5-I-2)	-5.61 (5-I-2)	-0.41 (5-II-4)	2.54 (5-II-2)
9	10	0.65 (5-I-2)	0.05 (4-I-2)	-0.09 (5-II-2)	-5.71 (5-I-2)	0.76 (5-II-2)	2.53 (5-II-2)
9	11	0.61 (5-I-2)	-0.12 (5-II-2)	-0.19 (5-II-2)	-5.72 (5-I-2)	1.75 (5-II-2)	-2.00 (5-I-2)
9	12	0.59 (5-I-2)	-0.19 (5-II-2)	-0.24 (5-II-2)	-5.83 (5-I-2)	2.26 (5-II-2)	-0.85 (5-II-2)
9	13	0.45 (5-I-2)	0.10 (5-II-2)	0.07 (5-II-2)	-3.68 (5-I-2)	0.84 (5-II-2)	3.12 (5-II-2)
9	14	0.43 (5-I-2)	-0.11 (5-I-2)	0.04 (5-II-2)	-3.86 (5-I-2)	0.57 (5-II-2)	2.57 (5-II-2)
9	15	0.42 (5-I-2)	-0.06 (5-I-2)	0.01 (5-II-2)	-3.96 (5-I-2)	-0.53 (5-I-2)	2.33 (5-II-2)
9	16	0.40 (5-I-2)	0.02 (4-I-3)	-0.01 (5-II-2)	-3.99 (5-I-2)	-0.56 (4-II-2)	2.22 (5-II-2)
9	17	0.38 (5-I-2)	-0.06 (2)	-0.03 (5-II-2)	-3.94 (5-I-2)	-0.65 (4-II-2)	2.22 (5-II-2)
9	18	0.38 (5-I-2)	0.07 (5-I-2)	-0.06 (5-II-2)	-3.90 (5-I-2)	-0.81 (5-II-2)	-1.81 (5-I-2)
9	19	0.46 (5-II-2)	0.10 (5-I-2)	-0.07 (5-I-2)	-3.71 (5-II-2)	0.84 (5-I-2)	-3.15 (5-I-2)
9	20	0.43 (5-II-2)	-0.11 (5-II-2)	-0.04 (5-I-2)	-3.90 (5-II-2)	0.57 (5-I-2)	-2.65 (5-I-2)
9	21	0.42 (5-II-2)	-0.06 (5-II-2)	-0.01 (5-I-2)	-3.99 (5-II-2)	-0.54 (5-II-2)	-2.42 (5-I-2)
9	22	0.41 (5-II-2)	0.03 (4-I-1)	0.01 (5-I-2)	-4.03 (5-II-2)	-0.56 (4-II-2)	-2.32 (5-I-2)
9	23	0.39 (5-II-2)	-0.06 (2)	0.03 (5-I-2)	-3.98 (5-II-2)	-0.65 (4-II-2)	-2.33 (5-I-2)
9	24	0.39 (5-II-2)	0.07 (5-II-2)	0.07 (5-I-2)	-3.93 (5-II-2)	-0.81 (5-I-2)	1.67 (5-II-2)
9	25	0.73 (5-II-2)	0.38 (5-I-2)	-0.08 (5-I-2)	-5.10 (5-II-2)	-2.57 (5-I-2)	-2.55 (5-I-2)
9	26	0.70 (5-II-2)	0.17 (5-I-2)	-0.04 (3)	-5.44 (5-II-2)	-1.49 (5-I-2)	-2.46 (5-I-2)
9	27	0.68 (5-II-2)	0.09 (5-I-2)	-0.03 (5-II-2)	-5.66 (5-II-2)	-0.40 (5-I-4)	-2.64 (5-I-2)
9	28	0.66 (5-II-2)	0.05 (4-I-2)	0.09 (5-I-2)	-5.76 (5-II-2)	0.77 (5-I-2)	-2.64 (5-I-2)
9	29	0.62 (5-II-2)	-0.12 (5-I-2)	0.19 (5-I-2)	-5.76 (5-II-2)	1.76 (5-I-2)	-1.90 (5-I-2)
9	30	0.60 (5-II-2)	-0.19 (5-I-2)	0.24 (5-I-2)	-5.88 (5-II-2)	2.27 (5-I-2)	0.73 (5-I-2)
9	31	-0.76 (5-I-2)	0.29 (2)	-0.04 (3)	5.37 (5-I-2)	-0.83 (4-I-3)	3.21 (5-I-2)
9	32	-0.78 (5-I-2)	0.11 (5-II-3)	-0.04 (5-I-2)	6.53 (5-I-2)	1.42 (4-II-3)	3.88 (5-I-2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 32 di 103

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
9	33	-0.81 (5-I-2)	0.08 (5-II-2)	-0.09 (5-I-2)	7.86 (5-I-2)	2.56 (4-II-3)	4.38 (5-I-2)
9	34	-0.86 (5-I-2)	-0.06 (5-I-2)	-0.14 (5-I-2)	9.37 (5-I-2)	3.93 (4-II-3)	5.14 (5-I-2)
9	35	-0.97 (5-I-2)	-0.17 (5-II-3)	-0.21 (5-I-2)	11.02 (5-I-2)	5.58 (4-II-3)	6.87 (5-I-2)
9	36	-1.09 (5-I-2)	0.13 (5-I-2)	-0.23 (5-I-2)	12.40 (5-I-2)	6.80 (4-II-3)	8.84 (5-I-2)
10	1	-1.39 (2)	0.71 (2)	0.09 (4-I-1)	9.97 (2)	-2.51 (2)	6.42 (4-I-1)
10	2	-1.35 (2)	0.27 (2)	0.02 (5-I-4)	11.36 (4-II-1)	0.16 (4-I-1)	6.54 (4-I-1)
10	3	-1.31 (2)	0.07 (4-II-1)	-0.07 (4-I-1)	12.79 (4-II-1)	2.94 (2)	6.65 (4-I-1)
10	4	-1.31 (4-II-1)	-0.06 (4-I-1)	-0.16 (4-I-1)	14.25 (4-II-1)	6.26 (2)	6.70 (4-I-1)
10	5	-1.36 (4-II-1)	0.08 (4-II-1)	-0.25 (4-I-1)	15.74 (4-II-1)	10.22 (2)	6.86 (4-I-1)
10	6	-1.46 (4-II-1)	-0.10 (4-I-1)	-0.34 (4-I-1)	17.00 (4-II-1)	14.13 (2)	6.43 (4-I-1)
10	7	0.49 (4-I-1)	0.18 (4-II-1)	0.21 (2)	-3.21 (4-I-1)	1.57 (2)	8.20 (2)
10	8	0.44 (4-I-1)	-0.12 (4-I-1)	0.13 (2)	-3.47 (4-I-1)	1.11 (2)	7.38 (2)
10	9	0.41 (4-I-1)	-0.10 (2)	0.07 (4-I-1)	-3.70 (4-I-1)	1.10 (4-II-1)	6.90 (2)
10	10	0.38 (4-I-1)	-0.08 (2)	-0.10 (4-II-1)	-3.89 (4-I-1)	1.30 (4-II-1)	6.25 (2)
10	11	0.37 (4-I-1)	0.07 (5-II-1)	-0.20 (4-II-1)	-4.02 (4-I-1)	-2.15 (4-I-1)	4.88 (2)
10	12	0.36 (4-I-1)	0.09 (4-I-1)	-0.28 (2)	-4.06 (4-I-1)	-2.72 (4-I-1)	3.90 (5-II-4)
10	13	1.03 (2)	-0.47 (2)	0.12 (2)	-7.78 (2)	0.64 (5-II-2)	4.06 (2)
10	14	0.99 (2)	-0.29 (2)	0.10 (2)	-8.24 (2)	-0.43 (5-I-2)	3.62 (5-II-4)
10	15	0.94 (2)	-0.15 (2)	0.07 (2)	-8.59 (2)	-1.16 (2)	3.74 (5-II-4)
10	16	0.91 (2)	-0.04 (2)	0.03 (4-I-3)	-8.87 (2)	-1.93 (2)	3.86 (5-II-4)
10	17	0.88 (2)	0.15 (2)	-0.03 (4-II-4)	-9.06 (2)	-2.57 (2)	3.87 (5-II-4)
10	18	0.85 (2)	0.13 (2)	-0.08 (4-II-1)	-9.09 (2)	-3.35 (2)	3.53 (5-II-4)
10	19	1.13 (2)	-0.60 (2)	0.05 (4-II-1)	-8.83 (2)	1.33 (2)	-1.81 (4-I-2)
10	20	1.13 (2)	-0.22 (2)	0.04 (4-II-1)	-9.46 (2)	0.51 (4-I-1)	-1.43 (5-I-4)
10	21	1.12 (2)	-0.06 (4-II-1)	0.04 (2)	-9.99 (2)	-0.65 (5-I-2)	-1.41 (5-I-4)
10	22	1.10 (2)	0.04 (2)	0.04 (2)	-10.50 (2)	-1.64 (2)	1.38 (5-II-4)
10	23	1.10 (2)	0.16 (2)	0.04 (4-I-3)	-11.01 (2)	-2.71 (2)	1.68 (5-II-4)
10	24	1.06 (2)	0.06 (4-II-1)	0.04 (4-I-4)	-11.35 (2)	-3.77 (2)	2.37 (5-II-4)
10	25	0.69 (4-II-1)	-0.33 (4-II-1)	-0.11 (2)	-5.59 (4-II-1)	-1.69 (4-I-1)	-5.08 (2)
10	26	0.71 (4-II-1)	0.12 (4-I-1)	-0.06 (2)	-6.12 (4-II-1)	-1.22 (4-I-3)	-4.77 (5-I-4)
10	27	0.71 (4-I-1)	0.13 (2)	-0.02 (5-I-2)	-6.78 (2)	-1.27 (5-II-2)	-4.72 (5-I-4)
10	28	0.71 (4-II-1)	0.10 (5-II-2)	0.07 (4-I-4)	-7.44 (2)	-1.25 (5-II-2)	-4.30 (5-I-4)
10	29	0.71 (4-II-1)	0.08 (4-II-1)	0.16 (4-I-1)	-7.92 (2)	-1.32 (4-II-1)	-3.20 (5-I-4)
10	30	0.73 (2)	-0.16 (4-I-1)	0.24 (4-I-4)	-8.27 (2)	-1.86 (4-II-1)	-2.53 (5-I-4)
10	31	-0.33 (4-I-1)	0.26 (5-I-1)	-0.11 (2)	2.49 (4-I-1)	-2.78 (5-II-2)	-2.54 (4-II-1)
10	32	-0.32 (4-I-1)	0.22 (2)	-0.13 (2)	3.33 (4-I-1)	-2.88 (5-II-2)	-2.57 (5-I-4)
10	33	-0.33 (4-I-1)	0.13 (5-II-2)	-0.11 (2)	4.18 (4-I-1)	-3.28 (5-II-2)	-2.90 (5-I-4)
10	34	-0.37 (4-I-1)	0.07 (5-II-2)	-0.11 (4-I-2)	5.02 (4-I-1)	4.56 (5-I-2)	-3.03 (5-I-4)
10	35	-0.43 (4-I-1)	-0.07 (5-II-2)	-0.12 (4-I-1)	5.75 (4-I-1)	7.02 (5-I-2)	-3.27 (4-II-1)
10	36	-0.50 (4-I-1)	0.08 (4-I-1)	0.15 (4-II-1)	6.11 (4-I-1)	8.58 (5-I-2)	-4.26 (4-II-1)
11	1	-0.33 (4-II-1)	0.26 (5-I-1)	0.11 (2)	2.49 (4-II-1)	-2.78 (5-II-2)	2.54 (4-I-1)
11	2	-0.32 (4-II-1)	0.22 (2)	0.13 (2)	3.33 (4-II-1)	-2.87 (5-II-4)	2.57 (5-I-2)
11	3	-0.33 (4-II-1)	0.13 (5-II-4)	0.11 (2)	4.18 (4-II-1)	-3.28 (5-II-4)	2.90 (5-I-2)
11	4	-0.37 (4-II-1)	0.07 (5-II-4)	0.11 (4-II-4)	5.02 (4-II-1)	4.56 (5-I-4)	3.02 (5-I-2)
11	5	-0.43 (4-II-1)	-0.07 (5-II-4)	0.12 (4-II-1)	5.75 (4-II-1)	7.02 (5-I-4)	3.27 (4-I-1)
11	6	-0.50 (4-II-1)	0.08 (4-II-1)	-0.15 (4-I-1)	6.11 (4-II-1)	8.57 (5-I-4)	4.26 (4-I-1)
11	7	0.69 (4-I-1)	-0.33 (4-I-1)	0.11 (2)	-5.59 (4-I-1)	-1.69 (4-II-1)	5.08 (2)
11	8	0.71 (4-I-1)	0.12 (4-II-1)	0.06 (2)	-6.12 (4-I-1)	-1.22 (4-II-3)	4.77 (5-I-2)
11	9	0.71 (4-I-1)	0.13 (2)	0.02 (5-I-4)	-6.78 (2)	-1.27 (5-II-4)	4.71 (5-I-2)
11	10	0.71 (4-I-1)	0.10 (5-II-4)	-0.07 (4-II-2)	-7.44 (2)	-1.24 (5-II-4)	4.29 (5-I-2)
11	11	0.71 (4-I-1)	0.08 (4-I-1)	-0.16 (4-II-1)	-7.92 (2)	-1.32 (4-I-1)	3.19 (5-I-2)
11	12	0.73 (2)	-0.16 (4-II-1)	-0.24 (4-II-2)	-8.27 (2)	-1.86 (4-I-1)	2.53 (5-I-2)
11	13	1.13 (2)	-0.60 (2)	-0.05 (4-I-1)	-8.83 (2)	1.33 (2)	1.81 (4-II-4)
11	14	1.13 (2)	-0.22 (2)	-0.04 (4-I-1)	-9.46 (2)	0.51 (4-II-1)	1.43 (5-I-2)
11	15	1.12 (2)	-0.06 (4-I-1)	-0.04 (2)	-9.99 (2)	-0.65 (5-I-4)	1.41 (5-I-2)
11	16	1.10 (2)	0.04 (2)	-0.04 (2)	-10.50 (2)	-1.64 (2)	-1.38 (5-II-2)
11	17	1.10 (2)	0.16 (2)	-0.04 (4-II-3)	-11.01 (2)	-2.71 (2)	-1.68 (5-II-2)
11	18	1.06 (2)	0.06 (4-I-1)	-0.04 (4-II-2)	-11.35 (2)	-3.77 (2)	-2.37 (5-II-2)
11	19	1.03 (2)	-0.47 (2)	-0.12 (2)	-7.78 (2)	0.65 (5-II-4)	-4.06 (2)
11	20	0.99 (2)	-0.29 (2)	-0.10 (2)	-8.24 (2)	-0.43 (5-I-4)	-3.62 (5-II-2)
11	21	0.94 (2)	-0.15 (2)	-0.07 (2)	-8.59 (2)	-1.16 (2)	-3.74 (5-II-2)
11	22	0.91 (2)	-0.04 (2)	-0.03 (4-II-3)	-8.87 (2)	-1.93 (2)	-3.86 (5-II-2)
11	23	0.88 (2)	0.15 (2)	0.03 (4-I-2)	-9.06 (2)	-2.57 (2)	-3.86 (5-II-2)
11	24	0.85 (2)	0.13 (2)	0.08 (4-I-1)	-9.09 (2)	-3.35 (2)	-3.53 (5-II-2)
11	25	0.49 (4-II-1)	0.18 (4-I-1)	-0.21 (2)	-3.21 (4-II-1)	1.57 (2)	-8.20 (2)
11	26	0.44 (4-II-1)	-0.12 (4-II-1)	-0.13 (2)	-3.47 (4-II-1)	1.11 (2)	-7.38 (2)
11	27	0.41 (4-II-1)	-0.10 (2)	-0.07 (4-II-1)	-3.70 (4-II-1)	1.10 (4-I-1)	-6.90 (2)
11	28	0.38 (4-II-1)	-0.08 (2)	0.10 (4-I-1)	-3.89 (4-II-1)	1.30 (4-I-1)	-6.25 (2)
11	29	0.37 (4-II-1)	0.07 (5-II-1)	0.20 (4-I-1)	-4.02 (4-II-1)	-2.15 (4-II-1)	-4.88 (2)
11	30	0.36 (4-II-1)	0.09 (4-II-1)	0.28 (2)	-4.06 (4-II-1)	-2.72 (4-II-1)	-3.90 (5-II-2)
11	31	-1.39 (2)	0.71 (2)	-0.09 (4-I-1)	9.97 (2)	-2.51 (2)	-6.42 (4-II-1)
11	32	-1.35 (2)	0.27 (2)	-0.02 (5-I-2)	11.36 (4-I-1)	0.16 (4-II-1)	-6.54 (4-II-1)
11	33	-1.31 (2)	0.07 (4-I-1)	0.07 (4-II-1)	12.79 (4-I-1)	2.94 (2)	-6.65 (4-II-1)
11	34	-1.31 (4-I-1)	-0.06 (4-II-1)	0.16 (4-II-1)	14.25 (4-I-1)	6.26 (2)	-6.70 (4-II-1)
11	35	-1.36 (4-I-1)	0.08 (4-I-1)	0.25 (4-II-1)	15.74 (4-I-1)	10.22 (2)	-6.86 (4-II-1)
11	36	-1.46 (4-I-1)	-0.10 (4-II-1)	0.34 (4-II-1)	17.00 (4-I-1)	14.13 (2)	-6.43 (4-II-1)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 33 di 103

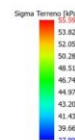
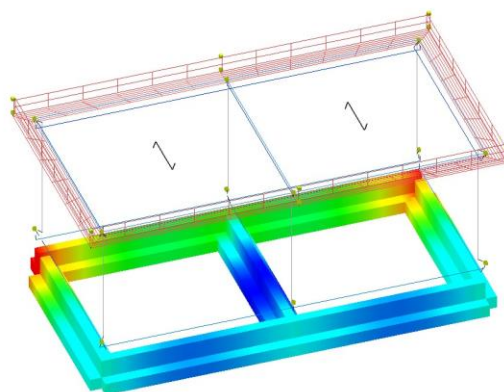
Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
12	1	0.27 (5-I-4)	-0.28 (5-II-4)	-0.51 (5-II-4)	1.56 (5-I-1)	5.88 (5-II-4)	2.71 (5-II-4)
12	2	0.30 (5-I-4)	0.28 (5-I-4)	-0.53 (5-II-4)	2.94 (5-II-4)	-2.87 (3)	-3.33 (5-I-4)
12	3	0.19 (3)	0.23 (5-I-4)	0.27 (5-I-4)	-4.11 (5-I-4)	-3.02 (5-II-4)	-1.71 (5-I-4)
12	4	0.23 (5-II-4)	0.19 (3)	0.28 (5-II-4)	-3.04 (5-I-4)	-4.09 (5-II-4)	-1.72 (5-II-4)
12	5	0.28 (5-II-4)	0.30 (5-II-4)	-0.54 (5-I-4)	-2.93 (3)	2.99 (5-I-4)	-3.36 (5-II-4)
12	6	-0.28 (5-I-4)	0.27 (5-II-4)	-0.51 (5-I-4)	5.87 (5-I-4)	1.64 (5-II-3)	2.71 (5-I-4)
12	7	-0.33 (5-II-4)	-0.42 (5-II-4)	-0.40 (5-II-4)	1.83 (4-I-1)	7.49 (5-II-4)	2.97 (5-II-4)
12	8	0.31 (5-I-4)	-0.28 (5-II-4)	-0.41 (5-II-4)	3.36 (5-II-4)	-2.15 (3)	-3.18 (5-I-4)
12	9	0.13 (5-I-4)	0.19 (5-I-4)	0.27 (5-I-4)	-4.29 (5-I-4)	-2.65 (5-II-4)	-1.71 (5-I-4)
12	10	0.19 (5-II-4)	0.13 (5-II-4)	0.27 (5-II-4)	-2.71 (5-I-4)	-4.22 (5-II-4)	-1.73 (5-II-4)
12	11	-0.28 (5-I-4)	0.32 (5-II-4)	-0.41 (5-I-4)	-2.27 (3)	3.46 (5-I-4)	-3.21 (5-II-4)
12	12	-0.42 (5-I-4)	-0.34 (5-I-4)	-0.40 (5-I-4)	7.45 (5-I-4)	1.87 (4-I-3)	2.97 (5-I-4)
12	13	-0.34 (5-II-4)	-0.52 (5-II-4)	-0.38 (5-II-4)	2.53 (4-I-1)	9.28 (5-II-4)	3.03 (5-II-4)
12	14	0.36 (5-I-4)	0.29 (5-I-4)	0.35 (5-I-4)	4.05 (5-II-4)	-1.83 (3)	-2.94 (5-I-4)
12	15	0.17 (5-I-4)	0.19 (5-I-4)	0.24 (5-I-4)	-4.31 (5-I-4)	-2.60 (5-II-4)	-1.71 (5-I-4)
12	16	0.19 (5-II-4)	0.17 (5-II-4)	0.24 (5-II-4)	-2.68 (5-I-4)	-4.23 (5-II-4)	-1.73 (5-II-4)
12	17	0.30 (5-II-4)	0.36 (5-II-4)	0.35 (5-II-4)	-1.97 (3)	4.17 (5-I-4)	-2.97 (5-II-4)
12	18	-0.52 (5-I-4)	-0.34 (5-I-4)	-0.38 (5-I-4)	9.22 (5-I-4)	2.57 (4-I-3)	3.02 (5-I-4)
12	19	-0.31 (5-II-4)	-0.60 (5-II-4)	-0.40 (5-II-4)	3.17 (4-I-1)	11.51 (5-II-4)	3.08 (5-II-4)
12	20	0.40 (5-I-4)	0.29 (5-I-4)	0.31 (5-I-4)	-4.60 (5-I-4)	-1.65 (5-I-4)	-2.60 (5-I-4)
12	21	0.21 (5-I-4)	0.19 (5-I-4)	0.20 (5-I-4)	-4.24 (5-I-4)	-2.71 (5-II-4)	-1.75 (5-I-4)
12	22	0.20 (5-II-4)	0.22 (5-II-4)	0.20 (5-II-4)	-2.81 (5-I-4)	-4.15 (5-II-4)	-1.76 (5-II-4)
12	23	0.29 (5-II-4)	0.41 (5-II-4)	0.31 (5-II-4)	-1.78 (5-II-4)	4.69 (5-I-4)	-2.62 (5-II-4)
12	24	-0.60 (5-I-4)	-0.31 (5-I-4)	-0.40 (5-I-4)	11.45 (5-I-4)	3.22 (4-I-3)	3.07 (5-I-4)
12	25	-0.29 (5-II-4)	-0.71 (5-II-4)	-0.47 (5-II-4)	3.41 (4-I-1)	14.77 (5-II-4)	3.19 (5-II-4)
12	26	-0.50 (5-II-4)	0.21 (5-I-4)	0.31 (5-I-4)	-5.52 (5-I-4)	-1.52 (5-I-4)	-2.20 (5-I-4)
12	27	0.20 (5-I-4)	0.14 (5-I-4)	0.21 (5-I-4)	-4.25 (5-I-4)	-2.97 (5-II-4)	-1.79 (5-I-4)
12	28	0.15 (5-II-4)	0.20 (5-II-4)	0.21 (5-II-4)	-3.07 (5-I-4)	-4.15 (5-II-4)	-1.80 (5-II-4)
12	29	0.22 (5-II-4)	-0.50 (5-I-4)	0.31 (5-II-4)	-1.66 (5-II-4)	-5.43 (5-II-4)	-2.22 (5-II-4)
12	30	-0.71 (5-I-4)	-0.29 (5-I-4)	-0.47 (5-I-4)	14.73 (5-I-4)	3.47 (4-I-3)	3.16 (5-I-4)
12	31	-0.25 (5-II-4)	-0.71 (5-II-4)	-0.60 (5-II-4)	3.75 (4-I-2)	17.94 (5-II-4)	-3.72 (5-I-4)
12	32	-0.54 (5-II-4)	0.26 (5-I-4)	0.22 (5-I-4)	-4.04 (5-I-4)	3.78 (5-II-4)	-2.07 (5-I-4)
12	33	0.28 (5-I-4)	0.18 (3)	0.16 (5-I-4)	-3.87 (5-I-4)	-2.38 (5-II-4)	-1.83 (5-I-4)
12	34	0.18 (5-II-4)	0.28 (5-II-4)	0.16 (5-II-4)	-2.50 (5-I-4)	-3.75 (5-II-4)	-1.85 (5-II-4)
12	35	0.27 (5-II-4)	-0.54 (5-I-4)	0.22 (5-II-4)	3.67 (5-I-4)	-3.92 (5-II-4)	-2.09 (5-II-4)
12	36	-0.71 (5-I-4)	-0.25 (5-I-4)	-0.61 (5-I-4)	17.91 (5-I-4)	3.82 (4-I-2)	-3.76 (5-II-4)

Risultati Analisi Dinamica - Massime tensioni sul terreno aste per combinazione - S.L.E.

Scenario di calcolo: **ScenarioNT_2018 A2_SLV_SLD_STR_GEO**

Combinazione	Asta	N.in.	N.fin.	SigmaMax kPa	SigmaMin
6	9002	5	6	52.7	39.2
7	9002	5	6	52.6	38.5
8	9002	5	6	52.3	38.2
9-I-1	9002	5	6	55.3	37.9
9-I-2	9002	5	6	54.9	37.9
9-I-3	9002	5	6	54.4	37.9
9-I-4	9002	5	6	54.8	37.9
9-II-1	9002	4	5	55.3	37.9
9-II-2	9002	4	5	54.8	37.9
9-II-3	9002	4	5	54.4	37.9
9-II-4	9002	4	5	54.9	37.9
10-I-1	9002	4	5	58.0	37.9
10-I-2	9002	5	6	58.8	38.0
10-I-3	9002	5	6	58.1	38.0
10-I-4	9002	4	5	58.9	38.0
10-II-1	9004	3	2	53.9	38.0
10-II-2	9004	3	2	54.5	38.0
10-II-3	9004	2	1	53.8	38.0
10-II-4	9004	2	1	54.5	38.0

Tipo diagramma: Tensioni medie terreno
Combinazione corrente : Scenario ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO - C 10-I
Posizione masse N° 1
Tensioni medie terreno aste
Tensioni medie terreno piatte



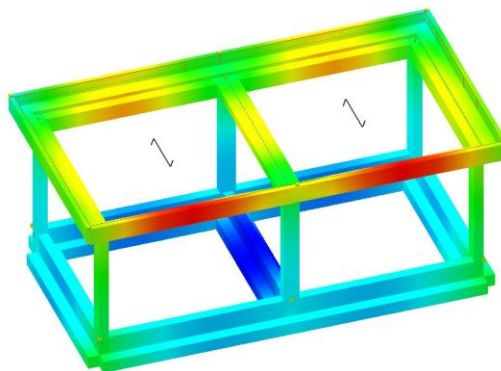
Risultati Analisi Dinamica - Spostamenti massimi - Nodi - S.L.E.

Scenario di calcolo: **ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO**

la tripletta (Cb [-SubC-Cbm]) indica la Combinazione - SottoCombinazione sismica - Posizione Masse, nel caso non sismico mancano SubC-Cbm

Nodo	Trasl. X mm	Trasl. Y mm	Trasl. Z mm	Rotaz. X °	Rotaz. Y °	Rotaz. Z °
1	0.00 (6)	0.00 (6)	-1.77 (10-II-4)	0.01 (10-II-4)	-0.01 (10-II-4)	0.00 (6)
2	0.00 (6)	0.00 (6)	-1.53 (10-II-1)	0.01 (10-II-1)	0.00 (9-I-3)	0.00 (6)
3	0.00 (6)	0.00 (6)	-1.77 (10-II-2)	0.01 (10-II-2)	0.01 (10-II-2)	0.00 (6)
4	0.00 (6)	0.00 (6)	-1.90 (10-I-4)	-0.01 (10-I-4)	-0.01 (10-I-4)	0.00 (6)
5	0.00 (6)	0.00 (6)	-1.59 (10-I-3)	-0.01 (10-I-3)	0.00 (9-I-1)	0.00 (6)
6	0.00 (6)	0.00 (6)	-1.90 (10-I-2)	-0.01 (10-I-2)	0.01 (10-I-2)	0.00 (6)
101	1.00 (9-I-1)	1.23 (10-I-4)	-1.74 (10-II-4)	-0.01 (10-I-4)	0.01 (9-I-3)	0.00 (10-II-4)
102	1.00 (9-I-1)	1.06 (10-I-1)	-1.58 (10-II-1)	0.02 (10-II-1)	-0.00 (9-II-1)	-0.00 (10-I-4)
103	-1.00 (9-II-1)	1.23 (10-I-2)	-1.74 (10-II-2)	-0.01 (10-I-2)	-0.01 (9-II-3)	-0.00 (10-I-4)
104	1.00 (9-I-3)	1.23 (10-I-4)	-1.87 (10-I-4)	0.01 (10-II-4)	0.01 (9-I-1)	-0.00 (10-I-4)
105	1.00 (9-I-3)	1.06 (10-I-1)	-1.64 (10-I-3)	-0.02 (10-I-3)	0.00 (9-I-3)	-0.00 (10-I-4)
106	-1.00 (9-II-3)	1.23 (10-I-2)	-1.87 (10-I-2)	0.01 (10-II-2)	-0.01 (9-II-1)	0.00 (10-II-4)
107	-1.02 (9-II-1)	1.24 (10-I-4)	-1.69 (10-II-4)	-0.01 (10-I-4)	0.01 (9-I-3)	0.00 (10-II-4)
108	1.01 (9-I-1)	1.06 (10-I-1)	-1.75 (10-II-1)	0.02 (10-II-1)	-0.00 (9-II-3)	-0.00 (10-I-4)
109	1.02 (9-I-1)	1.24 (10-I-2)	-1.69 (10-II-2)	-0.01 (10-I-2)	-0.01 (9-II-3)	-0.00 (10-II-2)
110	-1.01 (9-II-3)	1.23 (10-I-4)	-1.84 (10-I-4)	0.01 (10-II-4)	0.01 (9-I-1)	-0.00 (10-I-4)
111	1.00 (9-I-3)	1.07 (10-I-1)	-1.83 (10-I-3)	-0.02 (10-I-3)	0.00 (9-I-1)	-0.00 (10-I-4)
112	1.01 (9-I-3)	1.23 (10-I-2)	-1.84 (10-I-2)	0.01 (10-II-2)	-0.01 (9-II-1)	0.00 (10-I-2)
207	1.13 (9-I-1)	1.34 (10-I-4)	-1.68 (10-II-4)	-0.01 (10-I-4)	0.01 (9-I-3)	-0.00 (10-I-4)
208	1.03 (9-I-1)	1.11 (10-I-1)	-1.76 (10-II-1)	0.02 (10-II-1)	-0.00 (9-II-3)	-0.00 (10-I-4)
209	-1.13 (9-II-1)	1.34 (10-I-2)	-1.68 (10-II-2)	-0.01 (10-I-2)	-0.01 (9-II-3)	0.00 (10-I-2)
210	1.11 (9-I-3)	1.29 (10-I-4)	-1.84 (10-I-4)	0.01 (10-II-4)	0.01 (9-I-1)	0.00 (10-II-4)
211	1.02 (9-I-3)	1.24 (10-I-3)	-1.84 (10-I-3)	-0.02 (10-I-3)	0.00 (9-I-1)	-0.00 (10-I-4)
212	-1.11 (9-II-3)	1.29 (10-I-2)	-1.84 (10-I-2)	0.01 (10-II-2)	-0.01 (9-II-1)	-0.00 (10-II-2)

Tipo diagramma: Deformata
Combinazione corrente : Scenario ScenarioNT_2018 A2_SLV_SLD_STR_GEO - C 10-II
Posizione masse N° 1



Risultati Analisi Dinamica - Sollecitazioni Massime - Muri discretizzati - S.L.E
Scenario di calcolo: **ScenarioNT_2018 A2_SLV_SLD_STR_GEO**

Muro	Pann.	Sxx MPa	Syy MPa	Sxy MPa	Mxx kN	Myy kN	Mxy kN
1	1	-0.10 (10-I-4)	-0.09 (9-II-3)	-0.15 (9-I-3)	-0.20 (6)	-0.73 (10-I-4)	-0.31 (10-II-3)
1	2	-0.17 (9-I-3)	-0.06 (9-I-3)	-0.05 (9-I-3)	-0.26 (10-II-3)	-0.24 (10-II-4)	-0.32 (10-II-2)
1	3	-0.23 (6)	0.06 (9-I-1)	-0.26 (10-II-4)	0.06 (9-I-1)	-0.12 (9-II-1)	-0.57 (10-II-2)
1	4	-0.96 (9-I-3)	-0.13 (9-I-3)	-0.13 (9-II-3)	-0.08 (10-I-4)	0.06 (10-II-4)	-0.50 (10-II-2)
1	5	-0.25 (6)	0.02 (10-I-4)	-0.08 (9-II-3)	0.22 (6)	0.35 (6)	-0.24 (10-II-2)
1	6	-1.45 (6)	-0.21 (10-I-4)	-0.03 (9-II-3)	0.20 (6)	0.08 (6)	-0.21 (10-II-2)
1	7	-0.18 (9-II-2)	-0.01 (9-I-1)	0.19 (9-I-3)	0.23 (6)	0.32 (6)	0.60 (10-I-2)
1	8	-1.22 (6)	-0.16 (9-II-3)	0.08 (9-I-3)	0.26 (6)	0.10 (6)	0.55 (10-I-2)
1	9	-0.04 (10-II-2)	0.05 (9-I-3)	0.41 (9-I-3)	0.13 (9-II-3)	0.34 (9-II-3)	1.09 (10-I-2)
1	10	-0.32 (9-II-3)	0.11 (9-I-3)	0.19 (9-I-3)	0.18 (9-II-3)	0.06 (9-II-3)	1.01 (10-I-2)
1	11	0.12 (10-I-3)	-0.14 (9-I-3)	0.35 (9-II-3)	-0.45 (9-I-3)	-0.74 (9-I-3)	0.76 (9-II-3)
1	12	1.49 (9-I-3)	0.27 (6)	0.18 (9-II-3)	-0.49 (9-I-3)	-0.17 (9-I-3)	0.59 (9-II-3)
2	1	0.12 (10-I-3)	-0.14 (9-II-3)	-0.35 (9-I-3)	-0.45 (9-II-3)	-0.74 (9-II-3)	-0.76 (9-I-3)
2	2	1.49 (9-II-3)	0.27 (6)	-0.18 (9-I-3)	-0.49 (9-II-3)	-0.17 (9-II-3)	-0.59 (9-I-3)
2	3	-0.04 (10-II-4)	0.05 (9-II-3)	-0.41 (9-II-3)	0.13 (9-I-3)	0.34 (9-I-3)	-1.09 (10-I-4)
2	4	-0.32 (9-I-3)	0.11 (9-II-3)	-0.19 (9-II-3)	0.18 (9-I-3)	0.06 (9-I-3)	-1.01 (10-I-4)
2	5	-0.18 (9-I-4)	-0.01 (9-II-1)	-0.19 (9-II-3)	0.23 (6)	0.32 (6)	-0.60 (10-I-4)
2	6	-1.22 (6)	-0.16 (9-I-3)	-0.08 (9-II-3)	0.26 (6)	0.10 (6)	-0.55 (10-I-4)
2	7	-0.25 (6)	0.02 (10-I-2)	0.08 (9-I-3)	0.22 (6)	0.35 (6)	0.24 (10-II-4)
2	8	-1.45 (6)	-0.21 (10-I-2)	0.03 (9-I-3)	0.20 (6)	0.08 (6)	0.21 (10-II-4)
2	9	-0.23 (6)	0.06 (9-II-1)	0.26 (10-II-2)	0.06 (9-II-1)	-0.12 (9-I-1)	0.57 (10-II-4)
2	10	-0.96 (9-II-3)	-0.13 (9-II-3)	0.13 (9-I-3)	-0.08 (10-I-2)	0.06 (10-II-2)	0.50 (10-II-4)
2	11	-0.10 (10-I-2)	-0.09 (9-I-3)	0.15 (9-II-3)	-0.20 (6)	-0.73 (10-I-2)	0.31 (10-II-3)
2	12	-0.17 (9-II-3)	-0.06 (9-II-3)	0.05 (9-II-3)	-0.26 (10-II-3)	-0.24 (10-II-2)	0.32 (10-II-4)
3	1	-0.10 (10-II-2)	-0.09 (9-I-1)	-0.15 (9-II-1)	-0.20 (6)	-0.75 (10-II-2)	-0.30 (10-I-1)
3	2	-0.17 (9-II-1)	-0.06 (9-II-1)	-0.05 (9-II-1)	-0.26 (10-I-1)	-0.24 (10-I-2)	-0.31 (10-I-4)
3	3	-0.23 (6)	0.06 (9-II-3)	-0.26 (10-I-2)	0.05 (9-II-3)	-0.14 (9-I-3)	-0.57 (10-I-4)
3	4	-0.95 (9-II-1)	-0.12 (9-II-1)	-0.14 (9-I-1)	-0.09 (10-II-2)	0.06 (10-I-2)	-0.49 (10-I-4)
3	5	-0.26 (6)	0.02 (10-II-2)	-0.08 (9-I-1)	0.22 (6)	0.35 (6)	-0.24 (10-I-4)
3	6	-1.45 (6)	-0.20 (10-II-2)	-0.03 (9-I-1)	0.20 (6)	0.07 (6)	-0.21 (10-I-4)
3	7	-0.18 (9-I-4)	-0.01 (9-II-3)	0.19 (9-II-1)	0.23 (6)	0.32 (6)	0.59 (10-II-4)
3	8	-1.24 (6)	-0.16 (9-I-1)	0.08 (9-II-1)	0.26 (6)	0.10 (6)	0.54 (10-II-4)
3	9	-0.05 (10-I-4)	0.05 (9-II-1)	0.41 (9-II-1)	0.13 (9-I-1)	0.34 (9-I-1)	1.08 (10-II-4)
3	10	-0.36 (9-I-1)	0.11 (9-II-1)	0.19 (9-II-1)	0.18 (9-I-1)	0.06 (9-I-1)	1.00 (10-II-4)
3	11	0.10 (10-II-1)	-0.14 (9-II-1)	0.34 (9-I-1)	-0.45 (9-II-1)	-0.74 (9-II-1)	0.76 (9-I-1)
3	12	1.44 (9-II-1)	0.27 (6)	0.18 (9-I-1)	-0.49 (9-II-1)	-0.17 (9-II-1)	0.60 (9-I-1)
4	1	0.10 (10-II-1)	-0.14 (9-I-1)	-0.34 (9-II-1)	-0.45 (9-I-1)	-0.74 (9-I-1)	-0.76 (9-II-1)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 36 di 103

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
4	2	1.44 (9-I-1)	0.27 (6)	-0.18 (9-II-1)	-0.49 (9-I-1)	-0.17 (9-I-1)	-0.60 (9-II-1)
4	3	-0.05 (10-I-2)	0.05 (9-I-1)	-0.41 (9-I-1)	0.13 (9-II-1)	0.34 (9-II-1)	-1.08 (10-II-2)
4	4	-0.36 (9-II-1)	0.11 (9-I-1)	-0.19 (9-I-1)	0.18 (9-II-1)	0.06 (9-II-1)	-1.00 (10-II-2)
4	5	-0.18 (9-II-2)	-0.01 (9-I-3)	-0.19 (9-I-1)	0.23 (6)	0.32 (6)	-0.59 (10-II-2)
4	6	-1.24 (6)	-0.16 (9-II-1)	-0.08 (9-I-1)	0.26 (6)	0.10 (6)	-0.54 (10-II-2)
4	7	-0.26 (6)	0.02 (10-II-4)	0.08 (9-II-1)	0.22 (6)	0.35 (6)	0.24 (10-I-2)
4	8	-1.45 (6)	-0.20 (10-II-4)	0.03 (9-II-1)	0.20 (6)	0.07 (6)	0.21 (10-I-2)
4	9	-0.23 (6)	0.06 (9-I-3)	0.26 (10-I-4)	0.05 (9-I-3)	-0.14 (9-I-3)	0.57 (10-I-2)
4	10	-0.95 (9-I-1)	-0.12 (9-I-1)	0.14 (9-II-1)	-0.09 (10-II-4)	0.06 (10-I-4)	0.49 (10-I-2)
4	11	-0.10 (10-II-4)	-0.09 (9-II-1)	0.15 (9-I-1)	-0.20 (6)	-0.75 (10-II-4)	0.30 (10-I-1)
4	12	-0.17 (9-I-1)	-0.06 (9-I-1)	0.05 (9-I-1)	-0.26 (10-I-1)	-0.24 (10-I-4)	0.31 (10-I-2)
5	1	-0.06 (10-I-4)	-0.15 (10-II-4)	-0.09 (10-I-4)	-0.04 (10-II-2)	-0.39 (10-II-1)	0.24 (10-II-4)
5	2	0.37 (10-II-4)	0.09 (10-II-4)	0.07 (10-II-4)	-0.05 (9-I-4)	-0.40 (10-II-4)	0.25 (10-II-4)
5	3	-0.14 (10-I-4)	0.02 (10-I-4)	-0.17 (10-II-4)	-0.09 (10-II-4)	-0.29 (10-II-4)	-0.10 (9-I-1)
5	4	-0.55 (10-I-4)	-0.07 (10-I-4)	-0.10 (10-II-4)	-0.09 (10-II-4)	0.08 (9-I-2)	-0.08 (9-I-1)
5	5	-0.16 (10-I-4)	-0.03 (10-II-4)	-0.11 (10-I-4)	0.05 (10-I-4)	0.08 (9-II-4)	-0.22 (10-II-4)
5	6	-0.69 (10-I-4)	-0.10 (10-I-4)	-0.04 (10-II-4)	0.06 (10-I-4)	-0.02 (10-II-4)	-0.20 (10-II-4)
5	7	-0.17 (10-II-4)	-0.03 (10-I-4)	0.11 (10-I-4)	0.05 (10-II-4)	0.08 (9-II-4)	0.24 (10-I-4)
5	8	-0.69 (10-II-4)	-0.10 (10-II-4)	0.04 (10-I-4)	0.06 (10-II-4)	-0.02 (10-I-4)	0.22 (10-I-4)
5	9	-0.14 (10-II-4)	0.02 (10-II-4)	0.17 (10-I-4)	-0.09 (10-I-4)	-0.28 (10-I-4)	0.12 (9-I-3)
5	10	-0.56 (10-I-4)	-0.07 (10-II-4)	0.10 (10-I-4)	-0.09 (10-I-4)	0.08 (9-I-2)	0.10 (9-I-3)
5	11	-0.07 (10-II-4)	-0.15 (10-I-4)	0.09 (10-II-4)	-0.05 (10-I-2)	-0.37 (10-I-3)	-0.22 (10-I-4)
5	12	0.37 (10-I-4)	0.09 (10-I-4)	-0.07 (10-I-4)	-0.06 (9-I-4)	-0.40 (10-I-4)	-0.23 (10-II-4)
6	1	0.37 (10-II-2)	0.09 (10-II-2)	-0.07 (10-II-2)	-0.05 (9-II-2)	-0.40 (10-II-2)	-0.25 (10-II-2)
6	2	-0.06 (10-I-2)	-0.15 (10-II-2)	0.09 (10-I-2)	-0.04 (10-II-4)	-0.39 (10-II-1)	-0.24 (10-II-2)
6	3	-0.55 (10-I-2)	-0.07 (10-I-2)	0.10 (10-II-2)	-0.09 (10-II-2)	0.08 (9-II-4)	0.08 (9-II-1)
6	4	-0.14 (10-I-2)	0.02 (10-I-2)	0.17 (10-II-2)	-0.09 (10-II-2)	-0.29 (10-II-2)	0.10 (9-II-1)
6	5	-0.69 (10-I-2)	-0.10 (10-I-2)	0.04 (10-II-2)	0.06 (10-I-2)	-0.02 (10-II-2)	0.20 (10-II-2)
6	6	-0.16 (10-I-2)	-0.03 (10-II-2)	0.11 (10-II-2)	0.05 (10-I-2)	0.08 (9-I-2)	0.22 (10-II-2)
6	7	-0.69 (10-II-2)	-0.10 (10-II-2)	-0.04 (10-I-2)	0.06 (10-II-2)	-0.02 (10-I-2)	-0.22 (10-I-2)
6	8	-0.17 (10-II-2)	-0.03 (10-I-2)	-0.11 (10-I-2)	0.05 (10-II-2)	0.08 (9-I-2)	-0.24 (10-I-2)
6	9	-0.56 (10-II-2)	-0.07 (10-II-2)	-0.10 (10-I-2)	-0.09 (10-I-2)	0.08 (9-II-4)	-0.10 (9-II-3)
6	10	-0.14 (10-II-2)	0.02 (10-II-2)	-0.17 (10-I-2)	-0.09 (10-I-2)	-0.28 (10-I-2)	-0.12 (9-II-3)
6	11	0.37 (10-I-2)	0.09 (10-I-2)	0.07 (10-I-2)	-0.06 (9-II-2)	-0.40 (10-I-2)	0.23 (10-I-2)
6	12	-0.07 (10-II-2)	-0.15 (10-I-2)	-0.09 (10-II-2)	-0.05 (10-I-4)	-0.37 (10-I-3)	0.22 (10-I-2)
7	1	-0.04 (9-II-3)	-1.09 (9-I-3)	0.24 (9-II-3)	10.67 (9-I-3)	12.87 (9-I-3)	-3.29 (9-II-3)
7	2	0.04 (9-II-3)	0.16 (9-II-3)	0.21 (9-I-3)	-1.35 (9-II-3)	-1.97 (9-II-3)	-2.72 (10-I-2)
7	3	0.09 (9-II-3)	0.59 (6)	0.06 (9-I-3)	-2.38 (6)	-6.32 (6)	-2.35 (10-I-2)
7	4	0.05 (9-I-3)	0.75 (6)	-0.03 (9-II-2)	-2.67 (6)	-7.98 (6)	-1.20 (10-I-2)
7	5	-0.11 (9-II-3)	0.56 (9-I-3)	-0.18 (9-II-2)	-1.32 (9-I-3)	-6.18 (9-I-3)	1.31 (10-II-2)
7	6	0.04 (9-II-3)	-0.22 (9-II-3)	-0.09 (9-I-3)	3.68 (10-II-4)	2.88 (9-II-3)	1.72 (9-I-3)
7	7	0.03 (9-I-3)	-1.05 (9-I-3)	0.17 (9-II-3)	7.81 (9-I-3)	12.15 (9-I-3)	-4.24 (9-II-3)
7	8	0.05 (10-I-3)	0.15 (9-II-3)	0.14 (9-I-3)	-1.06 (9-II-3)	-2.14 (9-II-3)	-3.66 (10-I-2)
7	9	0.11 (10-I-4)	0.62 (6)	0.02 (9-I-2)	-1.80 (6)	-6.30 (6)	-2.79 (10-I-2)
7	10	0.11 (9-I-3)	0.77 (6)	-0.03 (9-II-1)	-1.90 (6)	-7.73 (6)	-0.74 (10-I-2)
7	11	0.05 (9-I-3)	0.55 (9-I-3)	-0.12 (9-II-3)	-0.89 (9-I-3)	-5.94 (9-I-3)	2.11 (10-II-2)
7	12	-0.05 (10-I-4)	-0.18 (9-II-3)	0.06 (9-II-3)	2.96 (10-II-4)	3.00 (9-II-3)	1.43 (9-I-3)
7	13	-0.04 (9-II-3)	-1.04 (9-I-3)	0.10 (9-II-3)	4.84 (9-I-3)	11.21 (9-I-3)	-4.79 (9-II-3)
7	14	-0.06 (10-I-4)	0.15 (9-II-3)	0.06 (9-I-3)	0.55 (9-I-3)	-2.17 (9-II-3)	-4.54 (10-I-2)
7	15	-0.03 (9-I-3)	0.63 (6)	-0.02 (9-II-1)	-1.33 (6)	-6.16 (6)	-2.85 (10-I-2)
7	16	0.03 (10-I-3)	0.78 (6)	-0.03 (9-II-1)	-1.18 (10-II-4)	-7.38 (6)	-0.55 (10-I-2)
7	17	0.08 (10-I-4)	0.53 (9-I-3)	-0.05 (9-II-2)	-0.76 (10-I-4)	-5.65 (9-I-3)	3.03 (10-II-2)
7	18	0.03 (10-I-4)	-0.14 (9-II-3)	0.07 (9-II-4)	1.85 (10-II-4)	2.79 (9-II-3)	1.50 (10-II-2)
7	19	0.05 (9-I-3)	-1.04 (9-I-3)	0.04 (9-II-3)	2.30 (9-I-3)	10.17 (9-I-3)	-5.01 (9-II-3)
7	20	-0.08 (9-II-3)	0.17 (9-II-3)	-0.04 (9-II-3)	0.70 (9-I-3)	-2.08 (9-II-3)	-4.96 (10-I-2)
7	21	-0.11 (6)	0.66 (6)	-0.05 (6)	-0.82 (10-II-4)	-5.95 (6)	-2.79 (10-I-2)
7	22	-0.04 (9-I-3)	0.79 (6)	-0.03 (10-I-4)	-0.47 (10-II-4)	-7.01 (6)	0.58 (10-II-2)
7	23	0.09 (9-II-3)	0.52 (9-I-3)	0.01 (10-II-4)	-0.76 (9-I-3)	-5.24 (9-I-3)	3.37 (10-II-2)
7	24	0.10 (10-I-4)	-0.13 (9-II-3)	0.09 (10-I-4)	-1.33 (10-I-4)	2.37 (9-II-3)	1.46 (10-II-2)
7	25	0.20 (9-I-3)	-1.06 (9-I-3)	-0.02 (10-II-2)	0.12 (9-II-3)	9.12 (9-I-3)	-5.03 (9-II-3)
7	26	-0.08 (9-II-3)	0.20 (9-II-3)	-0.10 (9-II-3)	0.80 (6)	-1.94 (9-II-3)	-5.25 (10-I-2)
7	27	-0.20 (6)	0.69 (6)	-0.08 (9-I-3)	-0.29 (10-II-4)	-5.70 (6)	-2.78 (10-I-2)
7	28	-0.16 (9-I-3)	0.80 (6)	-0.03 (9-I-3)	0.35 (9-II-3)	-6.64 (6)	0.70 (9-II-1)
7	29	0.07 (9-II-3)	0.51 (9-I-3)	0.05 (9-II-3)	-0.77 (9-II-1)	-4.79 (9-I-3)	3.50 (10-II-2)
7	30	0.16 (6)	-0.13 (9-II-3)	0.10 (10-I-4)	-1.46 (10-I-4)	1.86 (9-II-3)	1.37 (10-II-2)
7	31	0.52 (9-I-3)	-1.09 (9-I-3)	-0.07 (9-II-3)	-1.94 (9-I-3)	8.04 (9-I-3)	-5.03 (9-II-3)
7	32	0.09 (9-I-3)	0.24 (9-II-3)	-0.15 (6)	1.17 (9-II-3)	-1.78 (9-II-3)	-5.79 (6)
7	33	-0.33 (6)	0.72 (6)	-0.10 (9-I-3)	0.44 (10-I-4)	-5.39 (6)	-3.17 (9-I-4)
7	34	-0.43 (6)	0.80 (6)	-0.03 (9-I-3)	0.96 (9-II-3)	-6.20 (6)	0.97 (9-II-4)
7	35	-0.24 (9-I-3)	0.48 (9-I-3)	0.08 (9-II-3)	-0.97 (9-II-3)	-4.30 (9-I-3)	3.65 (10-II-2)
7	36	0.17 (10-II-3)	-0.16 (9-II-3)	0.08 (6)	-1.68 (10-I-4)	1.30 (9-II-3)	1.66 (9-I-3)
8	1	-0.10 (9-I-1)	0.14 (9-II-3)	0.13 (9-I-3)	3.23 (10-II-2)	3.47 (9-I-3)	-1.40 (10-I-2)
8	2	0.14 (9-II-3)	0.38 (6)	-0.31 (9-II-3)	-3.25 (10-I-4)	-4.56 (9-II-3)	2.43 (9-II-3)
8	3	0.38 (6)	0.41 (6)	-0.36 (6)	-6.04 (10-I-4)	-5.13 (10-II-4)	2.66 (6)
8	4	0.38 (6)	0.32 (9-I-3)	-0.25 (6)	-6.27 (10-I-4)	-2.96 (10-II-4)	2.06 (9-I-3)
8	5	0.25 (9-I-3)	-0.25 (9-II-3)	-0.06 (9-I-3)	-4.24 (9-I-3)	2.09 (10-I-4)	0.31 (9-I-3)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 37 di 103

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
8	6	-0.41 (9-II-3)	-0.66 (6)	0.56 (9-II-3)	11.97 (9-II-3)	12.22 (10-I-4)	-1.10 (9-II-3)
8	7	-0.04 (9-I-4)	-0.17 (9-I-3)	0.08 (9-I-3)	3.30 (10-II-2)	2.81 (9-I-3)	-1.43 (10-I-2)
8	8	0.23 (9-II-3)	0.37 (6)	-0.25 (9-II-3)	-2.15 (9-II-1)	-5.21 (6)	2.52 (9-II-3)
8	9	0.42 (6)	0.46 (6)	-0.33 (6)	-5.14 (10-I-4)	-4.91 (10-II-4)	2.92 (6)
8	10	0.38 (6)	0.35 (9-I-3)	-0.26 (9-I-3)	-6.45 (10-I-4)	-2.10 (10-II-4)	2.28 (9-I-3)
8	11	0.17 (9-I-3)	-0.16 (9-II-3)	-0.06 (9-I-3)	-4.76 (9-I-3)	3.23 (9-II-1)	0.54 (9-I-3)
8	12	-0.43 (9-II-3)	-0.59 (6)	0.54 (9-II-3)	8.66 (9-II-3)	11.89 (10-I-4)	-2.17 (9-II-3)
8	13	0.10 (9-II-3)	-0.14 (9-I-3)	0.08 (9-I-3)	3.27 (10-II-2)	1.86 (9-I-3)	-1.24 (10-I-2)
8	14	0.28 (9-II-3)	0.33 (9-II-3)	-0.23 (9-II-3)	-0.99 (9-II-1)	-5.80 (6)	2.52 (9-II-3)
8	15	0.38 (6)	0.43 (6)	-0.37 (6)	-4.47 (9-II-1)	-4.49 (10-II-4)	3.12 (6)
8	16	0.28 (6)	0.32 (9-I-3)	-0.33 (6)	-6.25 (10-I-4)	-1.71 (10-II-4)	2.41 (9-I-3)
8	17	0.06 (9-I-3)	-0.13 (9-II-3)	-0.10 (9-I-3)	-5.14 (9-I-3)	4.39 (9-II-1)	0.93 (9-I-3)
8	18	-0.48 (9-II-3)	-0.57 (9-II-3)	0.51 (9-II-3)	5.35 (9-II-3)	11.16 (6)	-3.18 (9-II-3)
8	19	0.16 (9-II-3)	-0.12 (9-I-3)	0.10 (9-I-3)	2.73 (10-II-2)	-1.29 (9-II-3)	-1.20 (9-I-1)
8	20	0.30 (9-II-3)	0.29 (9-II-3)	-0.22 (9-II-3)	0.97 (10-II-3)	-5.87 (6)	2.40 (9-II-3)
8	21	0.35 (6)	0.40 (6)	-0.41 (6)	-3.87 (9-II-1)	-4.08 (10-II-4)	3.30 (6)
8	22	0.23 (9-I-3)	0.33 (6)	-0.38 (6)	-5.85 (10-I-4)	-1.41 (9-I-1)	2.58 (6)
8	23	-0.09 (9-II-3)	0.09 (9-I-3)	-0.12 (9-I-3)	-5.26 (6)	4.94 (9-II-1)	1.16 (9-I-3)
8	24	-0.48 (9-II-3)	-0.51 (9-II-3)	0.55 (9-II-3)	3.06 (9-II-3)	9.95 (6)	-3.94 (9-II-3)
8	25	0.20 (9-II-3)	-0.09 (9-I-3)	0.13 (9-I-3)	2.10 (10-II-2)	-1.51 (9-II-3)	-1.22 (9-I-2)
8	26	0.30 (9-II-3)	0.23 (9-II-3)	-0.25 (9-II-3)	1.30 (10-II-3)	-5.77 (6)	2.23 (9-II-3)
8	27	0.29 (6)	0.35 (6)	-0.48 (6)	-3.23 (9-II-1)	-3.67 (10-II-4)	3.46 (6)
8	28	0.18 (9-I-3)	0.32 (6)	-0.45 (6)	-5.46 (10-I-4)	-0.97 (9-I-1)	2.76 (6)
8	29	-0.13 (9-II-3)	0.16 (9-I-3)	-0.14 (9-I-3)	-5.41 (6)	5.35 (9-II-1)	1.32 (9-I-3)
8	30	-0.44 (9-II-3)	-0.42 (9-II-3)	0.63 (9-II-3)	-1.81 (9-I-3)	8.58 (10-I-4)	-4.53 (9-II-3)
8	31	0.14 (9-II-3)	-0.08 (9-I-3)	0.15 (9-I-3)	1.68 (10-II-2)	-2.21 (9-II-3)	-1.18 (9-I-3)
8	32	0.18 (9-II-4)	0.06 (9-II-3)	-0.36 (9-II-3)	1.64 (10-II-2)	-5.84 (6)	2.04 (9-II-3)
8	33	0.17 (10-II-1)	0.21 (9-II-3)	-0.61 (6)	-2.56 (9-II-3)	-3.27 (9-I-1)	3.56 (6)
8	34	0.11 (9-I-3)	0.29 (6)	-0.53 (6)	-5.37 (6)	1.04 (9-II-3)	2.90 (6)
8	35	-0.11 (9-II-3)	0.25 (9-I-3)	-0.13 (9-I-3)	-5.82 (6)	6.00 (9-II-4)	1.48 (9-I-3)
8	36	-0.33 (9-II-3)	-0.25 (9-II-3)	0.80 (9-II-3)	-2.90 (9-I-3)	7.22 (10-I-4)	-4.99 (9-II-3)
9	1	-0.40 (10-II-2)	0.21 (10-II-2)	0.03 (10-II-4)	2.90 (10-II-2)	-0.41 (9-I-1)	-1.36 (10-II-2)
9	2	-0.39 (10-II-2)	0.08 (10-I-1)	0.03 (10-II-2)	3.57 (10-II-2)	0.75 (9-II-1)	-1.96 (10-II-2)
9	3	-0.39 (10-II-2)	0.04 (10-I-2)	0.06 (10-II-2)	4.28 (10-II-2)	1.59 (9-II-1)	-2.27 (10-II-2)
9	4	-0.41 (10-II-2)	-0.03 (10-II-2)	0.08 (10-II-2)	5.01 (10-II-2)	2.53 (9-II-1)	-2.62 (10-II-2)
9	5	-0.46 (10-II-2)	-0.12 (10-I-1)	0.11 (10-II-2)	5.65 (10-II-2)	3.51 (9-II-1)	-3.40 (10-II-2)
9	6	-0.51 (10-II-2)	0.06 (10-II-2)	0.10 (10-II-2)	6.06 (10-II-2)	4.28 (9-II-1)	-4.08 (10-II-2)
9	7	0.28 (10-I-2)	0.20 (10-II-2)	0.05 (10-II-2)	-2.36 (10-I-2)	-1.25 (10-II-2)	1.82 (10-II-2)
9	8	0.27 (10-I-2)	0.08 (10-II-2)	0.03 (10-II-2)	-2.59 (10-I-2)	-0.72 (10-II-2)	1.48 (10-II-2)
9	9	0.27 (10-I-2)	0.05 (10-II-2)	0.02 (10-I-2)	-2.75 (10-I-2)	-0.19 (10-II-4)	1.42 (10-II-2)
9	10	0.27 (10-I-2)	0.04 (9-I-2)	-0.05 (10-II-2)	-2.85 (10-I-2)	0.35 (10-II-2)	1.27 (10-II-2)
9	11	0.27 (10-I-2)	-0.08 (10-II-2)	-0.10 (10-II-2)	-2.84 (10-I-2)	0.78 (10-II-2)	-0.77 (10-I-2)
9	12	0.28 (10-I-2)	-0.08 (10-II-2)	-0.13 (10-II-2)	-2.84 (10-I-2)	1.00 (10-II-2)	-0.63 (10-II-2)
9	13	0.32 (10-I-2)	0.04 (10-II-2)	0.03 (10-II-2)	-2.67 (10-I-2)	0.48 (10-II-2)	1.45 (10-II-2)
9	14	0.30 (10-I-2)	-0.07 (10-I-2)	0.02 (10-II-2)	-2.82 (10-I-2)	0.25 (10-II-2)	1.09 (10-II-2)
9	15	0.29 (10-I-2)	-0.04 (10-I-2)	0.01 (10-II-2)	-2.91 (10-I-2)	-0.27 (10-I-2)	0.94 (10-II-2)
9	16	0.29 (10-I-2)	0.02 (9-I-3)	-0.01 (10-II-2)	-2.96 (10-I-2)	-0.39 (9-II-2)	0.89 (10-II-2)
9	17	0.28 (10-I-2)	-0.05 (10-II-2)	-0.01 (10-II-2)	-2.97 (10-I-2)	-0.50 (9-II-2)	0.86 (10-II-2)
9	18	0.28 (10-I-2)	0.04 (10-I-2)	-0.03 (10-II-2)	-2.95 (10-I-2)	-0.61 (10-II-2)	-0.76 (10-I-2)
9	19	0.32 (10-II-2)	0.04 (10-I-2)	-0.03 (10-I-2)	-2.68 (10-II-2)	0.48 (10-I-2)	-1.48 (10-I-2)
9	20	0.30 (10-II-2)	-0.08 (10-II-2)	-0.02 (10-I-2)	-2.83 (10-I-2)	0.25 (10-II-2)	-1.16 (10-I-2)
9	21	0.30 (10-II-2)	-0.04 (10-II-2)	-0.01 (10-I-2)	-2.92 (10-II-2)	-0.28 (10-II-2)	-1.04 (10-I-2)
9	22	0.29 (10-II-2)	0.02 (9-I-1)	0.01 (10-I-2)	-2.97 (10-II-2)	-0.39 (9-II-2)	-0.99 (10-I-2)
9	23	0.28 (10-II-2)	-0.05 (10-I-2)	0.01 (10-I-2)	-2.99 (10-II-2)	-0.50 (9-II-2)	-0.97 (10-I-2)
9	24	0.28 (10-II-2)	0.04 (10-II-2)	0.03 (10-I-2)	-2.97 (10-II-2)	-0.61 (10-I-2)	0.63 (10-II-2)
9	25	0.28 (10-II-2)	0.20 (10-I-2)	-0.05 (10-I-2)	-2.39 (10-II-2)	-1.24 (10-I-2)	-1.86 (10-I-2)
9	26	0.27 (10-II-2)	0.08 (10-I-2)	-0.03 (10-I-2)	-2.61 (10-II-2)	-0.70 (10-I-2)	-1.56 (10-I-2)
9	27	0.27 (10-II-2)	0.05 (10-I-2)	-0.02 (10-II-2)	-2.78 (10-II-2)	-0.17 (10-I-4)	-1.52 (10-I-2)
9	28	0.28 (10-II-2)	0.04 (9-I-2)	0.05 (10-I-2)	-2.87 (10-II-2)	0.36 (10-I-2)	-1.38 (10-I-2)
9	29	0.27 (10-II-2)	-0.08 (10-I-2)	0.10 (10-I-2)	-2.87 (10-II-2)	0.78 (10-I-2)	-0.73 (10-I-2)
9	30	0.28 (10-II-2)	-0.08 (10-I-2)	0.13 (10-I-2)	-2.87 (10-I-2)	1.01 (10-II-2)	0.51 (10-I-2)
9	31	-0.40 (10-I-2)	0.21 (10-I-2)	-0.03 (10-I-4)	2.90 (10-I-2)	-0.38 (9-I-3)	1.31 (10-I-2)
9	32	-0.39 (10-I-2)	0.08 (10-II-3)	-0.03 (10-I-2)	3.57 (10-I-2)	0.76 (9-II-3)	1.88 (10-I-2)
9	33	-0.39 (10-I-2)	0.04 (10-II-2)	-0.06 (10-I-2)	4.28 (10-I-2)	1.59 (9-II-3)	2.17 (10-I-2)
9	34	-0.41 (10-I-2)	-0.03 (10-I-2)	-0.08 (10-I-2)	5.00 (10-I-2)	2.53 (9-II-3)	2.52 (10-I-2)
9	35	-0.46 (10-I-2)	-0.12 (10-II-3)	-0.11 (10-I-2)	5.65 (10-I-2)	3.51 (9-II-3)	3.29 (10-I-2)
9	36	-0.51 (10-I-2)	0.06 (10-I-2)	-0.10 (10-I-2)	6.06 (10-I-2)	4.29 (9-II-3)	3.96 (10-I-2)
10	1	-1.07 (9-II-1)	0.51 (9-II-1)	0.07 (9-I-1)	7.85 (9-II-1)	-1.93 (9-II-1)	5.01 (9-I-1)
10	2	-1.04 (9-II-1)	0.20 (9-II-1)	0.02 (10-I-4)	8.92 (9-II-1)	0.11 (9-I-1)	5.03 (9-I-1)
10	3	-1.02 (9-II-1)	0.05 (9-II-1)	-0.04 (9-I-1)	9.97 (9-II-1)	2.27 (9-II-1)	5.02 (9-I-1)
10	4	-1.02 (9-II-1)	-0.04 (9-I-1)	-0.10 (9-I-1)	11.00 (9-II-1)	4.79 (9-II-1)	4.81 (9-I-1)
10	5	-1.03 (9-II-1)	0.03 (9-II-1)	-0.17 (9-I-1)	11.95 (9-II-1)	7.74 (9-II-1)	4.27 (9-I-1)
10	6	-1.07 (9-II-1)	-0.04 (9-I-1)	-0.24 (9-I-1)	12.66 (9-II-1)	10.58 (9-II-1)	3.35 (9-I-1)
10	7	0.26 (9-I-1)	0.08 (9-II-1)	0.15 (6)	-1.93 (9-I-1)	1.17 (9-I-1)	5.73 (6)
10	8	0.21 (9-I-1)	-0.08 (9-I-1)	0.10 (9-I-1)	-2.09 (9-I-1)	0.79 (6)	5.19 (10-II-4)
10	9	0.18 (9-I-1)	-0.08 (9-I-1)	0.04 (9-I-1)	-2.24 (9-I-1)	0.69 (9-II-1)	4.91 (10-II-4)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 38 di 103

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
10	10	0.17 (9-I-1)	-0.05 (10-II-2)	-0.06 (9-II-1)	-2.33 (9-I-1)	0.55 (9-II-1)	4.51 (10-II-4)
10	11	0.17 (9-I-1)	0.05 (10-II-1)	-0.14 (9-II-1)	-2.30 (9-I-1)	-1.07 (9-I-1)	3.63 (10-II-4)
10	12	0.17 (9-I-1)	0.04 (9-I-1)	-0.21 (9-II-1)	-2.13 (9-I-1)	-1.37 (9-I-1)	2.71 (10-II-4)
10	13	0.73 (6)	-0.33 (6)	0.09 (9-II-1)	-5.47 (6)	0.44 (10-II-2)	3.10 (9-II-3)
10	14	0.70 (6)	-0.20 (6)	0.08 (9-II-1)	-5.79 (6)	-0.28 (10-I-2)	2.73 (10-II-4)
10	15	0.67 (6)	-0.11 (6)	0.05 (6)	-6.04 (6)	-0.82 (10-I-2)	2.74 (10-II-4)
10	16	0.64 (6)	-0.03 (9-II-1)	0.02 (9-I-3)	-6.24 (6)	-1.33 (6)	2.81 (10-II-4)
10	17	0.63 (6)	0.11 (10-II-2)	-0.02 (9-II-4)	-6.39 (6)	-1.80 (6)	2.76 (10-II-4)
10	18	0.60 (6)	0.09 (9-I-1)	-0.06 (9-II-1)	-6.42 (6)	-2.37 (6)	2.33 (10-II-4)
10	19	0.80 (6)	-0.42 (6)	0.03 (9-II-1)	-6.22 (6)	0.97 (9-I-1)	-1.03 (9-I-2)
10	20	0.80 (6)	-0.16 (9-II-1)	0.03 (9-II-1)	-6.66 (6)	0.36 (9-I-1)	-0.72 (9-I-3)
10	21	0.79 (6)	-0.04 (9-II-1)	0.03 (10-II-2)	-7.03 (6)	-0.47 (10-I-2)	-0.59 (10-I-4)
10	22	0.78 (6)	0.03 (10-II-1)	0.03 (9-I-3)	-7.40 (6)	-1.18 (10-I-2)	0.52 (10-II-4)
10	23	0.77 (6)	0.11 (9-II-1)	0.03 (9-I-3)	-7.76 (6)	-1.90 (6)	0.71 (10-II-4)
10	24	0.75 (6)	0.04 (9-II-1)	0.03 (9-I-4)	-8.01 (6)	-2.67 (6)	1.18 (10-II-4)
10	25	0.47 (9-II-1)	-0.23 (9-II-1)	-0.09 (9-I-1)	-4.28 (9-II-1)	-1.02 (9-I-1)	-3.67 (10-I-4)
10	26	0.50 (9-II-1)	0.07 (9-I-1)	-0.05 (9-I-1)	-4.76 (9-II-1)	-0.81 (9-I-3)	-3.50 (10-I-4)
10	27	0.52 (9-II-1)	0.09 (9-I-1)	-0.01 (10-I-2)	-5.22 (9-II-1)	-0.77 (10-II-2)	-3.38 (10-I-4)
10	28	0.53 (9-II-1)	0.08 (10-II-2)	0.05 (9-I-4)	-5.63 (9-II-1)	-0.75 (10-II-2)	-3.04 (10-I-4)
10	29	0.54 (9-II-1)	0.05 (9-II-1)	0.12 (9-I-1)	-5.91 (9-II-1)	-0.87 (9-II-1)	-2.12 (10-I-4)
10	30	0.56 (9-II-1)	-0.11 (9-I-1)	0.18 (9-I-4)	-6.15 (9-II-1)	-1.30 (9-II-1)	-1.29 (10-I-4)
10	31	-0.17 (9-I-1)	0.17 (10-I-1)	-0.08 (6)	1.35 (9-I-1)	-1.70 (10-II-2)	-1.62 (9-II-1)
10	32	-0.14 (9-I-1)	0.16 (6)	-0.10 (10-II-2)	1.93 (9-I-1)	-1.48 (10-II-2)	-1.31 (10-I-4)
10	33	-0.14 (9-I-1)	0.09 (10-II-2)	-0.09 (10-II-2)	2.46 (9-I-1)	-1.34 (10-II-2)	-1.39 (10-I-4)
10	34	-0.16 (9-I-1)	0.03 (10-II-2)	-0.08 (9-I-2)	2.90 (9-I-1)	1.81 (10-I-2)	-1.43 (10-I-4)
10	35	-0.19 (9-I-1)	-0.04 (9-II-1)	-0.07 (9-I-1)	3.13 (9-I-1)	2.92 (10-I-2)	-1.37 (9-II-1)
10	36	-0.23 (9-I-1)	0.04 (9-I-1)	0.09 (9-II-1)	3.04 (9-I-1)	3.64 (10-I-2)	-1.65 (9-II-1)
11	1	-0.17 (9-II-1)	0.17 (10-I-1)	0.08 (6)	1.35 (9-II-1)	-1.70 (10-II-2)	1.62 (9-I-1)
11	2	-0.14 (9-II-1)	0.16 (6)	0.10 (10-II-4)	1.93 (9-II-1)	-1.47 (10-II-4)	1.31 (10-I-2)
11	3	-0.14 (9-II-1)	0.09 (10-II-4)	0.09 (10-II-4)	2.46 (9-II-1)	-1.34 (10-II-4)	1.39 (10-I-2)
11	4	-0.16 (9-II-1)	0.03 (10-II-4)	0.03 (9-II-4)	2.90 (9-II-1)	1.81 (10-I-4)	1.43 (10-I-2)
11	5	-0.19 (9-II-1)	-0.04 (10-II-4)	0.07 (9-II-1)	3.13 (9-II-1)	2.92 (10-I-4)	1.37 (9-I-1)
11	6	-0.23 (9-II-1)	0.04 (9-II-1)	-0.09 (9-I-1)	3.04 (9-II-1)	3.64 (10-I-4)	1.65 (9-I-1)
11	7	0.47 (9-I-1)	-0.23 (9-I-1)	0.09 (9-II-1)	-4.28 (9-I-1)	-1.02 (9-II-1)	3.67 (10-I-2)
11	8	0.50 (9-I-1)	0.07 (9-II-1)	0.05 (9-II-1)	-4.76 (9-I-1)	-0.81 (9-II-3)	3.50 (10-I-2)
11	9	0.52 (9-I-1)	0.09 (9-II-1)	0.01 (10-I-4)	-5.22 (9-I-1)	-0.77 (10-II-4)	3.38 (10-I-2)
11	10	0.53 (9-I-1)	0.08 (10-II-4)	-0.05 (9-II-2)	-5.63 (9-I-1)	-0.75 (10-II-4)	3.04 (10-I-2)
11	11	0.54 (9-I-1)	0.05 (9-I-1)	-0.12 (9-II-1)	-5.91 (9-I-1)	-0.87 (9-I-1)	2.12 (10-I-2)
11	12	0.56 (9-I-1)	-0.11 (9-II-1)	-0.18 (9-II-2)	-6.15 (9-I-1)	-1.30 (9-I-1)	1.28 (10-I-2)
11	13	0.80 (6)	-0.42 (6)	-0.03 (9-I-1)	-6.22 (6)	0.97 (9-II-1)	1.03 (9-II-4)
11	14	0.80 (6)	-0.16 (9-I-1)	-0.03 (9-I-1)	-6.66 (6)	0.36 (9-II-1)	0.72 (9-II-3)
11	15	0.79 (6)	-0.04 (9-I-1)	-0.03 (10-II-4)	-7.03 (6)	-0.47 (10-I-4)	0.59 (10-I-2)
11	16	0.78 (6)	0.03 (10-II-1)	-0.03 (9-II-3)	-7.40 (6)	-1.18 (10-I-4)	-0.52 (10-II-2)
11	17	0.77 (6)	0.11 (9-I-1)	-0.03 (9-II-3)	-7.76 (6)	-1.90 (6)	-0.71 (10-II-2)
11	18	0.75 (6)	0.04 (9-I-1)	-0.03 (9-II-2)	-8.01 (6)	-2.67 (6)	-1.18 (10-II-2)
11	19	0.73 (6)	-0.33 (6)	-0.09 (9-I-1)	-5.47 (6)	0.44 (10-II-4)	-3.10 (9-I-3)
11	20	0.70 (6)	-0.20 (6)	-0.08 (9-I-1)	-5.79 (6)	-0.29 (10-I-4)	-2.73 (10-II-2)
11	21	0.67 (6)	-0.11 (6)	-0.05 (6)	-6.04 (6)	-0.82 (10-I-4)	-2.74 (10-II-2)
11	22	0.64 (6)	-0.03 (9-I-1)	-0.02 (9-II-3)	-6.24 (6)	-1.33 (6)	-2.81 (10-II-2)
11	23	0.63 (6)	0.11 (10-II-4)	0.02 (9-I-2)	-6.39 (6)	-1.80 (6)	-2.76 (10-II-2)
11	24	0.60 (6)	0.09 (9-II-1)	0.06 (9-I-1)	-6.42 (6)	-2.37 (6)	-2.33 (10-II-2)
11	25	0.26 (9-II-1)	0.08 (9-I-1)	-0.15 (6)	-1.93 (9-II-1)	1.17 (9-II-1)	-5.73 (6)
11	26	0.21 (9-II-1)	-0.08 (9-II-1)	-0.10 (9-II-1)	-2.09 (9-II-1)	0.79 (6)	-5.19 (10-II-2)
11	27	0.18 (9-II-1)	-0.08 (9-II-1)	-0.04 (9-II-1)	-2.24 (9-II-1)	0.69 (9-I-1)	-4.91 (10-II-2)
11	28	0.17 (9-II-1)	-0.05 (10-II-4)	0.06 (9-I-1)	-2.33 (9-II-1)	0.55 (9-I-1)	-4.51 (10-II-2)
11	29	0.17 (9-II-1)	0.05 (10-II-1)	0.14 (9-I-1)	-2.30 (9-II-1)	-1.07 (9-II-1)	-3.63 (10-II-2)
11	30	0.17 (9-II-1)	0.04 (9-II-1)	0.21 (9-I-1)	-2.13 (9-II-1)	-1.37 (9-II-1)	-2.71 (10-II-2)
11	31	-1.07 (9-I-1)	0.51 (9-I-1)	-0.07 (9-II-1)	7.85 (9-I-1)	-1.93 (9-I-1)	-5.01 (9-II-1)
11	32	-1.04 (9-I-1)	0.20 (9-I-1)	-0.02 (10-I-2)	8.92 (9-I-1)	0.11 (9-II-1)	-5.03 (9-II-1)
11	33	-1.02 (9-I-1)	0.05 (9-I-1)	0.04 (9-II-1)	9.97 (9-I-1)	2.27 (9-I-1)	-5.02 (9-II-1)
11	34	-1.02 (9-I-1)	-0.04 (9-II-1)	0.10 (9-II-1)	11.00 (9-I-1)	4.79 (9-I-1)	-4.81 (9-II-1)
11	35	-1.03 (9-I-1)	0.03 (9-I-1)	0.17 (9-II-1)	11.95 (9-I-1)	7.74 (9-I-1)	-4.27 (9-II-1)
11	36	-1.07 (9-I-1)	-0.04 (9-II-1)	0.24 (9-II-1)	12.66 (9-I-1)	10.58 (9-I-1)	-3.35 (9-II-1)
12	1	0.11 (10-I-4)	-0.12 (10-II-4)	-0.30 (10-II-4)	0.83 (10-I-1)	2.74 (10-II-4)	1.51 (10-II-4)
12	2	0.17 (10-I-4)	0.12 (10-I-4)	-0.22 (10-II-4)	1.58 (10-II-4)	-2.14 (9-I-3)	-1.33 (10-I-4)
12	3	0.14 (9-I-2)	0.15 (10-I-4)	0.18 (10-I-4)	-1.78 (10-I-4)	-1.99 (10-II-4)	-1.37 (10-I-4)
12	4	0.15 (10-II-4)	0.14 (9-I-2)	0.18 (10-II-4)	-2.02 (10-I-4)	-1.76 (10-II-4)	-1.38 (10-II-4)
12	5	0.12 (10-II-4)	0.17 (10-II-4)	-0.22 (10-I-4)	-2.18 (9-I-1)	1.62 (10-I-4)	-1.35 (10-II-4)
12	6	-0.12 (10-I-4)	0.12 (10-II-4)	-0.31 (10-I-4)	2.71 (10-I-4)	0.89 (10-II-3)	1.50 (10-I-4)
12	7	-0.14 (10-II-4)	-0.21 (10-II-4)	-0.22 (10-II-4)	0.87 (9-I-1)	3.95 (10-II-4)	1.58 (10-II-4)
12	8	0.15 (10-I-4)	-0.11 (10-II-4)	-0.15 (10-II-4)	1.46 (10-II-4)	-1.70 (9-I-3)	-1.39 (10-I-4)
12	9	0.10 (10-I-4)	0.12 (10-I-4)	0.19 (10-I-4)	-2.12 (10-I-4)	-1.79 (10-II-4)	-1.35 (10-I-4)
12	10	0.12 (10-II-4)	0.11 (10-II-4)	0.19 (10-II-4)	-1.86 (10-I-4)	-2.05 (10-II-4)	-1.36 (10-II-4)
12	11	-0.10 (10-I-4)	0.15 (10-II-4)	-0.15 (10-I-4)	-1.77 (9-I-1)	1.55 (10-I-4)	-1.41 (10-II-4)
12	12	-0.20 (10-I-4)	-0.14 (10-I-4)	-0.22 (10-I-4)	3.88 (9-I-1)	0.95 (9-I-3)	1.57 (10-I-4)
12	13	-0.15 (10-II-4)	-0.26 (10-II-4)	-0.19 (10-II-4)	1.32 (9-I-1)	5.05 (10-II-4)	1.51 (10-II-4)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 39 di 103

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
12	14	0.16(10-I-4)	0.12(10-I-4)	0.13(10-I-4)	1.62(10-II-4)	-1.48(10-I-4)	-1.41(10-I-4)
12	15	0.12(10-I-4)	0.13(10-I-4)	0.17(10-I-4)	-2.27(10-I-4)	-1.81(10-II-4)	-1.32(10-I-4)
12	16	0.13(10-II-4)	0.13(10-II-4)	0.17(10-II-4)	-1.90(10-I-4)	-2.18(10-II-4)	-1.32(10-II-4)
12	17	0.13(10-II-4)	0.16(10-II-4)	0.13(10-II-4)	-1.58(10-II-4)	1.72(10-I-4)	-1.42(10-II-4)
12	18	-0.26(10-I-4)	-0.15(10-I-4)	-0.19(10-I-4)	4.96(10-I-4)	1.41(9-I-3)	1.49(10-I-4)
12	19	-0.14(10-II-4)	-0.30(10-II-4)	-0.19(10-II-4)	1.79(9-I-1)	6.23(10-II-4)	1.40(10-II-4)
12	20	0.16(10-I-4)	0.14(10-I-4)	0.12(10-I-4)	1.69(10-II-4)	-1.28(10-I-4)	-1.36(10-I-4)
12	21	0.15(10-I-4)	0.15(10-I-4)	0.14(10-I-4)	-2.32(10-I-4)	-1.91(10-II-4)	-1.30(10-I-4)
12	22	0.15(10-II-4)	0.15(10-II-4)	0.14(10-II-4)	-2.01(10-I-4)	-2.23(10-II-4)	-1.30(10-II-4)
12	23	0.14(10-II-4)	0.16(10-II-4)	0.12(10-II-4)	-1.40(10-II-4)	1.79(10-I-4)	-1.38(10-II-4)
12	24	-0.30(10-I-4)	-0.14(10-I-4)	-0.19(10-I-4)	6.14(10-I-4)	1.88(9-I-3)	1.38(10-I-4)
12	25	-0.16(10-II-4)	-0.37(10-II-4)	-0.20(10-II-4)	1.93(9-I-1)	7.78(10-II-4)	1.28(10-II-4)
12	26	-0.21(10-II-4)	0.11(10-I-4)	0.15(10-I-4)	-2.37(10-I-4)	-0.83(10-I-4)	-1.25(10-I-4)
12	27	0.13(10-I-4)	0.11(10-I-4)	0.16(10-I-4)	-2.40(10-I-4)	-2.02(10-II-4)	-1.29(10-I-4)
12	28	0.11(10-II-4)	0.13(10-II-4)	0.16(10-II-4)	-2.13(10-I-4)	-2.30(10-II-4)	-1.30(10-II-4)
12	29	0.11(10-II-4)	-0.21(10-I-4)	0.15(10-II-4)	-0.95(10-II-4)	-2.27(10-II-4)	-1.26(10-II-4)
12	30	-0.37(10-I-4)	-0.16(10-I-4)	-0.20(10-I-4)	7.69(10-I-4)	2.04(9-I-3)	1.25(10-I-4)
12	31	-0.12(10-II-4)	-0.33(10-II-4)	-0.28(10-II-4)	2.22(9-I-2)	9.01(10-II-4)	-1.47(10-I-4)
12	32	-0.21(10-II-4)	0.16(10-I-4)	0.12(10-I-4)	-2.06(10-I-4)	1.44(10-II-4)	-1.19(10-I-4)
12	33	0.17(10-I-4)	0.15(10-I-4)	0.12(10-I-4)	-2.44(10-I-4)	-1.69(10-II-4)	-1.27(10-I-4)
12	34	0.15(10-II-4)	0.17(10-II-4)	0.12(10-II-4)	-1.82(10-I-4)	-2.32(10-II-4)	-1.28(10-II-4)
12	35	0.16(10-II-4)	-0.22(10-I-4)	0.12(10-II-4)	-1.39(10-II-4)	-1.94(10-II-4)	-1.21(10-II-4)
12	36	-0.32(10-I-4)	-0.12(10-I-4)	-0.28(10-I-4)	8.92(10-I-4)	2.34(9-I-2)	-1.51(10-II-4)

Risultati Analisi Dinamica - Sollecitazioni - Involuppi - Travi di fondazione - S.L.E
Scenario di calcolo: ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO

Asta	N.in. N.fin.	Comb.	N kN	Ty kN	Tz kN	Mt kN*m	My kN*m	Mz kN*m
9001	1	6	0.00	0.00	62.65	-0.47	-24.65	0.00
	4		0.00	0.00	-54.34	-1.69	2.17	0.00
9001	1	7	0.00	0.00	62.26	-0.44	-24.63	0.00
	4		0.00	0.00	-54.01	-1.72	2.01	0.00
9001	1	8	0.00	0.00	61.59	-0.43	-24.34	0.00
	4		0.00	0.00	-53.42	-1.70	2.02	0.00
9001	1	9-I-1	0.00	0.00	55.58	-0.14	-19.24	0.00
	4		0.00	0.00	-49.17	-1.10	-0.40	0.00
9001	1	9-II-1	0.00	0.00	67.59	-0.73	-29.43	0.00
	4		0.00	0.00	-57.68	-2.30	4.43	0.00
9001	1	9-I-2	0.00	0.00	56.07	-0.39	-21.75	0.00
	4		0.00	0.00	-48.63	-1.39	1.78	0.00
9001	1	9-II-2	0.00	0.00	67.10	-0.48	-26.92	0.00
	4		0.00	0.00	-58.22	-2.02	2.25	0.00
9001	1	9-I-3	0.00	0.00	56.55	-0.78	-23.01	0.00
	4		0.00	0.00	-48.02	-1.52	4.64	0.00
9001	1	9-II-3	0.00	0.00	66.63	-0.08	-25.66	0.00
	4		0.00	0.00	-58.83	-1.88	-0.61	0.00
9001	1	9-I-4	0.00	0.00	55.96	-0.50	-21.82	0.00
	4		0.00	0.00	-48.48	-1.40	2.36	0.00
9001	1	9-II-4	0.00	0.00	67.21	-0.37	-26.85	0.00
	4		0.00	0.00	-58.37	-2.00	1.68	0.00
9001	1	10-I-1	0.00	0.00	64.42	-4.00	-44.51	0.00
	4		0.00	0.00	-49.39	-5.29	20.95	0.00
9001	1	10-II-1	0.00	0.00	58.75	3.13	-4.17	0.00
	4		0.00	0.00	-57.46	1.89	-16.92	0.00
9001	1	10-I-2	0.00	0.00	63.75	-3.43	-40.51	0.00
	4		0.00	0.00	-50.32	-4.72	17.19	0.00
9001	1	10-II-2	0.00	0.00	59.42	2.56	-8.17	0.00
	4		0.00	0.00	-56.52	1.31	-13.16	0.00
9001	1	10-I-3	0.00	0.00	64.55	-4.00	-44.58	0.00
	4		0.00	0.00	-49.51	-5.30	20.91	0.00
9001	1	10-II-3	0.00	0.00	58.63	3.14	-4.09	0.00
	4		0.00	0.00	-57.34	1.89	-16.88	0.00
9001	1	10-I-4	0.00	0.00	65.16	-4.45	-47.95	0.00
	4		0.00	0.00	-48.68	-5.74	24.07	0.00
9001	1	10-II-4	0.00	0.00	58.02	3.58	-0.73	0.00
	4		0.00	0.00	-58.17	2.34	-20.04	0.00
9002	4	6	0.00	0.00	57.14	-0.91	-9.81	0.00
	5		0.00	0.00	-74.02	-2.58	-71.21	0.00
9002	4	7	0.00	0.00	56.94	-0.73	-10.40	0.00
	5		0.00	0.00	-70.61	-2.37	-64.92	0.00
9002	4	8	0.00	0.00	56.34	-0.73	-10.35	0.00

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 40 di 103

Asta	N.in.	Comb.	N	Ty	Tz	Mt	My	Mz
	5		0.00	0.00	-69.57	-2.35	-63.65	0.00
9002	4	9-I-1	0.00	0.00	55.07	-1.68	-20.23	0.00
	5		0.00	0.00	-63.16	-3.20	-49.81	0.00
9002	4	9-II-1	0.00	0.00	57.61	0.22	-0.47	0.00
	5		0.00	0.00	-75.98	-1.51	-77.49	0.00
9002	4	9-I-2	0.00	0.00	56.16	-1.29	-21.51	0.00
	5		0.00	0.00	-63.01	-2.85	-48.67	0.00
9002	4	9-II-2	0.00	0.00	56.52	-0.18	0.81	0.00
	5		0.00	0.00	-76.13	-1.86	-78.64	0.00
9002	4	9-I-3	0.00	0.00	57.63	-1.02	-22.65	0.00
	5		0.00	0.00	-62.97	-2.61	-47.82	0.00
9002	4	9-II-3	0.00	0.00	55.05	-0.44	1.95	0.00
	5		0.00	0.00	-76.17	-2.09	-79.49	0.00
9002	4	9-I-4	0.00	0.00	56.58	-1.28	-21.51	0.00
	5		0.00	0.00	-63.00	-2.84	-48.72	0.00
9002	4	9-II-4	0.00	0.00	56.10	-0.18	0.81	0.00
	5		0.00	0.00	-76.14	-1.87	-78.59	0.00
9002	4	10-I-1	0.00	0.00	67.85	1.98	-17.21	0.00
	5		0.00	0.00	-73.73	-0.32	-58.38	0.00
9002	4	10-II-1	0.00	0.00	44.83	-3.44	-3.49	0.00
	5		0.00	0.00	-65.41	-4.39	-68.93	0.00
9002	4	10-I-2	0.00	0.00	65.78	1.29	-15.10	0.00
	5		0.00	0.00	-73.82	-0.91	-60.07	0.00
9002	4	10-II-2	0.00	0.00	46.90	-2.75	-5.60	0.00
	5		0.00	0.00	-65.33	-3.79	-67.24	0.00
9002	4	10-I-3	0.00	0.00	67.98	1.99	-17.23	0.00
	5		0.00	0.00	-73.91	-0.32	-58.48	0.00
9002	4	10-II-3	0.00	0.00	44.70	-3.45	-3.47	0.00
	5		0.00	0.00	-65.23	-4.39	-68.83	0.00
9002	4	10-I-4	0.00	0.00	69.66	2.62	-19.31	0.00
	5		0.00	0.00	-73.61	0.26	-56.77	0.00
9002	4	10-II-4	0.00	0.00	43.03	-4.08	-1.39	0.00
	5		0.00	0.00	-65.53	-4.97	-70.53	0.00
9002	5	6	0.00	0.00	74.02	2.58	-71.21	0.00
	6		0.00	0.00	-57.14	0.91	-9.81	0.00
9002	5	7	0.00	0.00	70.61	2.37	-64.92	0.00
	6		0.00	0.00	-56.94	0.73	-10.40	0.00
9002	5	8	0.00	0.00	69.57	2.35	-63.65	0.00
	6		0.00	0.00	-56.34	0.73	-10.35	0.00
9002	5	9-I-1	0.00	0.00	75.98	1.51	-77.49	0.00
	6		0.00	0.00	-57.61	-0.22	-0.47	0.00
9002	5	9-II-1	0.00	0.00	63.16	3.20	-49.81	0.00
	6		0.00	0.00	-55.07	1.68	-20.23	0.00
9002	5	9-I-2	0.00	0.00	76.14	1.87	-78.59	0.00
	6		0.00	0.00	-56.10	0.18	0.81	0.00
9002	5	9-II-2	0.00	0.00	63.00	2.84	-48.72	0.00
	6		0.00	0.00	-56.58	1.28	-21.51	0.00
9002	5	9-I-3	0.00	0.00	76.17	2.09	-79.49	0.00
	6		0.00	0.00	-55.05	0.44	1.95	0.00
9002	5	9-II-3	0.00	0.00	62.97	2.61	-47.82	0.00
	6		0.00	0.00	-57.63	1.02	-22.65	0.00
9002	5	9-I-4	0.00	0.00	76.13	1.86	-78.64	0.00
	6		0.00	0.00	-56.52	0.17	0.81	0.00
9002	5	9-II-4	0.00	0.00	63.01	2.85	-48.67	0.00
	6		0.00	0.00	-56.16	1.29	-21.51	0.00
9002	5	10-I-1	0.00	0.00	73.73	0.32	-58.38	0.00
	6		0.00	0.00	-67.85	-1.98	-17.21	0.00
9002	5	10-II-1	0.00	0.00	65.41	4.39	-68.93	0.00
	6		0.00	0.00	-44.83	3.44	-3.49	0.00
9002	5	10-I-2	0.00	0.00	73.61	-0.26	-56.78	0.00
	6		0.00	0.00	-69.65	-2.62	-19.30	0.00
9002	5	10-II-2	0.00	0.00	65.53	4.97	-70.53	0.00
	6		0.00	0.00	-43.03	4.08	-1.40	0.00
9002	5	10-I-3	0.00	0.00	73.91	0.32	-58.48	0.00
	6		0.00	0.00	-67.98	-1.99	-17.23	0.00
9002	5	10-II-3	0.00	0.00	65.23	4.39	-68.83	0.00
	6		0.00	0.00	-44.70	3.45	-3.47	0.00
9002	5	10-I-4	0.00	0.00	73.81	0.91	-60.06	0.00
	6		0.00	0.00	-65.78	-1.29	-15.10	0.00
9002	5	10-II-4	0.00	0.00	65.33	3.79	-67.24	0.00
	6		0.00	0.00	-46.90	2.75	-5.60	0.00
9003	5	6	0.00	0.00	72.52	0.00	-0.31	0.00
	2		0.00	0.00	-81.02	-0.00	-25.41	0.00
9003	5	7	0.00	0.00	70.28	0.00	-0.34	0.00
	2		0.00	0.00	-78.54	-0.00	-24.77	0.00
9003	5	8	0.00	0.00	69.58	0.00	-0.31	0.00

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 41 di 103

Asta	N.in.	Comb.	N	Ty	Tz	Mt	My	Mz
	2		0.00	0.00	-77.76	-0.00	-24.50	0.00
9003	5	9-I-1	0.00	0.00	69.58	0.28	-0.31	0.00
	2		0.00	0.00	-77.76	-0.06	-24.50	0.00
9003	5	9-II-1	0.00	0.00	69.58	-0.28	-0.31	0.00
	2		0.00	0.00	-77.76	0.06	-24.50	0.00
9003	5	9-I-2	0.00	0.00	69.68	0.21	-0.42	0.00
	2		0.00	0.00	-77.66	-0.09	-24.38	0.00
9003	5	9-II-2	0.00	0.00	69.48	-0.21	-0.21	0.00
	2		0.00	0.00	-77.86	0.09	-24.62	0.00
9003	5	9-I-3	0.00	0.00	69.58	0.15	-0.31	0.00
	2		0.00	0.00	-77.76	-0.16	-24.50	0.00
9003	5	9-II-3	0.00	0.00	69.58	-0.15	-0.31	0.00
	2		0.00	0.00	-77.76	0.16	-24.50	0.00
9003	5	9-I-4	0.00	0.00	69.48	0.21	-0.21	0.00
	2		0.00	0.00	-77.86	-0.09	-24.62	0.00
9003	5	9-II-4	0.00	0.00	69.68	-0.21	-0.42	0.00
	2		0.00	0.00	-77.66	0.09	-24.38	0.00
9003	5	10-I-1	0.00	0.00	65.99	-0.00	12.54	0.00
	2		0.00	0.00	-81.01	-0.00	-38.44	0.00
9003	5	10-II-1	0.00	0.00	73.16	0.00	-13.17	0.00
	2		0.00	0.00	-74.51	0.00	-10.57	0.00
9003	5	10-I-2	0.00	0.00	66.12	0.18	12.24	0.00
	2		0.00	0.00	-80.98	0.18	-38.15	0.00
9003	5	10-II-2	0.00	0.00	73.03	-0.18	-12.87	0.00
	2		0.00	0.00	-74.54	-0.18	-10.85	0.00
9003	5	10-I-3	0.00	0.00	66.08	0.00	12.52	0.00
	2		0.00	0.00	-81.11	-0.00	-38.50	0.00
9003	5	10-II-3	0.00	0.00	73.07	-0.00	-13.14	0.00
	2		0.00	0.00	-74.41	0.00	-10.51	0.00
9003	5	10-I-4	0.00	0.00	66.12	-0.18	12.24	0.00
	2		0.00	0.00	-80.98	-0.18	-38.15	0.00
9003	5	10-II-4	0.00	0.00	73.03	0.18	-12.87	0.00
	2		0.00	0.00	-74.54	0.18	-10.85	0.00
9004	2	6	0.00	0.00	69.15	3.38	-70.71	0.00
	1		0.00	0.00	-49.44	2.21	-5.75	0.00
9004	2	7	0.00	0.00	65.85	3.19	-64.57	0.00
	1		0.00	0.00	-49.29	2.05	-6.35	0.00
9004	2	8	0.00	0.00	64.86	3.16	-63.30	0.00
	1		0.00	0.00	-48.78	2.03	-6.34	0.00
9004	2	9-I-1	0.00	0.00	58.34	2.88	-47.21	0.00
	1		0.00	0.00	-50.63	1.71	-19.16	0.00
9004	2	9-II-1	0.00	0.00	71.38	3.44	-79.39	0.00
	1		0.00	0.00	-46.93	2.34	6.47	0.00
9004	2	9-I-2	0.00	0.00	58.42	3.41	-48.01	0.00
	1		0.00	0.00	-49.61	2.30	-18.10	0.00
9004	2	9-II-2	0.00	0.00	71.30	2.91	-78.60	0.00
	1		0.00	0.00	-47.95	1.75	5.41	0.00
9004	2	9-I-3	0.00	0.00	58.55	3.80	-49.13	0.00
	1		0.00	0.00	-48.14	2.75	-16.83	0.00
9004	2	9-II-3	0.00	0.00	71.17	2.52	-77.47	0.00
	1		0.00	0.00	-49.42	1.31	4.14	0.00
9004	2	9-I-4	0.00	0.00	58.36	3.42	-48.11	0.00
	1		0.00	0.00	-49.46	2.33	-18.02	0.00
9004	2	9-II-4	0.00	0.00	71.36	2.90	-78.50	0.00
	1		0.00	0.00	-48.11	1.73	5.34	0.00
9004	2	10-I-1	0.00	0.00	60.80	5.28	-67.67	0.00
	1		0.00	0.00	-38.22	4.87	0.17	0.00
9004	2	10-II-1	0.00	0.00	68.92	1.04	-58.93	0.00
	1		0.00	0.00	-59.34	-0.82	-12.86	0.00
9004	2	10-I-2	0.00	0.00	60.81	4.64	-66.12	0.00
	1		0.00	0.00	-40.23	4.13	-1.92	0.00
9004	2	10-II-2	0.00	0.00	68.91	1.68	-60.48	0.00
	1		0.00	0.00	-57.33	-0.08	-10.77	0.00
9004	2	10-I-3	0.00	0.00	60.97	5.28	-67.76	0.00
	1		0.00	0.00	-38.32	4.87	0.16	0.00
9004	2	10-II-3	0.00	0.00	68.75	1.04	-58.85	0.00
	1		0.00	0.00	-59.24	-0.82	-12.85	0.00
9004	2	10-I-4	0.00	0.00	61.16	5.90	-69.42	0.00
	1		0.00	0.00	-36.67	5.56	2.24	0.00
9004	2	10-II-4	0.00	0.00	68.56	0.42	-57.19	0.00
	1		0.00	0.00	-60.89	-1.50	-14.93	0.00
9004	3	6	0.00	0.00	49.44	-2.21	-5.75	0.00
	2		0.00	0.00	-69.15	-3.38	-70.71	0.00
9004	3	7	0.00	0.00	49.29	-2.05	-6.35	0.00
	2		0.00	0.00	-65.85	-3.19	-64.57	0.00
9004	3	8	0.00	0.00	48.78	-2.03	-6.34	0.00

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 42 di 103

Asta	N.in.	Comb.	N	Ty	Tz	Mt	My	Mz
	2		0.00	0.00	-64.86	-3.16	-63.30	0.00
9004	3	9-I-1	0.00	0.00	46.93	-2.34	6.47	0.00
	2		0.00	0.00	-71.38	-3.44	-79.39	0.00
9004	3	9-II-1	0.00	0.00	50.63	-1.71	-19.16	0.00
	2		0.00	0.00	-58.34	-2.88	-47.21	0.00
9004	3	9-I-2	0.00	0.00	48.10	-1.73	5.34	0.00
	2		0.00	0.00	-71.36	-2.90	-78.49	0.00
9004	3	9-II-2	0.00	0.00	49.46	-2.33	-18.03	0.00
	2		0.00	0.00	-58.36	-3.42	-48.11	0.00
9004	3	9-I-3	0.00	0.00	49.42	-1.31	4.14	0.00
	2		0.00	0.00	-71.17	-2.52	-77.47	0.00
9004	3	9-II-3	0.00	0.00	48.14	-2.75	-16.83	0.00
	2		0.00	0.00	-58.55	-3.80	-49.13	0.00
9004	3	9-I-4	0.00	0.00	47.95	-1.75	5.41	0.00
	2		0.00	0.00	-71.30	-2.91	-78.60	0.00
9004	3	9-II-4	0.00	0.00	49.61	-2.30	-18.10	0.00
	2		0.00	0.00	-58.41	-3.41	-48.01	0.00
9004	3	10-I-1	0.00	0.00	38.22	-4.87	0.17	0.00
	2		0.00	0.00	-60.80	-5.28	-67.67	0.00
9004	3	10-II-1	0.00	0.00	59.34	0.82	-12.86	0.00
	2		0.00	0.00	-68.92	-1.04	-58.93	0.00
9004	3	10-I-2	0.00	0.00	36.68	-5.56	2.23	0.00
	2		0.00	0.00	-61.16	-5.90	-69.41	0.00
9004	3	10-II-2	0.00	0.00	60.88	1.50	-14.92	0.00
	2		0.00	0.00	-68.56	-0.42	-57.19	0.00
9004	3	10-I-3	0.00	0.00	38.32	-4.87	0.16	0.00
	2		0.00	0.00	-60.97	-5.28	-67.76	0.00
9004	3	10-II-3	0.00	0.00	59.24	0.82	-12.85	0.00
	2		0.00	0.00	-68.75	-1.04	-58.85	0.00
9004	3	10-I-4	0.00	0.00	40.23	-4.13	-1.92	0.00
	2		0.00	0.00	-60.81	-4.64	-66.12	0.00
9004	3	10-II-4	0.00	0.00	57.33	0.08	-10.77	0.00
	2		0.00	0.00	-68.91	-1.68	-60.48	0.00
9005	6	6	0.00	0.00	54.34	1.69	2.17	0.00
	3		0.00	0.00	-62.65	0.47	-24.65	0.00
9005	6	7	0.00	0.00	54.01	1.72	2.01	0.00
	3		0.00	0.00	-62.26	0.44	-24.63	0.00
9005	6	8	0.00	0.00	53.42	1.70	2.02	0.00
	3		0.00	0.00	-61.59	0.43	-24.34	0.00
9005	6	9-I-1	0.00	0.00	57.68	2.30	4.43	0.00
	3		0.00	0.00	-67.59	0.73	-29.43	0.00
9005	6	9-II-1	0.00	0.00	49.17	1.10	-0.40	0.00
	3		0.00	0.00	-55.58	0.14	-19.24	0.00
9005	6	9-I-2	0.00	0.00	58.36	2.00	1.68	0.00
	3		0.00	0.00	-67.21	0.37	-26.85	0.00
9005	6	9-II-2	0.00	0.00	48.48	1.40	2.35	0.00
	3		0.00	0.00	-55.97	0.50	-21.82	0.00
9005	6	9-I-3	0.00	0.00	58.83	1.88	-0.61	0.00
	3		0.00	0.00	-66.63	0.08	-25.66	0.00
9005	6	9-II-3	0.00	0.00	48.02	1.52	4.64	0.00
	3		0.00	0.00	-56.55	0.78	-23.01	0.00
9005	6	9-I-4	0.00	0.00	58.23	2.02	2.25	0.00
	3		0.00	0.00	-67.11	0.48	-26.93	0.00
9005	6	9-II-4	0.00	0.00	48.62	1.39	1.78	0.00
	3		0.00	0.00	-56.07	0.39	-21.75	0.00
9005	6	10-I-1	0.00	0.00	49.39	5.29	20.95	0.00
	3		0.00	0.00	-64.42	4.00	-44.51	0.00
9005	6	10-II-1	0.00	0.00	57.46	-1.89	-16.92	0.00
	3		0.00	0.00	-58.75	-3.13	-4.17	0.00
9005	6	10-I-2	0.00	0.00	48.68	5.74	24.06	0.00
	3		0.00	0.00	-65.16	4.44	-47.94	0.00
9005	6	10-II-2	0.00	0.00	58.17	-2.34	-20.03	0.00
	3		0.00	0.00	-58.02	-3.58	-0.73	0.00
9005	6	10-I-3	0.00	0.00	49.51	5.30	20.91	0.00
	3		0.00	0.00	-64.55	4.00	-44.58	0.00
9005	6	10-II-3	0.00	0.00	57.34	-1.89	-16.88	0.00
	3		0.00	0.00	-58.63	-3.14	-4.09	0.00
9005	6	10-I-4	0.00	0.00	50.33	4.72	17.18	0.00
	3		0.00	0.00	-63.75	3.43	-40.50	0.00
9005	6	10-II-4	0.00	0.00	56.52	-1.31	-13.15	0.00
	3		0.00	0.00	-59.43	-2.56	-8.18	0.00

Risultati Analisi Dinamica - Sollecitazioni massime - Involuppi - Pilastrini - S.L.E
Scenario di calcolo: ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO

Asta	N.in. N.fin.	N kN	Ty kN	Tz kN	Mt kN*m	My kN*m	Mz kN*m
1	1	-118.95 (10-II-4)	-7.68 (9-II-1)	14.15 (10-I-4)	0.37 (10-II-4)	-33.55 (10-I-4)	-12.87 (9-II-1)
	101	-103.95 (10-II-4)	-7.68 (9-II-1)	14.15 (10-I-4)	0.37 (10-II-4)	23.05 (10-I-4)	17.86 (9-II-1)
2	2	-219.31 (6)	15.26 (9-I-1)	7.08 (10-I-3)	-0.37 (10-I-4)	-15.78 (10-I-3)	32.19 (9-I-1)
	102	-204.31 (6)	15.26 (9-I-1)	7.08 (10-I-3)	-0.37 (10-I-4)	12.54 (10-I-3)	-28.84 (9-I-1)
3	3	-118.94 (10-II-2)	7.68 (9-I-1)	14.15 (10-I-2)	-0.37 (10-I-4)	-33.54 (10-I-2)	12.87 (9-I-1)
	103	-103.94 (10-II-2)	7.68 (9-I-1)	14.15 (10-I-2)	-0.37 (10-I-4)	23.05 (10-I-2)	-17.86 (9-I-1)
4	4	-118.38 (10-I-4)	-7.28 (9-II-3)	-14.39 (10-II-4)	-0.37 (10-I-4)	34.35 (10-II-4)	12.36 (9-I-3)
	104	-103.38 (10-I-4)	-7.28 (9-II-3)	-14.39 (10-II-4)	-0.37 (10-I-4)	-23.20 (10-II-4)	17.14 (9-II-3)
5	5	-220.56 (6)	15.07 (9-I-3)	-6.91 (10-II-1)	-0.37 (10-I-4)	15.37 (10-II-1)	31.81 (9-I-3)
	105	-205.56 (6)	15.07 (9-I-3)	-6.91 (10-II-1)	-0.37 (10-I-4)	-12.28 (10-II-1)	-28.47 (9-I-3)
6	6	-118.37 (10-I-2)	7.28 (9-I-3)	-14.39 (10-II-2)	0.37 (10-II-4)	34.35 (10-II-2)	-12.36 (9-II-3)
	106	-103.37 (10-I-2)	7.28 (9-I-3)	-14.39 (10-II-2)	0.37 (10-II-4)	-23.20 (10-II-2)	-17.14 (9-I-3)

Risultati Analisi Dinamica - Sollecitazioni massime - Involuppi - Travi - S.L.E
Scenario di calcolo: ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO

Asta	N.in. N.fin.	N kN	Ty kN	Tz kN	Mt kN*m	My kN*m	Mz kN*m
101	101	0	-2.29 (10-II-4)	-20.70 (10-II-4)	-1.05 (10-II-4)	23.36 (10-II-4)	-1.14 (10-II-4)
	104	0	2.09 (10-I-4)	20.80 (10-I-4)	0.96 (10-I-4)	23.38 (10-I-4)	-1.04 (10-I-4)
102	104	0	6.45 (6)	-37.45 (9-II-4)	2.98 (6)	22.51 (9-II-3)	3.23 (6)
	105	0	-7.83 (9-II-3)	53.39 (9-I-3)	-3.61 (9-II-3)	51.37 (9-I-3)	3.92 (9-II-3)
102	105	0	7.83 (9-I-3)	-53.39 (9-II-3)	3.61 (9-I-3)	51.37 (9-II-3)	3.92 (9-I-3)
	106	0	-6.45 (6)	37.45 (9-I-2)	-2.98 (6)	22.51 (9-I-3)	3.23 (6)
103	105	0	0.01 (10-I-4)	-14.95 (10-I-3)	0.05 (10-I-4)	19.79 (10-I-3)	0.03 (10-I-4)
	102	0	0.01 (10-I-4)	14.77 (10-II-3)	-0.05 (10-II-4)	19.21 (10-II-1)	-0.03 (10-I-4)
104	102	0	7.91 (9-II-1)	-53.25 (9-I-1)	3.64 (9-II-1)	50.84 (9-I-1)	3.95 (9-II-1)
	101	0	-6.42 (6)	37.83 (9-II-4)	-2.96 (6)	23.09 (9-II-1)	3.21 (6)
104	103	0	6.42 (6)	-37.83 (9-I-2)	2.96 (6)	23.09 (9-I-1)	3.21 (6)
	102	0	-7.91 (9-I-1)	53.25 (9-II-1)	-3.64 (9-I-1)	50.84 (9-II-1)	3.95 (9-I-1)
105	106	0	-2.09 (10-I-2)	-20.80 (10-I-2)	-0.96 (10-I-2)	23.37 (10-I-2)	-1.04 (10-I-2)
	103	0	2.29 (10-II-2)	20.70 (10-II-2)	1.05 (10-II-2)	23.36 (10-II-2)	-1.14 (10-II-2)

Verifiche stato limite ultimo

Verifica delle travi

Scenario di calcolo: ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO

Simbologia:

Terreno Nome della stratigrafia per travi Winkler
L [cm] Lunghezza teorica elemento (distanza tra i nodi)
Ln [cm] Lunghezza netta elemento (tiene conto dei conci rigidi)
L2,L3 [cm] Lunghezze libere di inflessione
Sez. R: Sezione Rettangolare
By[cm]: Larghezza (asse locale y)

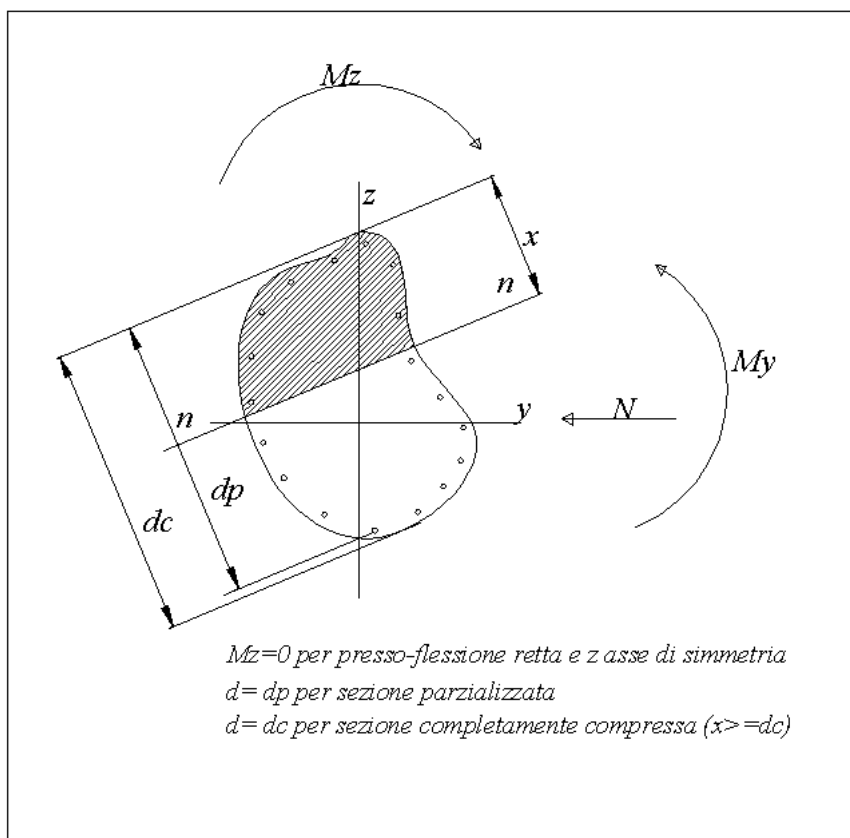
Bz[cm]: Larghezza (asse locale z)
Sez. T: Sezione a T (rovescia e non)
Ba[cm]: Larghezza base inferiore
Ha[cm]: Altezza inferiore
Bs[cm]: Larghezza superiore
Hs[cm]: Altezza superiore
Sez. L: Sezione ad L (rovescia e non)
Ba[cm]: Larghezza base inferiore
Ha[cm]: Altezza inferiore
Bs[cm]: Larghezza superiore
Hs[cm]: Altezza superiore
Sez. C: Sezione circolare
R[cm]: Raggio
Sez. G: Sezione generica
B[cm]: Larghezza
H[cm]: Altezza
Fatt.Ampl.Sisma Fattore moltiplicativo di gruppo per le azioni sismiche (solo se diverso da 1.0)
X [cm] Punto di verifica
ILN Inizio luce netta
CAMP Punto di massimo momento sia superiore che inferiore ad esclusione degli estremi
FLN Fine luce netta
M- [kN*m] Momento negativo massimo di calcolo⁽¹⁾
N- [kN] Sforzo normale corrispondente ad M-
M+ [kN*m] Momento positivo massimo di calcolo⁽¹⁾
N+ [kN] Sforzo normale corrispondente ad M+
ΔM- [kN*m] Incremento di M- per la traslazione del diagramma del momento a causa del taglio
ΔM+ [kN*m] Incremento di M+ per la traslazione del diagramma del momento a causa del taglio
Afs [cmq] Area di ferro superiore
Afi [cmq] Area di ferro inferiore
εsc- Deformazione nel cls per effetto di M-:N-⁽⁴⁾
εsc+ Deformazione nel cls per effetto di M+:N+⁽⁴⁾
εsf- Deformazione nell'acciaio per effetto di M-:N-⁽⁴⁾
εsf+ Deformazione nell'acciaio per effetto di M+:N+⁽⁴⁾
C- Combinazione di carico generatore di M-:N-
C+ Combinazione di carico generatore di M+:N+
x- [cm] Profondità asse neutro per la combinazione C-⁽⁵⁾
d- [cm] Altezza utile della sezione per la combinazione C-⁽⁶⁾
x+ [cm] Profondità asse neutro per la combinazione C+⁽⁵⁾
d+ [cm] Altezza utile della sezione per la combinazione C+⁽⁶⁾
Mr- [kN*m] Momento resistente superiore
Mr+ [kN*m] Momento resistente inferiore
Stato- Stato della sezione per la combinazione C-⁽⁷⁾
Stato+ Stato della sezione per la combinazione C+⁽⁷⁾
Comb Combinazione di carico: quando Comb non è sismica è individuata dal codice [C], quando è sismica è individuata dal codice [(Cx+Cy) Cm Sc].
- C Individua la Combinazione di Carico non sismica (1, 2, ecc. come da scenario);
- Cx Individua la Combinazione di Carico sismica in direzione x (SismaX, come da scenario);
- Cy Individua la Combinazione di Carico sismica in direzione y (SismaY, come da scenario);
- Cm Individua la Combinazione spostamento masse (I, II, III, IV, V, ecc. come da Combinazioni Sisma in Spostamento masse impalcato);
- Sc Individua la sottocombinazione ottenuta mediante la permutazione dei segni (1, 2, 3, 4, 5, 6, 7, 8):
1) Sc = + SismaZ*fx + SismaX*fx + SismaY*fy
2) Sc = + SismaZ*fx + SismaX*fx - SismaY*fy
3) Sc = + SismaZ*fx - SismaX*fx + SismaY*fy
4) Sc = + SismaZ*fx - SismaX*fx - SismaY*fy.
5) Sc = - SismaZ*fx + SismaX*fx + SismaY*fy
6) Sc = - SismaZ*fx + SismaX*fx - SismaY*fy
7) Sc = - SismaZ*fx - SismaX*fx + SismaY*fy
8) Sc = - SismaZ*fx - SismaX*fx - SismaY*fy.
Le ultime quattro sono assenti quando non è richiesto il contributo del sisma in direzione verticale. Le combinazioni delle azioni sismiche così ottenute vengono combinate con i carichi verticali (come da scenario).
Sez Sezione di verifica [Sinistra/Destra]
Td [kN] Taglio di verifica⁽²⁾
VRdns [kN] Resistenza a taglio in assenza di armature
VRcd [kN] Resistenza taglio-compressione calcestruzzo
VRsd [kN] Resistenza taglio-trazione acciaio
VRd [kN] Resistenza a taglio =min(VRcd,VRsd)
VRd,f [kN] Resistenza a taglio dovuta alla resistenza a trazione del calcestruzzo ad alte prestazioni (quando presente)(cfr. eq 4.2 CNR204/2006), oppure resistenza rinforzo del composito (quando presente)(cfr. eq 4.19 CNR200/2013), oppure resistenza rinforzo della camicia in acciaio (quando presente)(cfr. eq C8.7.4.5 Circolare NTC)
Mt [kN*m] Momento torcente
Tpl [kN] Taglio dovuto ai momenti resistenti alle estremità della trave
Mr [kN*m] Momento resistente (ultimo) utilizzato per il calcolo di Tpl quando richiesto
Dx [cm] Distanza dall'estremo da armare con staffe
Staffe [cmq] Area delle staffe
cot(θ) secondo il punto 4.1.2.3.5 delle Norme Tecniche
F.Par. [cmq] Area armatura longitudinale di parete⁽³⁾
Cs Coefficiente di sicurezza definito dal rapporto Fr/Fd (Fr=resistenza,Fd=azione)
ζs Livello di sicurezza sismico definito come rapporto tra l'accelerazione sopportabile e l'accelerazione di progetto, quando richiesto dal criterio di verifica

Verifiche duttilità (quando richieste):

Zona	Sezione di verifica dell'elemento
Comb.	Combinazione di verifica
Nmax [kN]	Sforzo Normale massimo
Dir	Direzione di flessione (pilastri=Y o Z, travi =Z, pareti= ortogonale alla base)
Mry [kN*m]	Momento di snervamento corrispondente a Nmax
MrU [kN*m]	Momento ultimo (resistente) corrispondente a Nmax sulla sezione depurata del calcestruzzo non confinato, considerando il confinamento
ϕ_y [1/m]	Curvatura allo snervamento ($\phi_y = MrU/Mry * \phi'_y$)
ϕ_u [1/m]	Curvatura allo corrispondente a MrU
μ	Capacità in duttilità della sezione
F.Conf	Fattore di confinamento adottato (= $f_{ck,c}/f_{ck}$)
μ_d	Richiesta in duttilità della sezione
Cs	Livello di sicurezza ($Cs = \mu/\mu_d$)

Note Verifica travi:

- (1) il valore del momento di verifica è dato da $M + \Delta M$
- (2) T_d è il valore di verifica a taglio esso è calcolato in funzione della somma tra taglio da carichi verticali il valore di T_{pl} ovvero quando la trave è tozza amplificando il taglio di calcolo dovuto al sisma per il fattore di comportamento
- (3) armatura necessaria per la sola verifica a torsione
- (4) le deformazioni sono stampate a meno del fattore 10^{-3}
- (5) distanza tra la fibra di cls compressa più lontana e l'asse neutro in direzione ortogonale all'asse neutro
- (6) distanza tra le fibre sollecitate più lontane dall'asse neutro: nel caso di sezione parzializzata le due fibre sono quella di cls compresso e quella dell'acciaio teso più lontane da n-n, mentre nel caso di sezione completamente compressa le due fibre sono le due di cls compresso più lontane da n-n
- (7) Indica lo stato della sezione se: completamente compressa (Compr.), completamente tesa (Tesa), parzializzata (Parz.)



Schema geometrico verifica della sezione

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 46 di 103

Trave: 101 [101,104], Pilastrate [1,4] Sez. R: By=30.00 cm Bz=50.00 cm L=600.00 cm Ln=600.00 cm Criterio :
CLS_TraviAlte_ND - Verifica a flessione, $\zeta_e=3.167$ [(4+5)-V-3] : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	47.61	27.36	--	--	8.04	8.04	129.53	129.53	(4+5)-XI-4	(4+5)-XI-1	2.7
60.00	26.39	19.30	--	--	8.04	8.04	129.53	129.53	(4+5)-XI-4	(4+5)-XI-1	4.9
CAMP	--	16.36	--	--	8.04	8.04	129.53	129.53	(4+5)-I-4	(4+5)-V-2	7.9
540.00	26.45	19.54	--	--	8.04	8.04	129.53	129.53	(4+5)-V-3	(4+5)-V-2	4.9
FLN	47.79	27.65	--	--	8.04	8.04	129.53	129.53	(4+5)-V-3	(4+5)-V-2	2.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	12.01	45.40	0.264	11.93	45.40	0.263	129.53	129.53	(4+5)-XI-4	(4+5)-XI-1	Parz.	Parz.
60.00	11.93	45.40	0.263	11.90	45.40	0.262	129.53	129.53	(4+5)-XI-4	(4+5)-XI-1	Parz.	Parz.
CAMP	--	--	--	11.89	45.40	0.262	129.53	129.53	(4+5)-I-4	(4+5)-V-2	--	Parz.
540.00	11.93	45.40	0.263	11.90	45.40	0.262	129.53	129.53	(4+5)-V-3	(4+5)-V-2	Parz.	Parz.
FLN	12.01	45.40	0.264	11.93	45.40	0.263	129.53	129.53	(4+5)-V-3	(4+5)-V-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=(4+5)-XI-4 Cen=(4+5)-V-3 Des=(4+5)-V-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	36.49	--	447.31	401.84	401.84	0.00	129.53	61.00	10.05	11
Cen	18.29	--	447.31	182.65	182.65	--	--	--	4.57	10.0
Des	36.69	--	447.31	401.84	401.84	0.00	129.53	61.00	10.05	11

Trave: 102 [104,105], Pilastrate [4,5] Sez. R: By=30.00 cm Bz=50.00 cm L=600.00 cm Ln=600.00 cm Criterio :
CLS_TraviAlte_ND - Verifica a flessione, $\zeta_e=3.387$ [(4+5)-X-1] : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	33.82	1.40	--	--	8.04	8.04	129.53	129.53	(4+5)-VII-3	(4+5)-VII-2	3.8
60.00	9.41	12.39	--	--	8.04	8.04	129.53	129.53	(4+5)-VII-3	(4+5)-VII-2	10
CAMP	--	27.22	--	--	8.04	8.04	129.53	129.53	(4+5)-I-4		2 4.8
540.00	33.76	--	--	--	8.04	8.04	129.53	129.53	(4+5)-X-1	(4+5)-X-4	3.8
FLN	68.37	--	--	--	8.04	8.04	129.53	129.53	(4+5)-X-1	(4+5)-X-4	1.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	11.96	45.40	0.263	11.84	45.40	0.261	129.53	129.53	(4+5)-VII-3	(4+5)-VII-2	Parz.	Parz.
60.00	11.87	45.40	0.261	11.88	45.40	0.262	129.53	129.53	(4+5)-VII-3	(4+5)-VII-2	Parz.	Parz.
CAMP	--	--	--	11.93	45.40	0.263	129.53	129.53	(4+5)-I-4	2	--	Parz.
540.00	11.95	45.40	0.263	--	--	--	129.53	129.53	(4+5)-X-1	(4+5)-X-4	Parz.	--
FLN	12.09	45.40	0.266	--	--	--	129.53	129.53	(4+5)-X-1	(4+5)-X-4	Parz.	--

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=2 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	51.09	--	447.31	430.10	430.10	0.00	129.53	66.00	10.76	8.4
Cen	45.01	--	447.31	184.33	184.33	--	--	--	4.61	4.1
Des	74.00	--	447.31	430.10	430.10	0.00	129.53	66.00	10.76	5.8

Trave: 102 [105,106], Pilastrate [5,6] Sez. R: By=30.00 cm Bz=50.00 cm L=600.00 cm Ln=600.00 cm Criterio :
CLS_TraviAlte_ND - Verifica a flessione, $\zeta_e=3.387$ [(4+5)-VII-2] : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	68.37	--	--	--	8.04	8.04	129.53	129.53	(4+5)-VII-3	(4+5)-VII-2	1.9
60.00	33.76	--	--	--	8.04	8.04	129.53	129.53	(4+5)-VII-3	(4+5)-VII-2	3.8
CAMP	--	27.22	--	--	8.04	8.04	129.53	129.53	(4+5)-X-1	2	4.8
540.00	9.41	12.39	--	--	8.04	8.04	129.53	129.53	(4+5)-X-1	(4+5)-X-4	10
FLN	33.82	1.40	--	--	8.04	8.04	129.53	129.53	(4+5)-X-1	(4+5)-X-4	3.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kN*m	kN*m				

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021
Pagina 47 di 103

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
ILN	12.09	45.40	0.266	--	--	--	129.53	129.53	(4+5)-VII-3	(4+5)-VII-2	Parz.	--
60.00	11.95	45.40	0.263	--	--	--	129.53	129.53	(4+5)-VII-3	(4+5)-VII-2	Parz.	--
CAMP	--	--	--	11.93	45.40	0.263	129.53	129.53	(4+5)-X-1	2	--	Parz.
540.00	11.87	45.40	0.261	11.88	45.40	0.262	129.53	129.53	(4+5)-X-1	(4+5)-X-4	Parz.	Parz.
FLN	11.96	45.40	0.263	11.84	45.40	0.261	129.53	129.53	(4+5)-X-1	(4+5)-X-4	Parz.	Parz.

Verifica a taglio: cot(0) Sin=2.500,cot(0) Cen=2.500,cot(0) Des=2.500 Comb: Sin=2 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	74.00	--	447.31	430.10	430.10	0.00	129.53	66.00	10.76	5.8
Cen	45.01	--	447.31	184.33	184.33	--	--	--	4.61	4.1
Des	51.09	--	447.31	430.10	430.10	0.00	129.53	66.00	10.76	8.4

Trave: 103 [105,102], Pilastrate [5,2] Sez. R: By=70.00 cm Bz=25.00 cm L=600.00 cm Ln=600.00 cm Criterio :
CLS_TraviSpessore_ND - Verifica a flessione, $\zeta_e=5.931$ [(4+5)-V-1] : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	28.39	--	--	--	14.07	14.07	96.59	96.59	(4+5)-V-1	(4+5)-V-4	3.4
60.00	18.49	3.65	--	--	14.07	14.07	96.59	96.59	(4+5)-V-1	(4+5)-V-4	5.2
CAMP	10.16	6.92	--	--	14.07	14.07	96.59	96.59	(4+5)-V-1	1	9.5
540.00	17.99	4.04	--	--	14.07	14.07	96.59	96.59	(4+5)-V-4	(4+5)-V-1	5.4
FLN	27.78	--	--	--	14.07	14.07	96.59	96.59	(4+5)-V-4	(4+5)-V-1	3.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	6.86	20.40	0.337	--	--	--	96.59	96.59	(4+5)-V-1	(4+5)-V-4	Parz.	--
60.00	6.83	20.40	0.335	6.78	20.40	0.332	96.59	96.59	(4+5)-V-1	(4+5)-V-4	Parz.	Parz.
CAMP	6.80	20.40	0.333	6.79	20.40	0.333	96.59	96.59	(4+5)-V-1	1	Parz.	Parz.
540.00	6.83	20.40	0.335	6.78	20.40	0.332	96.59	96.59	(4+5)-V-4	(4+5)-V-1	Parz.	Parz.
FLN	6.86	20.40	0.336	--	--	--	96.59	96.59	(4+5)-V-4	(4+5)-V-1	Parz.	--

Verifica a taglio: cot(0) Sin=2.500,cot(0) Cen=2.500,cot(0) Des=2.500 Comb: Sin=(4+5)-V-1 Cen=(4+5)-V-1 Des=(4+5)-V-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	17.82	--	468.99	361.12	361.12	0.00	96.59	65.00	20.11	20
Cen	12.57	--	468.99	228.78	228.78	--	--	--	12.74	18
Des	17.63	--	468.99	361.12	361.12	0.00	96.59	65.00	20.11	20

Trave: 104 [102,101], Pilastrate [2,1] Sez. R: By=30.00 cm Bz=50.00 cm L=600.00 cm Ln=600.00 cm Criterio :
CLS_TraviAlte_ND - Verifica a flessione, $\zeta_e=3.392$ [(4+5)-IV-3] : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	67.89	--	--	--	8.04	8.04	129.53	129.53	(4+5)-IV-2	(4+5)-IV-3	1.9
60.00	33.34	--	--	--	8.04	8.04	129.53	129.53	(4+5)-IV-2	(4+5)-IV-3	3.9
CAMP	--	27.30	--	--	8.04	8.04	129.53	129.53	(4+5)-I-4	2	4.7
540.00	9.91	12.29	--	--	8.04	8.04	129.53	129.53	(4+5)-I-4	(4+5)-I-1	11
FLN	34.58	1.14	--	--	8.04	8.04	129.53	129.53	(4+5)-I-4	(4+5)-I-1	3.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	12.08	45.40	0.266	--	--	--	129.53	129.53	(4+5)-IV-2	(4+5)-IV-3	Parz.	--
60.00	11.95	45.40	0.263	--	--	--	129.53	129.53	(4+5)-IV-2	(4+5)-IV-3	Parz.	--
CAMP	--	--	--	11.93	45.40	0.263	129.53	129.53	(4+5)-I-4	2	--	Parz.
540.00	11.87	45.40	0.261	11.88	45.40	0.262	129.53	129.53	(4+5)-I-4	(4+5)-I-1	Parz.	Parz.
FLN	11.96	45.40	0.263	11.84	45.40	0.261	129.53	129.53	(4+5)-I-4	(4+5)-I-1	Parz.	Parz.

Verifica a taglio: cot(0) Sin=2.500,cot(0) Cen=2.500,cot(0) Des=2.500 Comb: Sin=2 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	73.73	--	447.31	430.10	430.10	0.00	129.53	66.00	10.76	5.8
Cen	44.77	--	447.31	184.33	184.33	--	--	--	4.61	4.1
Des	51.60	--	447.31	430.10	430.10	0.00	129.53	66.00	10.76	8.3

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 48 di 103

Trave: 104 [103,102], Pilastrate [3,2] Sez. R: By=30.00 cm Bz=50.00 cm L=600.00 cm Ln=600.00 cm Criterio :
CLS_TraviAlte_ND - Verifica a flessione, $\zeta_e=3.392$ [(4+5)-I-1] : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	34.58	1.14	--	--	8.04	8.04	129.53	129.53	(4+5)-IV-2	(4+5)-IV-3	3.7
60.00	9.91	12.29	--	--	8.04	8.04	129.53	129.53	(4+5)-IV-2	(4+5)-IV-3	11
CAMP	--	27.30	--	--	8.04	8.04	129.53	129.53	(4+5)-II-1	2	4.7
540.00	33.34	--	--	--	8.04	8.04	129.53	129.53	(4+5)-I-4	(4+5)-I-1	3.9
FLN	67.89	--	--	--	8.04	8.04	129.53	129.53	(4+5)-I-4	(4+5)-I-1	1.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	11.96	45.40	0.263	11.84	45.40	0.261	129.53	129.53	(4+5)-IV-2	(4+5)-IV-3	Parz.	Parz.
60.00	11.87	45.40	0.261	11.88	45.40	0.262	129.53	129.53	(4+5)-IV-2	(4+5)-IV-3	Parz.	Parz.
CAMP	--	--	--	11.93	45.40	0.263	129.53	129.53	(4+5)-II-1	2	--	Parz.
540.00	11.95	45.40	0.263	--	--	--	129.53	129.53	(4+5)-I-4	(4+5)-I-1	Parz.	--
FLN	12.08	45.40	0.266	--	--	--	129.53	129.53	(4+5)-I-4	(4+5)-I-1	Parz.	--

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=2 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	51.60	--	447.31	430.10	430.10	0.00	129.53	66.00	10.76	8.3
Cen	44.77	--	447.31	184.33	184.33	--	--	--	4.61	4.1
Des	73.73	--	447.31	430.10	430.10	0.00	129.53	66.00	10.76	5.8

Trave: 105 [106,103], Pilastrate [6,3] Sez. R: By=30.00 cm Bz=50.00 cm L=600.00 cm Ln=600.00 cm Criterio :
CLS_TraviAlte_ND - Verifica a flessione, $\zeta_e=3.168$ [(4+5)-II-1] : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	47.78	27.64	--	--	8.04	8.04	129.53	129.53	(4+5)-II-1	(4+5)-II-4	2.7
60.00	26.45	19.53	--	--	8.04	8.04	129.53	129.53	(4+5)-II-1	(4+5)-II-4	4.9
CAMP	--	16.36	--	--	8.04	8.04	129.53	129.53	(4+5)-X-1	(4+5)-II-4	7.9
540.00	26.38	19.29	--	--	8.04	8.04	129.53	129.53	(4+5)-VIII-2	(4+5)-VIII-3	4.9
FLN	47.60	27.35	--	--	8.04	8.04	129.53	129.53	(4+5)-VIII-2	(4+5)-VIII-3	2.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	12.01	45.40	0.264	11.93	45.40	0.263	129.53	129.53	(4+5)-II-1	(4+5)-II-4	Parz.	Parz.
60.00	11.93	45.40	0.263	11.90	45.40	0.262	129.53	129.53	(4+5)-II-1	(4+5)-II-4	Parz.	Parz.
CAMP	--	--	--	11.89	45.40	0.262	129.53	129.53	(4+5)-X-1	(4+5)-II-4	--	Parz.
540.00	11.93	45.40	0.263	11.90	45.40	0.262	129.53	129.53	(4+5)-VIII-2	(4+5)-VIII-3	Parz.	Parz.
FLN	12.01	45.40	0.264	11.93	45.40	0.263	129.53	129.53	(4+5)-VIII-2	(4+5)-VIII-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=(4+5)-II-1 Cen=(4+5)-II-1 Des=(4+5)-VIII-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	36.68	--	447.31	401.84	401.84	0.00	129.53	61.00	10.05	11
Cen	18.29	--	447.31	182.65	182.65	--	--	--	4.57	10.0
Des	36.48	--	447.31	401.84	401.84	0.00	129.53	61.00	10.05	11

Verifica delle travi di fondazione

Scenario di calcolo: **ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO**

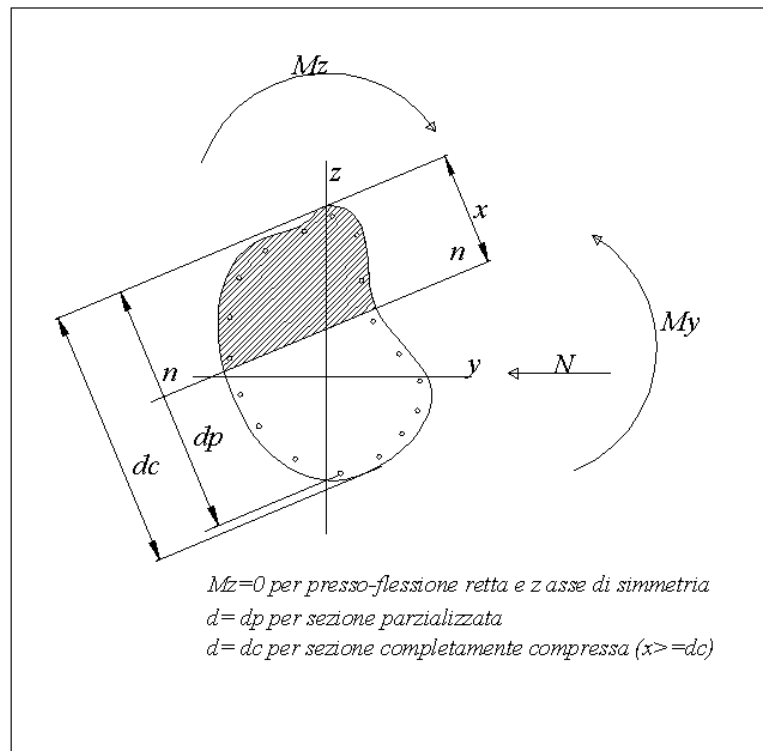
Simbologia:

Terreno Nome della stratigrafia per travi Winkler
L [cm] Lunghezza teorica elemento (distanza tra i nodi)
Ln [cm] Lunghezza netta elemento (tiene conto dei concii rigidi)
L2,L3 [cm] Lunghezze libere di inflessione
Sez. R: Sezione Rettangolare
By[cm]: Larghezza (asse locale y)
Bz[cm]: Larghezza (asse locale z)
Sez. T: Sezione a T (rovescia e non)
Ba[cm]: Larghezza base inferiore
Ha[cm]: Altezza inferiore
Bs[cm]: Larghezza superiore
Hs[cm]: Altezza superiore
Sez. L: Sezione ad L (rovescia e non)
Ba[cm]: Larghezza base inferiore
Ha[cm]: Altezza inferiore
Bs[cm]: Larghezza superiore
Hs[cm]: Altezza superiore
Sez. C: Sezione circolare
R[cm]: Raggio
Sez. G: Sezione generica
B[cm]: Larghezza
H[cm]: Altezza
Fatt.Ampl.Sisma Fattore moltiplicativo di gruppo per le azioni sismiche (solo se diverso da 1.0)
X [cm] Punto di verifica
ILN Inizio luce netta
CAMP Punto di massimo momento sia superiore che inferiore ad esclusione degli estremi
FLN Fine luce netta
M- [kN*m] Momento negativo massimo di calcolo⁽¹⁾
N- [kN] Sforzo normale corrispondente ad M-
M+ [kN*m] Momento positivo massimo di calcolo⁽¹⁾
N+ [kN] Sforzo normale corrispondente ad M+
ΔM- [kN*m] Incremento di M- per la traslazione del diagramma del momento a causa del taglio
ΔM+ [kN*m] Incremento di M+ per la traslazione del diagramma del momento a causa del taglio
Afs [cmq] Area di ferro superiore
Afi [cmq] Area di ferro inferiore
esc- Deformazione nel cls per effetto di M-:N-⁽⁴⁾
esc+ Deformazione nel cls per effetto di M+:N+⁽⁴⁾
esf- Deformazione nell'acciaio per effetto di M-:N-⁽⁴⁾
esf+ Deformazione nell'acciaio per effetto di M+:N+⁽⁴⁾
C- Combinazione di carico generatore di M-:N-
C+ Combinazione di carico generatore di M+:N+
x- [cm] Profondità asse neutro per la combinazione C-⁽⁵⁾
d- [cm] Altezza utile della sezione per la combinazione C-⁽⁶⁾
x+ [cm] Profondità asse neutro per la combinazione C+⁽⁵⁾
d+ [cm] Altezza utile della sezione per la combinazione C+⁽⁶⁾
Mr- [kN*m] Momento resistente superiore
Mr+ [kN*m] Momento resistente inferiore
Stato- Stato della sezione per la combinazione C-⁽⁷⁾
Stato+ Stato della sezione per la combinazione C+⁽⁷⁾
Comb Combinazione di carico: quando Comb non è sismica è individuata dal codice [C], quando è sismica è individuata dal codice [(Cx+Cy) Cm Sc].
- C Individua la Combinazione di Carico non sismica (1, 2, ecc. come da scenario);
- Cx Individua la Combinazione di Carico sismica in direzione x (SismaX, come da scenario);
- Cy Individua la Combinazione di Carico sismica in direzione y (SismaY, come da scenario);
- Cm Individua la Combinazione spostamento masse (I, II, III, IV, V, ecc. come da Combinazioni Sisma in Spostamento masse impalcato);
- Sc Individua la sottocombinazione ottenuta mediante la permutazione dei segni (1, 2, 3, 4, 5, 6, 7, 8):
1) $Sc = + SismaZ*fx + SismaX*fy + SismaY*fy$
2) $Sc = + SismaZ*fx + SismaX*fy - SismaY*fy$
3) $Sc = + SismaZ*fx - SismaX*fy + SismaY*fy$
4) $Sc = + SismaZ*fx - SismaX*fy - SismaY*fy$
5) $Sc = - SismaZ*fx + SismaX*fy + SismaY*fy$
6) $Sc = - SismaZ*fx + SismaX*fy - SismaY*fy$
7) $Sc = - SismaZ*fx - SismaX*fy + SismaY*fy$
8) $Sc = - SismaZ*fx - SismaX*fy - SismaY*fy$
Le ultime quattro sono assenti quando non è richiesto il contributo del sisma in direzione verticale. Le combinazioni delle azioni sismiche così ottenute vengono combinate con i carichi verticali (come da scenario).
Sez Sezione di verifica [Sinistra/Destra]
Td [kN] Taglio di verifica⁽²⁾
VRdns [kN] Resistenza a taglio in assenza di armature
VRcd [kN] Resistenza taglio-compressione calcestruzzo
VRsd [kN] Resistenza taglio-trazione acciaio
VRd [kN] Resistenza a taglio =min(VRcd,VRsd)

VRd,f [kN]	Resistenza a taglio dovuta alla resistenza a trazione del calcestruzzo ad alte prestazioni (quando presente) (cfr. eq 4.2 CNR204/2006), oppure resistenza rinforzo del composito (quando presente) (cfr. eq 4.19 CNR200/2013), oppure resistenza rinforzo della camicia in acciaio (quando presente) (cfr. eq C8.7.4.5 Circolare NTC)
Mt [kN*m]	Momento torcente
Tpl [kN]	Taglio dovuto ai momenti resistenti alle estremità della trave
Mr [kN*m]	Momento resistente (ultimo) utilizzato per il calcolo di Tpl quando richiesto
Dx [cm]	Distanza dall'estremo da armare con staffe
Staffe [cmq]	Area delle staffe
cot(θ)	cot(θ) secondo il punto 4.1.2.3.5 delle Norme Tecniche
F.Par. [cmq]	Area armatura longitudinale di parete ⁽³⁾
Cs	Coefficiente di sicurezza definito dal rapporto Fr/Fd (Fr=resistenza, Fd=azione)
ξs	Livello di sicurezza sismico definito come rapporto tra l'accelerazione sopportabile e l'accelerazione di progetto, quando richiesto dal criterio di verifica
Verifiche duttilità (quando richieste):	
Zona	Sezione di verifica dell'elemento
Comb.	Combinazione di verifica
Nmax [kN]	Sforzo Normale massimo
Dir	Direzione di flessione (pilastri=Y o Z, travi =Z, pareti= ortogonale alla base)
Mry [kN*m]	Momento di snervamento corrispondente a Nmax
MrU [kN*m]	Momento ultimo (resistente) corrispondente a Nmax sulla sezione depurata del calcestruzzo non confinato, considerando il confinamento
φy [1/m]	Curvatura allo snervamento ($\phi_y = M_{rU}/M_{ry} * \phi'_y$)
φu [1/m]	Curvatura allo corrispondente a MrU
μ	Capacità in duttilità della sezione
F.Conf	Fattore di confinamento adottato (= fck,c/fck)
μd	Richiesta in duttilità della sezione
Cs	Livello di sicurezza ($Cs = \mu/\mu_d$)

Note Verifica travi:

- ⁽¹⁾ il valore del momento di verifica è dato da $M + \Delta M$
- ⁽²⁾ Td è il valore di verifica a taglio esso è calcolato in funzione della somma tra taglio da carichi verticali il valore di Tpl ovvero quando la trave è tozza amplificando il taglio di calcolo dovuto al sisma per il fattore di comportamento
- ⁽³⁾ armatura necessaria per la sola verifica a torsione
- ⁽⁴⁾ le deformazioni sono stampate a meno del fattore 10^{-3}
- ⁽⁵⁾ distanza tra la fibra di cls compressa più lontana e l'asse neutro in direzione ortogonale all'asse neutro
- ⁽⁶⁾ distanza tra le fibre sollecitate più lontane dall'asse neutro: nel caso di sezione parzializzata le due fibre sono quella di cls compresso e quella dell'acciaio teso più lontane da n-n, mentre nel caso di sezione completamente compressa le due fibre sono le due di cls compresso più lontane da n-n
- ⁽⁷⁾ Indica lo stato della sezione se: completamente compressa (Compr.), completamente tesa (Tesa), parzializzata (Parz.)



Schema geometrico verifica della sezione

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 51 di 103

Trave di fondazione: 9001 [1,4], Pilastrate [1,4] Sez. T: Ba=100.00 cm Ha=40.00 cm Bs=30.00cm Hs=60.00 cm L=600.00 cm Ln=550.00 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett_ND - Verifica a flessione, $\zeta_E=2.382$ [(4+5)-XI-4] : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	38.75	92.58	40.23	--	6.16	12.32	221.79	423.81	(4+5)-XI-4	(4+5)-V-3	2.8
55.00	64.99	52.56	20.08	40.02	6.16	12.32	221.79	423.81	(4+5)-XI-4	(4+5)-V-3	2.6
CAMP	93.92	15.40	--	75.23	6.16	12.32	221.79	423.81	2	(4+5)-V-3	2.4
495.00	79.67	22.54	8.41	37.44	6.16	12.32	221.79	423.81	(4+5)-XI-3	(4+5)-XI-4	2.5
FLN	59.77	59.98	27.90	--	6.16	12.32	221.79	423.81	(4+5)-XI-3	(4+5)-XI-4	2.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	9.67	95.40	0.101	22.95	95.40	0.241	221.79	423.81	(4+5)-XI-4	(4+5)-V-3	Parz.	Parz.
55.00	9.67	95.40	0.101	22.95	95.40	0.241	221.79	423.81	(4+5)-XI-4	(4+5)-V-3	Parz.	Parz.
CAMP	9.68	95.40	0.101	22.95	95.40	0.241	221.79	423.81	2	(4+5)-V-3	Parz.	Parz.
495.00	9.68	95.40	0.101	22.88	95.40	0.240	221.79	423.81	(4+5)-XI-3	(4+5)-XI-4	Parz.	Parz.
FLN	9.68	95.40	0.101	22.88	95.40	0.240	221.79	423.81	(4+5)-XI-3	(4+5)-XI-4	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=2 Cen=(4+5)-V-3 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	89.28	--	939.94	844.39	844.39	0.00	423.81	101.00	10.05	9.5
Cen	62.38	--	939.94	394.05	394.05	--	--	--	4.69	6.3
Des	77.44	--	939.94	844.39	844.39	0.00	221.79	101.00	10.05	11

Trave di fondazione: 9002 [4,5], Pilastrate [4,5] Sez. T: Ba=100.00 cm Ha=40.00 cm Bs=30.00cm Hs=60.00 cm L=600.00 cm Ln=600.00 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett_ND - Verifica a flessione, $\zeta_E=2.945$ [(4+5)-XI-1] : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	19.21	51.05	45.66	--	6.16	12.32	221.79	423.81	(4+5)-VII-3	(4+5)-X-1	3.4
60.00	44.30	13.40	32.01	37.65	6.16	12.32	221.79	423.81	(4+5)-IV-3	(4+5)-X-1	2.9
CAMP	87.61	25.57	--	76.77	6.16	12.32	221.79	423.81	(4+5)-V-3	(4+5)-X-4	2.5
540.00	8.34	65.29	49.71	46.97	6.16	12.32	221.79	423.81	(4+5)-XI-1	(4+5)-X-4	3.8
FLN	-32.10	112.26	65.38	--	6.16	12.32	221.79	423.81	(4+5)-XI-1	(4+5)-X-4	3.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	9.66	95.40	0.101	22.86	95.40	0.240	221.79	423.81	(4+5)-VII-3	(4+5)-X-1	Parz.	Parz.
60.00	9.67	95.40	0.101	22.86	95.40	0.240	221.79	423.81	(4+5)-IV-3	(4+5)-X-1	Parz.	Parz.
CAMP	9.68	95.40	0.101	22.97	95.40	0.241	221.79	423.81	(4+5)-V-3	(4+5)-X-4	Parz.	Parz.
540.00	9.66	95.40	0.101	22.99	95.40	0.241	221.79	423.81	(4+5)-XI-1	(4+5)-X-4	Parz.	Parz.
FLN	9.64	95.40	0.101	22.99	95.40	0.241	221.79	423.81	(4+5)-XI-1	(4+5)-X-4	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=(4+5)-XI-1 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	93.53	--	939.94	844.39	844.39	0.00	423.81	101.00	10.05	9.0
Cen	66.83	--	939.94	391.60	391.60	--	--	--	4.66	5.9
Des	103.48	--	939.94	844.39	844.39	0.00	221.79	101.00	10.05	8.2

Trave di fondazione: 9002 [5,6], Pilastrate [5,6] Sez. T: Ba=100.00 cm Ha=40.00 cm Bs=30.00cm Hs=60.00 cm L=600.00 cm Ln=600.00 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett_ND - Verifica a flessione, $\zeta_E=4.032$ [(4+5)-VII-2] : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	-32.12	112.25	65.38	--	12.32	12.32	438.09	427.41	(4+5)-VIII-3	(4+5)-VII-2	3.8
60.00	8.32	65.28	49.71	46.97	12.32	12.32	438.09	427.41	(4+5)-VIII-3	(4+5)-VII-2	3.8
CAMP	87.60	25.56	--	76.77	12.32	12.32	438.09	427.41	(4+5)-II-1	(4+5)-VII-2	4.2
540.00	44.30	13.40	32.00	37.64	12.32	12.32	438.09	427.41	(4+5)-I-1	(4+5)-VII-3	5.7
FLN	19.20	51.04	45.67	--	12.32	12.32	438.09	427.41	(4+5)-X-1	(4+5)-VII-3	6.8

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021
Pagina 52 di 103

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	13.40	95.40	0.140	21.73	95.40	0.228	438.09	427.41	(4+5)-VIII-3	(4+5)-VII-2	Parz.	Parz.
60.00	13.42	95.40	0.141	21.73	95.40	0.228	438.09	427.41	(4+5)-VIII-3	(4+5)-VII-2	Parz.	Parz.
CAMP	13.44	95.40	0.141	21.71	95.40	0.228	438.09	427.41	(4+5)-II-1	(4+5)-VII-2	Parz.	Parz.
540.00	13.43	95.40	0.141	21.62	95.40	0.227	438.09	427.41	(4+5)-I-1	(4+5)-VII-3	Parz.	Parz.
FLN	13.42	95.40	0.141	21.62	95.40	0.227	438.09	427.41	(4+5)-X-1	(4+5)-VII-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=2 Cen=2 Des=(4+5)-VIII-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	103.48	--	939.94	844.39	844.39	0.00	427.41	101.00	10.05	8.2
Cen	66.83	--	939.94	391.60	391.60	--	--	--	4.66	5.9
Des	93.51	--	939.94	844.39	844.39	0.00	438.09	101.00	10.05	9.0

Trave di fondazione: 9003 [5,2], Pilastrate [5,2] Sez. T: Ba=100.00 cm Ha=40.00 cm Bs=30.00cm Hs=60.00 cm L=600.00 cm Ln=570.00 cm Terreno=Terrenol Criterio : CLS_TraviFondazione_Rett_ND - Verifica a flessione, $\zeta_E=2.674$ [(4+5)-V-4] : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	-1.06	34.40	85.77	--	6.16	12.32	221.79	423.81	2	(4+5)-V-4	2.6
57.00	50.90	-6.33	60.88	40.74	6.16	12.32	221.79	423.81	2	(4+5)-V-4	2.0
CAMP	130.44	-20.72	--	76.99	6.16	12.32	221.79	423.81	2	(4+5)-V-1	1.7
513.00	22.05	16.38	74.43	45.18	6.16	12.32	221.79	423.81	2	(4+5)-V-1	2.3
FLN	12.56	61.56	55.05	--	6.16	12.32	221.79	423.81	(4+5)-V-4	(4+5)-V-1	3.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	9.67	95.40	0.101	22.83	95.40	0.239	221.79	423.81	2	(4+5)-V-4	Parz.	Parz.
57.00	9.69	95.40	0.102	22.83	95.40	0.239	221.79	423.81	2	(4+5)-V-4	Parz.	Parz.
CAMP	9.70	95.40	0.102	22.87	95.40	0.240	221.79	423.81	2	(4+5)-V-1	Parz.	Parz.
513.00	9.68	95.40	0.101	22.88	95.40	0.240	221.79	423.81	2	(4+5)-V-1	Parz.	Parz.
FLN	9.66	95.40	0.101	22.88	95.40	0.240	221.79	423.81	(4+5)-V-4	(4+5)-V-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=2 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	103.79	--	939.94	844.39	844.39	0.00	423.81	101.00	10.05	8.1
Cen	68.43	--	939.94	383.82	383.82	--	--	--	4.57	5.6
Des	115.95	--	939.94	844.39	844.39	0.00	221.79	101.00	10.05	7.3

Trave di fondazione: 9004 [2,1], Pilastrate [2,1] Sez. T: Ba=100.00 cm Ha=40.00 cm Bs=30.00cm Hs=60.00 cm L=600.00 cm Ln=600.00 cm Terreno=Terrenol Criterio : CLS_TraviFondazione_Rett_ND - Verifica a flessione, $\zeta_E=3.154$ [(4+5)-IV-2] : **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	-14.64	111.96	41.73	--	6.16	12.32	221.79	423.81	(4+5)-IV-2	(4+5)-IV-3	3.8
60.00	3.79	67.51	46.03	44.45	6.16	12.32	221.79	423.81	(4+5)-V-2	(4+5)-IV-3	3.8
CAMP	77.92	29.75	--	72.82	6.16	12.32	221.79	423.81	(4+5)-XI-4	(4+5)-IV-3	2.8
540.00	50.60	14.11	20.41	34.03	6.16	12.32	221.79	423.81	(4+5)-I-4	(4+5)-IV-2	3.1
FLN	24.89	48.14	37.41	--	6.16	12.32	221.79	423.81	(4+5)-I-4	(4+5)-IV-2	3.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	9.64	95.40	0.101	22.99	95.40	0.241	221.79	423.81	(4+5)-IV-2	(4+5)-IV-3	Parz.	Parz.
60.00	9.65	95.40	0.101	22.99	95.40	0.241	221.79	423.81	(4+5)-V-2	(4+5)-IV-3	Parz.	Parz.
CAMP	9.67	95.40	0.101	22.97	95.40	0.241	221.79	423.81	(4+5)-XI-4	(4+5)-IV-3	Parz.	Parz.
540.00	9.67	95.40	0.101	22.86	95.40	0.240	221.79	423.81	(4+5)-I-4	(4+5)-IV-2	Parz.	Parz.
FLN	9.66	95.40	0.101	22.86	95.40	0.240	221.79	423.81	(4+5)-I-4	(4+5)-IV-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=2 Cen=2 Des=(4+5)-V-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	96.51	--	939.94	844.39	844.39	0.00	423.81	101.00	10.05	8.7

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 53 di 103

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
Cen	62.65	--	939.94	391.60	391.60	--	--	--	4.66	6.3
Des	83.15	--	939.94	844.39	844.39	0.00	221.79	101.00	10.05	10

Trave di fondazione: 9004 [3,2], Pilastrate [3,2] Sez. T: Ba=100.00 cm Ha=40.00 cm Bs=30.00cm Hs=60.00 cm L=600.00 cm Ln=600.00 cm Terreno=Terrenol Criterio : CLS_TraviFondazione_Rett_ND - Verifica a flessione, $\zeta_b=4.145 [(4+5)-I-1]$: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	24.89	48.14	37.41	--	12.32	12.32	438.09	427.41	(4+5)-IV-2	(4+5)-I-4	7.0
60.00	44.72	14.11	25.67	34.03	12.32	12.32	438.09	427.41	(4+5)-VII-2	(4+5)-I-4	6.2
CAMP	77.91	29.75	--	72.82	12.32	12.32	438.09	427.41	(4+5)-VIII-2	(4+5)-I-1	4.2
540.00	3.77	67.50	46.04	44.45	12.32	12.32	438.09	427.41	(4+5)-II-4	(4+5)-I-1	3.8
FLN	-14.65	111.96	41.74	--	12.32	12.32	438.09	427.41	(4+5)-I-4	(4+5)-I-1	3.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	13.42	95.40	0.141	21.62	95.40	0.227	438.09	427.41	(4+5)-IV-2	(4+5)-I-4	Parz.	Parz.
60.00	13.43	95.40	0.141	21.62	95.40	0.227	438.09	427.41	(4+5)-VII-2	(4+5)-I-4	Parz.	Parz.
CAMP	13.43	95.40	0.141	21.71	95.40	0.228	438.09	427.41	(4+5)-VIII-2	(4+5)-I-1	Parz.	Parz.
540.00	13.41	95.40	0.141	21.72	95.40	0.228	438.09	427.41	(4+5)-II-4	(4+5)-I-1	Parz.	Parz.
FLN	13.40	95.40	0.140	21.72	95.40	0.228	438.09	427.41	(4+5)-I-4	(4+5)-I-1	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500 Comb: Sin=(4+5)-II-4 Cen=2 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	83.13	--	939.94	844.39	844.39	0.00	427.41	101.00	10.05	10
Cen	62.65	--	939.94	391.60	391.60	--	--	--	4.66	6.3
Des	96.51	--	939.94	844.39	844.39	0.00	438.09	101.00	10.05	8.7

Trave di fondazione: 9005 [6,3], Pilastrate [6,3] Sez. T: Ba=100.00 cm Ha=40.00 cm Bs=30.00cm Hs=60.00 cm L=600.00 cm Ln=550.00 cm Terreno=Terrenol Criterio : CLS_TraviFondazione_Rett_ND - Verifica a flessione, $\zeta_b=3.793 [(4+5)-II-1]$: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	59.76	59.98	27.90	--	12.32	12.32	438.09	427.41	(4+5)-VIII-1	(4+5)-VIII-2	5.0
55.00	79.66	22.53	8.31	37.44	12.32	12.32	438.09	427.41	(4+5)-VIII-1	(4+5)-VIII-2	5.0
CAMP	93.92	15.40	--	75.23	12.32	12.32	438.09	427.41	2	(4+5)-II-1	4.7
495.00	64.98	52.55	20.25	40.02	12.32	12.32	438.09	427.41	(4+5)-VIII-2	(4+5)-II-1	4.6
FLN	38.74	92.57	40.23	--	12.32	12.32	438.09	427.41	(4+5)-VIII-2	(4+5)-II-1	4.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	13.44	95.40	0.141	21.64	95.40	0.227	438.09	427.41	(4+5)-VIII-1	(4+5)-VIII-2	Parz.	Parz.
55.00	13.44	95.40	0.141	21.64	95.40	0.227	438.09	427.41	(4+5)-VIII-1	(4+5)-VIII-2	Parz.	Parz.
CAMP	13.44	95.40	0.141	21.69	95.40	0.227	438.09	427.41	2	(4+5)-II-1	Parz.	Parz.
495.00	13.44	95.40	0.141	21.69	95.40	0.227	438.09	427.41	(4+5)-VIII-2	(4+5)-II-1	Parz.	Parz.
FLN	13.43	95.40	0.141	21.69	95.40	0.227	438.09	427.41	(4+5)-VIII-2	(4+5)-II-1	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=2.500, cot(θ) Cen=2.500, cot(θ) Des=2.500 Comb: Sin=2 Cen=(4+5)-II-1 Des=2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	77.44	--	939.94	844.39	844.39	0.00	427.41	101.00	10.05	11
Cen	62.38	--	939.94	394.05	394.05	--	--	--	4.69	6.3
Des	89.28	--	939.94	844.39	844.39	0.00	438.09	101.00	10.05	9.5

Verifica dei Pilastri

Scenario di calcolo: **ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO**

Simbologia

L [cm]	Lunghezza teorica elemento (distanza tra i nodi)
Ln [cm]	Lunghezza netta elemento (tiene conto dei concii rigidi)
L2,L3 [cm]	Lunghezze libere di inflessione
Sez. R: Sezione	Rettangolare
	By[cm]: Larghezza (asse locale y)
	Bz[cm]: Larghezza (asse locale z)
Sez. T: Sezione	a T (rovescia e non)
	Ba[cm]: Larghezza base inferiore
	Ha[cm]: Altezza inferiore
	Bs[cm]: Larghezza superiore
	Hs[cm]: Altezza superiore
Sez. L: Sezione	ad L (rovescia e non)
	Ba[cm]: Larghezza base inferiore
	Ha[cm]: Altezza inferiore
	Bs[cm]: Larghezza superiore
	Hs[cm]: Altezza superiore
Sez. C: Sezione	circolare
	R[cm]: Raggio
Sez. G: Sezione	generica
	B[cm]: Larghezza
	H[cm]: Altezza
Aspigoli	Area di ferro negli spigoli
Afy	Area di ferro sul lato Y
Afz	Area di ferro sul lato Z
Zona	Punto di verifica
1/N	Distanza dall'inizio della lunghezza netta
Piede	Inizio lunghezza netta
Testa	Fine lunghezza netta
Comb	Combinazione di carico: quando Comb non è sismica è individuata dal codice [(+/-)C], quando è sismica è individuata dal codice [(+/-)(Cx+Cy) Cm Sc], (+/-) rappresenta la eventuale traslazione del diagramma del momento dovuta al taglio, come specificato nel criterio di verifica [positiva (+) o negativa (-)]
- C	Individua la Combinazione di Carico non sismica (1, 2, ecc. come da scenario);
- Cx	Individua la Combinazione di Carico sismica in direzione x (SismaX, come da scenario);
- Cy	Individua la Combinazione di Carico sismica in direzione y (SismaY, come da scenario);
- Cm	Individua la Combinazione spostamento masse (I, II, III, IV, V, ecc. come da Combinazioni Sisma in Spostamento masse impalcato);
- Sc	Individua la sottocombinazione ottenuta mediante la permutazione dei segni (1, 2, 3, 4, 5, 6, 7, 8):
1)	Sc = + SismaZ*fz + SismaX*fx + SismaY*fy
2)	Sc = + SismaZ*fz + SismaX*fx - SismaY*fy
3)	Sc = + SismaZ*fz - SismaX*fx + SismaY*fy
4)	Sc = + SismaZ*fz - SismaX*fx - SismaY*fy.
5)	Sc = - SismaZ*fz + SismaX*fx + SismaY*fy
6)	Sc = - SismaZ*fz + SismaX*fx - SismaY*fy
7)	Sc = - SismaZ*fz - SismaX*fx + SismaY*fy
8)	Sc = - SismaZ*fz - SismaX*fx - SismaY*fy.
Le ultime quattro sono assenti quando non è richiesto il contributo del sisma in direzione verticale. Le combinazioni delle azioni sismiche così ottenute vengono combinate con i carichi verticali (come da scenario).	
N [kN]	Sforzo Normale
N'y [kN]	Sforzo Normale x Omega2
N'z [kN]	Sforzo Normale x Omega3
My [kN*m]	Momento flettente dir Y
M'y [kN*m]	Momento flettente dir Y x cy
cy [kN*m]	Coefficiente moltiplicativo momento flettente dir Y per verifica a carico di punta
cz [kN*m]	Coefficiente moltiplicativo momento flettente dir Z per verifica a carico di punta
Mz [kN*m]	Momento flettente dir Z
M'z [kN*m]	Momento flettente dir Z x cz
εcmax	Deformazione massima cls (1)
εfmax	Deformazione massima acciaio (1)
εcMy	Deformazione massima cls int direzione Y per pressoflessione retta (1)
εfMy	Deformazione massima acciaio int direzione Y per pressoflessione retta (1)
εcMz	Deformazione massima cls int direzione Z per pressoflessione retta (1)
εfMz	Deformazione massima acciaio int direzione Z per pressoflessione retta (1)
MyCal [kN*m]	Momento flettente dir Y di calcolo
ΔMy [kN*m]	Incremento di MyCal dovuto al taglio Tz
MzCal [kN*m]	Momento flettente dir Z di calcolo
ΔMz [kN*m]	Incremento di MzCal dovuto al taglio Ty
Mry+ [kN*m]	Momento resistente dir Y positiva
Mry- [kN*m]	Momento resistente dir Y negativa
Mrz+ [kN*m]	Momento resistente dir Z positiva
Mrz- [kN*m]	Momento resistente dir Z negativa
ΣMrtY	Somma dei momenti resistenti delle travi in direzione Y(2)
ΣMrtZ	Somma dei momenti resistenti delle travi in direzione Z(2)
ΣMyRich.	Momento resistente richiesto direzione Y per rispettare la gerarchia(2)
ΣMzRich.	Momento resistente richiesto direzione Z per rispettare la gerarchia(2)

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 55 di 103

T [kN]	Valore del taglio
Dir[Y-Z]	Direzione della componente di taglio
VRdns [kN]	Resistenza a taglio in assenza di armature
VRdns [kN]	Resistenza a taglio in assenza di armature
VRcd [kN]	Resistenza taglio-compresione calcestruzzo
VRsd [kN]	Resistenza taglio-trazione acciaio
VRd [kN]	Resistenza a taglio =min(VRcd,VRsd)
VRd,f [kN]	Resistenza a taglio dovuta alla resistenza a trazione del calcestruzzo ad alte prestazioni (quando presente)(cfr. eq 4.2 CNR204/2006), oppure resistenza rinforzo del composito (quando presente)(cfr. eq 4.19 CNR200/2013), oppure resistenza rinforzo della camicia in acciaio (quando presente)(cfr. eq C8.7.4.5 Circolare NTC)
Ast/m [cmq]	Armatura staffe
Min.Norm.	Valore minimo di norma dell' area delle staffe
cot(θ)	cot(θ) secondo il punto 4.1.2.3.5 delle Norme Tecniche
Fatt.Ampl.Sisma	Fattore moltiplicativo di gruppo per le azioni sismiche (solo se diverso da 1.0)
Cs	Coefficiente di sicurezza definito dal rapporto Fr / Fd (Fr=punto sul dominio di resistenza ottenuto aumentando proporzionalmente Fd,Fd=azione), quando richiesto dal criterio di verifica
ζ _s	Livello di sicurezza sismico definito come rapporto tra l'accelerazione sopportabile e l'accelerazione di progetto(valore stampato quando richiesto dal criterio di verifica)

Verifiche duttilità (quando richieste):

Zona	Sezione di verifica dell'elemento
Comb.	Combinazione di verifica
Nmax [kN]	Sforzo Normale massimo
Dir	Direzione di flessione (pilastri=Y o Z, travi =Z, pareti= ortogonale alla base)
Mry [kN*m]	Momento di snervamento corrispondente a Nmax
MrU [kN*m]	Momento ultimo (resistente) corrispondente a Nmax sulla sezione depurata del calcestruzzo non confinato, considerando il confinamento
φ _y [1/m]	Curvatura allo snervamento (φ _y = MrU/Mry * φ'y)
φ _u [1/m]	Curvatura allo corrispondente a MrU
μ	Capacità in duttilità della sezione
F.Conf	Fattore di confinamento adottato (= fck,c/fck)
μ _d	Richiesta in duttilità della sezione
Cs	Livello di sicurezza (Cs=μ/μ _d)

Note Verifica pilastri:

⁽¹⁾ le deformazioni sono stampate a meno del fattore 10⁻³

⁽²⁾ I momenti resistenti richiesti sono quelli dovuti alla ripartizione della somma dei momenti resistenti delle travi quando nella tabella dei momenti appare '-' significa che la gerarchia in quella direzione non è applicabile a seconda che il pilastro sia al piano terra o all'ultimo piano, oppure, la combinazione corrente non è sismica, oppure, la combinazione è sismica ma la sua direzione non è nella direzione del pilastro considerata. Un valore nullo dei momenti resistenti è relativo a piede o testa di pilastri in fondazione o copertura

Pilastro: 1 [1,101] Sez. R: By=30.00 cm Bz=50.00 cm L=400.00 cm Ln=400.00 cm Criterio: CLS_Pilastri_ND - Verifica a presso-flessione deviata,ζ_s=1.336 [(4+5)-V-3] : **Verificato**

Piede	AfSpigolo = 3.14	Afy = 0.00	Afz = 1.54
Testa	AfSpigolo = 3.14	Afy = 0.00	Afz = 1.54

v_{max}=N/(fcd*A)=0.043 <= 0.65 [Comb. (4+5)-XI-4(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	2(+)	-159.79	-8.62	-2.11	140.19	86.42	140.19	86.42	18
Piede	2(-)	-159.79	-9.14	-3.20	140.19	86.42	140.19	86.42	17
Piede	3(+)	-159.15	-9.08	-3.18	140.08	86.35	140.08	86.35	17
Piede	3(+)	-159.15	-8.56	-2.10	140.08	86.35	140.08	86.35	18
Piede	1(+)	-147.96	-7.82	-1.96	138.14	85.17	138.14	85.17	19
Piede	1(-)	-147.96	-8.28	-2.96	138.14	85.17	138.14	85.17	18
Piede	(4+5)-XI-4(-)	-137.94	70.33	-1.76	136.40	84.12	136.40	84.12	2.4
Piede	(4+5)-XI-4(+)	-137.94	63.53	-1.50	136.40	84.12	136.40	84.12	2.8
Piede	(4+5)-V-4(+)	-137.16	65.16	-3.00	136.27	84.04	136.27	84.04	2.6
Piede	(4+5)-V-4(+)	-137.16	58.85	-2.68	136.27	84.04	136.27	84.04	3.0
Piede	(4+5)-VIII-4(+)	-132.04	41.59	-10.57	135.38	83.49	135.38	83.49	4.1
Piede	(4+5)-VIII-4(-)	-132.04	46.10	-11.37	135.38	83.49	135.38	83.49	3.5
Piede	(4+5)-X-4(+)	-131.67	20.16	-25.89	135.31	83.46	135.31	83.46	3.7
Piede	(4+5)-X-4(-)	-131.67	22.50	-27.59	135.31	83.46	135.31	83.46	3.3
Piede	(4+5)-II-4(+)	-131.27	36.91	-11.75	135.24	83.41	135.24	83.41	4.5
Piede	(4+5)-II-4(-)	-131.27	40.93	-12.61	135.24	83.41	135.24	83.41	3.9
Piede	(4+5)-V-2(-)	-130.12	71.76	17.09	135.04	83.29	135.04	83.29	1.8
Piede	(4+5)-V-2(+)	-130.12	64.82	16.29	135.04	83.29	135.04	83.29	2.1
Piede	(4+5)-VII-4(+)	-129.90	13.58	-28.61	135.00	83.27	135.00	83.27	3.6
Piede	(4+5)-VII-4(-)	-129.90	15.23	-30.47	135.00	83.27	135.00	83.27	3.3
Piede	(4+5)-XI-2(-)	-129.35	66.60	15.84	134.91	83.21	134.91	83.21	2.0
Piede	(4+5)-XI-2(+)	-129.35	60.14	15.11	134.91	83.21	134.91	83.21	2.3
Piede	(4+5)-IV-4(-)	-129.09	5.28	-31.75	134.86	83.18	134.86	83.18	3.5
Piede	(4+5)-IV-4(+)	-129.09	4.58	-29.82	134.86	83.18	134.86	83.18	3.9
Piede	(4+5)-I-4(-)	-127.32	-1.99	-34.63	134.55	83.00	134.55	83.00	3.2
Piede	(4+5)-I-4(+)	-127.32	-2.01	-32.54	134.55	83.00	134.55	83.00	3.5
Piede	(4+5)-II-2(-)	-124.22	47.53	7.48	134.01	82.67	134.01	82.67	3.6

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 56 di 103

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
Piede	(4+5)-II-2(+)	-124.22	42.88	7.22	134.01	82.67	134.01	82.67	4.1
Piede	(4+5)-VIII-2(-)	-123.45	42.36	6.23	133.88	82.58	133.88	82.58	4.3
Piede	(4+5)-VIII-2(+)	-123.45	38.20	6.04	133.88	82.58	133.88	82.58	5.1
Piede	(4+5)-XII-4(+)	-121.65	16.21	-6.51	133.56	82.39	133.56	82.39	13
Piede	(4+5)-XII-4(-)	-121.65	18.14	-7.06	133.56	82.39	133.56	82.39	12
Piede	(4+5)-VI-4(+)	-120.87	11.53	-7.69	133.43	82.31	133.43	82.31	14
Piede	(4+5)-VI-4(-)	-120.87	12.98	-8.31	133.43	82.31	133.43	82.31	13
Piede	(4+5)-IX-4(+)	-119.88	9.63	-9.23	133.25	82.20	133.25	82.20	14
Piede	(4+5)-IX-4(-)	-119.88	10.87	-9.95	133.25	82.20	133.25	82.20	13
Piede	(4+5)-VII-3(+)	-119.47	-13.82	-27.47	133.18	82.16	133.18	82.16	3.7
Piede	(4+5)-VII-3(-)	-119.47	-14.96	-29.26	133.18	82.16	133.18	82.16	3.3
Piede	(4+5)-III-4(-)	-119.10	5.71	-11.19	133.12	82.12	133.12	82.12	13
Piede	(4+5)-III-4(+)	-119.10	4.95	-10.41	133.12	82.12	133.12	82.12	14
Piede	(4+5)-X-3(+)	-117.71	-20.40	-30.19	132.87	81.97	132.87	81.97	2.9
Piede	(4+5)-X-3(-)	-117.71	-22.23	-32.14	132.87	81.97	132.87	81.97	2.7
Piede	(4+5)-I-3(+)	-116.89	-29.40	-31.39	132.73	81.89	132.73	81.89	2.5
Piede	(4+5)-I-3(-)	-116.89	-32.18	-33.42	132.73	81.89	132.73	81.89	2.2
Piede	(4+5)-IV-3(+)	-115.13	-35.98	-34.11	132.42	81.70	132.42	81.70	2.1
Piede	(4+5)-IV-3(-)	-115.13	-39.45	-36.30	132.42	81.70	132.42	81.70	1.9
Piede	(4+5)-VI-2(-)	-113.83	19.57	11.78	132.19	81.56	132.19	81.56	7.9
Piede	(4+5)-VI-2(+)	-113.83	17.50	11.28	132.19	81.56	132.19	81.56	8.9
Piede	(4+5)-XII-2(-)	-113.05	14.41	10.53	132.06	81.48	132.06	81.48	11
Piede	(4+5)-XII-2(+)	-113.05	12.82	10.10	132.06	81.48	132.06	81.48	12
Piede	(4+5)-III-2(-)	-112.06	12.30	8.90	131.88	81.37	131.88	81.37	13
Piede	(4+5)-III-2(+)	-112.06	10.92	8.56	131.88	81.37	131.88	81.37	14
Piede	(4+5)-IX-2(-)	-111.29	7.14	7.65	131.75	81.29	131.75	81.29	17
Piede	(4+5)-IX-2(+)	-111.29	6.24	7.38	131.75	81.29	131.75	81.29	17
Piede	(4+5)-IX-3(-)	-109.45	-19.32	-8.73	131.42	81.09	131.42	81.09	9.6
Piede	(4+5)-IX-3(+)	-109.45	-17.77	-8.08	131.42	81.09	131.42	81.09	11
Piede	(4+5)-III-3(+)	-108.68	-22.44	-9.26	131.29	81.01	131.29	81.01	8.0
Piede	(4+5)-III-3(-)	-108.68	-24.49	-9.98	131.29	81.01	131.29	81.01	7.0
Piede	(4+5)-XII-3(+)	-107.68	-24.35	-10.80	131.11	80.91	131.11	80.91	6.7
Piede	(4+5)-XII-3(-)	-107.68	-26.59	-11.61	131.11	80.91	131.11	80.91	5.8
Piede	(4+5)-VI-3(+)	-106.91	-29.02	-11.98	130.98	80.82	130.98	80.82	5.2
Piede	(4+5)-VI-3(-)	-106.91	-31.76	-12.86	130.98	80.82	130.98	80.82	4.6
Piede	(4+5)-IV-2(-)	-105.61	27.27	35.22	130.75	80.68	130.75	80.68	2.2
Piede	(4+5)-IV-2(+)	-105.61	24.46	33.41	130.75	80.68	130.75	80.68	2.4
Piede	(4+5)-I-2(+)	-103.84	17.88	30.69	130.44	80.50	130.44	80.50	2.8
Piede	(4+5)-I-2(-)	-103.84	20.00	32.34	130.44	80.50	130.44	80.50	2.6
Piede	(4+5)-X-2(+)	-103.03	8.87	29.48	130.29	80.41	130.29	80.41	3.3
Piede	(4+5)-X-2(-)	-103.03	10.05	31.06	130.29	80.41	130.29	80.41	3.1
Piede	(4+5)-III-1(-)	-101.63	-17.89	10.11	130.05	80.26	130.05	80.26	9.0
Piede	(4+5)-III-1(+)	-101.63	-16.48	9.71	130.05	80.26	130.05	80.26	9.8
Piede	(4+5)-VII-2(+)	-101.26	2.29	26.76	129.98	80.22	129.98	80.22	4.2
Piede	(4+5)-VII-2(-)	-101.26	2.78	28.18	129.98	80.22	129.98	80.22	3.8
Piede	(4+5)-IX-1(+)	-100.86	-21.15	8.53	129.91	80.18	129.91	80.18	8.6
Piede	(4+5)-IX-1(-)	-100.86	-23.05	8.87	129.91	80.18	129.91	80.18	7.6
Piede	(4+5)-VI-1(+)	-99.86	-23.06	6.99	129.74	80.07	129.74	80.07	8.4
Piede	(4+5)-VI-1(-)	-99.86	-25.16	7.23	129.74	80.07	129.74	80.07	7.4
Piede	(4+5)-XII-1(-)	-99.09	-30.32	5.98	129.60	79.99	129.60	79.99	6.1
Piede	(4+5)-XII-1(+)	-99.09	-27.73	5.81	129.60	79.99	129.60	79.99	7.0
Piede	(4+5)-VIII-3(+)	-97.29	-49.73	-6.74	129.28	79.79	129.28	79.79	3.0
Piede	(4+5)-VIII-3(-)	-97.29	-54.54	-7.31	129.28	79.79	129.28	79.79	2.7
Piede	(4+5)-II-3(+)	-96.51	-54.40	-7.92	129.14	79.71	129.14	79.71	2.6
Piede	(4+5)-II-3(-)	-96.51	-59.71	-8.56	129.14	79.71	129.14	79.71	2.3
Piede	(4+5)-I-1(-)	-93.42	-10.19	33.55	128.60	79.38	128.60	79.38	2.7
Piede	(4+5)-I-1(+)	-93.42	-9.52	31.84	128.60	79.38	128.60	79.38	2.9
Piede	(4+5)-IV-1(+)	-91.65	-16.10	29.12	128.28	79.19	128.28	79.19	2.9
Piede	(4+5)-IV-1(-)	-91.65	-17.46	30.67	128.28	79.19	128.28	79.19	2.7
Piede	(4+5)-XI-3(+)	-91.39	-71.67	-15.81	128.24	79.16	128.24	79.16	1.7
Piede	(4+5)-XI-3(-)	-91.39	-78.78	-16.92	128.24	79.16	128.24	79.16	1.5
Piede	(4+5)-VII-1(+)	-90.84	-25.10	27.91	128.14	79.10	128.14	79.10	2.7
Piede	(4+5)-VII-1(-)	-90.84	-27.41	29.39	128.14	79.10	128.14	79.10	2.5
Piede	(4+5)-V-3(+)	-90.62	-76.34	-16.99	128.10	79.08	128.10	79.08	1.6
Piede	(4+5)-V-3(-)	-90.62	-83.94	-18.17	128.10	79.08	128.10	79.08	1.4
Piede	(4+5)-II-1(+)	-89.47	-48.44	11.05	127.90	78.95	127.90	78.95	2.8
Piede	(4+5)-II-1(-)	-89.47	-53.11	11.53	127.90	78.95	127.90	78.95	2.5
Piede	(4+5)-X-1(+)	-89.07	-31.69	25.19	127.83	78.91	127.83	78.91	2.6
Piede	(4+5)-X-1(-)	-89.07	-34.68	26.51	127.83	78.91	127.83	78.91	2.4
Piede	(4+5)-VIII-1(+)	-88.70	-53.11	9.87	127.76	78.87	127.76	78.87	2.5
Piede	(4+5)-VIII-1(-)	-88.70	-58.28	10.29	127.76	78.87	127.76	78.87	2.3
Piede	(4+5)-V-1(-)	-83.57	-77.35	1.93	126.85	78.32	126.85	78.32	1.8
Piede	(4+5)-V-1(+)	-83.57	-70.38	1.98	126.85	78.32	126.85	78.32	2.0
Piede	(4+5)-XI-1(-)	-82.80	-82.51	0.68	126.71	78.24	126.71	78.24	1.6
Piede	(4+5)-XI-1(+)	-82.80	-75.05	0.80	126.71	78.24	126.71	78.24	1.8
Testa	2(+)	-140.29	3.51	9.85	136.81	84.37	136.81	84.37	15

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 57 di 103

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
Testa	2 (-)	-140.29	1.33	9.53	136.81	84.37	136.81	84.37	15
Testa	3 (-)	-139.65	1.33	9.14	136.70	84.30	136.70	84.30	16
Testa	3 (+)	-139.65	3.49	9.44	136.70	84.30	136.70	84.30	15
Testa	1 (+)	-128.46	3.21	8.36	134.75	83.12	134.75	83.12	17
Testa	1 (-)	-128.46	1.22	8.10	134.75	83.12	134.75	83.12	17
Testa	(4+5)-XI-4 (-)	-122.94	-56.08	6.82	133.79	82.53	133.79	82.53	2.9
Testa	(4+5)-XI-4 (+)	-122.94	-62.88	7.07	133.79	82.53	133.79	82.53	2.5
Testa	(4+5)-V-4 (-)	-122.16	-52.12	7.97	133.65	82.45	133.65	82.45	3.1
Testa	(4+5)-V-4 (+)	-122.16	-58.44	8.29	133.65	82.45	133.65	82.45	2.6
Testa	(4+5)-VIII-4 (+)	-117.04	-42.19	16.43	132.76	81.90	132.76	81.90	3.2
Testa	(4+5)-VIII-4 (-)	-117.04	-37.68	15.64	132.76	81.90	132.76	81.90	3.6
Testa	(4+5)-X-4 (+)	-116.67	-23.32	31.81	132.69	81.86	132.69	81.86	2.6
Testa	(4+5)-X-4 (-)	-116.67	-20.98	30.11	132.69	81.86	132.69	81.86	2.9
Testa	(4+5)-II-4 (+)	-116.27	-37.75	17.65	132.62	81.82	132.62	81.82	3.4
Testa	(4+5)-II-4 (-)	-116.27	-33.73	16.78	132.62	81.82	132.62	81.82	3.9
Testa	(4+5)-V-2 (-)	-115.12	-57.28	-10.11	132.42	81.70	132.42	81.70	2.5
Testa	(4+5)-V-2 (+)	-115.12	-64.22	-10.91	132.42	81.70	132.42	81.70	2.2
Testa	(4+5)-VII-4 (+)	-114.90	-17.12	34.61	132.38	81.68	132.38	81.68	2.6
Testa	(4+5)-VII-4 (-)	-114.90	-15.47	32.75	132.38	81.68	132.38	81.68	2.8
Testa	(4+5)-XI-2 (-)	-114.35	-53.33	-8.96	132.28	81.62	132.28	81.62	2.8
Testa	(4+5)-XI-2 (+)	-114.35	-59.78	-9.69	132.28	81.62	132.28	81.62	2.4
Testa	(4+5)-IV-4 (-)	-114.09	-7.81	33.94	132.24	81.59	132.24	81.59	2.9
Testa	(4+5)-IV-4 (+)	-114.09	-8.52	35.87	132.24	81.59	132.24	81.59	2.7
Testa	(4+5)-I-4 (-)	-112.32	-2.29	36.58	131.93	81.40	131.93	81.40	2.8
Testa	(4+5)-I-4 (+)	-112.32	-2.31	38.67	131.93	81.40	131.93	81.40	2.6
Testa	(4+5)-II-2 (-)	-109.22	-38.88	-1.30	131.38	81.07	131.38	81.07	5.2
Testa	(4+5)-II-2 (+)	-109.22	-43.53	-1.55	131.38	81.07	131.38	81.07	4.3
Testa	(4+5)-VIII-2 (-)	-108.45	-34.93	-0.15	131.25	80.99	131.25	80.99	6.3
Testa	(4+5)-VIII-2 (+)	-108.45	-39.09	-0.34	131.25	80.99	131.25	80.99	5.2
Testa	(4+5)-XII-4 (+)	-106.65	-19.71	12.25	130.93	80.80	130.93	80.80	7.4
Testa	(4+5)-XII-4 (-)	-106.65	-17.78	11.69	130.93	80.80	130.93	80.80	8.3
Testa	(4+5)-VI-4 (+)	-105.87	-15.27	13.46	130.79	80.71	130.79	80.71	7.9
Testa	(4+5)-VI-4 (-)	-105.87	-13.83	12.84	130.79	80.71	130.79	80.71	8.8
Testa	(4+5)-IX-4 (+)	-104.88	-13.50	15.05	130.62	80.61	130.62	80.61	7.4
Testa	(4+5)-IX-4 (-)	-104.88	-12.26	14.34	130.62	80.61	130.62	80.61	8.2
Testa	(4+5)-VII-3 (+)	-104.47	7.47	33.43	130.55	80.56	130.55	80.56	2.9
Testa	(4+5)-VII-3 (-)	-104.47	6.32	31.64	130.55	80.56	130.55	80.56	3.2
Testa	(4+5)-III-4 (-)	-104.10	-8.31	15.49	130.48	80.52	130.48	80.52	8.4
Testa	(4+5)-III-4 (+)	-104.10	-9.06	16.27	130.48	80.52	130.48	80.52	7.7
Testa	(4+5)-X-3 (+)	-102.71	13.68	36.24	130.24	80.37	130.24	80.37	2.4
Testa	(4+5)-X-3 (-)	-102.71	11.84	34.28	130.24	80.37	130.24	80.37	2.6
Testa	(4+5)-I-3 (+)	-101.89	22.28	37.49	130.09	80.29	130.09	80.29	2.1
Testa	(4+5)-I-3 (-)	-101.89	19.50	35.47	130.09	80.29	130.09	80.29	2.3
Testa	(4+5)-IV-3 (+)	-100.13	28.48	40.30	129.78	80.10	129.78	80.10	1.8
Testa	(4+5)-IV-3 (-)	-100.13	25.01	38.11	129.78	80.10	129.78	80.10	2.0
Testa	(4+5)-VI-2 (-)	-98.83	-18.98	-5.24	129.55	79.96	129.55	79.96	12
Testa	(4+5)-VI-2 (+)	-98.83	-21.06	-5.74	129.55	79.96	129.55	79.96	10
Testa	(4+5)-XII-2 (-)	-98.05	-15.03	-4.09	129.42	79.88	129.42	79.88	16
Testa	(4+5)-XII-2 (+)	-98.05	-16.61	-4.52	129.42	79.88	129.42	79.88	14
Testa	(4+5)-III-2 (-)	-97.06	-13.46	-2.59	129.24	79.77	129.24	79.77	18
Testa	(4+5)-III-2 (+)	-97.06	-14.85	-2.93	129.24	79.77	129.24	79.77	17
Testa	(4+5)-IX-2 (-)	-96.29	-9.51	-1.45	129.10	79.69	129.10	79.69	24
Testa	(4+5)-IX-2 (+)	-96.29	-10.41	-1.71	129.10	79.69	129.10	79.69	22
Testa	(4+5)-IX-3 (-)	-94.45	9.53	13.22	128.78	79.49	128.78	79.49	9.4
Testa	(4+5)-IX-3 (+)	-94.45	11.08	13.87	128.78	79.49	128.78	79.49	8.3
Testa	(4+5)-III-3 (+)	-93.68	15.53	15.09	128.64	79.41	128.64	79.41	6.4
Testa	(4+5)-III-3 (-)	-93.68	13.48	14.37	128.64	79.41	128.64	79.41	7.3
Testa	(4+5)-XII-3 (+)	-92.68	17.29	16.68	128.47	79.30	128.47	79.30	5.4
Testa	(4+5)-XII-3 (-)	-92.68	15.05	15.87	128.47	79.30	128.47	79.30	6.1
Testa	(4+5)-VI-3 (+)	-91.91	21.73	17.90	128.33	79.22	128.33	79.22	4.4
Testa	(4+5)-VI-3 (-)	-91.91	19.00	17.02	128.33	79.22	128.33	79.22	5.0
Testa	(4+5)-IV-2 (-)	-90.61	-24.99	-26.33	128.10	79.08	128.10	79.08	2.8
Testa	(4+5)-IV-2 (+)	-90.61	-27.81	-28.14	128.10	79.08	128.10	79.08	2.6
Testa	(4+5)-I-2 (+)	-88.84	-21.60	-25.34	127.79	78.89	127.79	78.89	3.1
Testa	(4+5)-I-2 (-)	-88.84	-19.48	-23.69	127.79	78.89	127.79	78.89	3.4
Testa	(4+5)-X-2 (+)	-88.03	-13.00	-24.08	127.64	78.80	127.64	78.80	3.8
Testa	(4+5)-X-2 (-)	-88.03	-11.82	-22.50	127.64	78.80	127.64	78.80	4.2
Testa	(4+5)-III-1 (-)	-86.63	8.33	-3.71	127.39	78.65	127.39	78.65	23
Testa	(4+5)-III-1 (+)	-86.63	9.74	-4.11	127.39	78.65	127.39	78.65	20
Testa	(4+5)-VII-2 (+)	-86.26	-6.79	-21.27	127.33	78.61	127.33	78.61	4.9
Testa	(4+5)-VII-2 (-)	-86.26	-6.30	-19.86	127.33	78.61	127.33	78.61	5.5
Testa	(4+5)-IX-1 (+)	-85.86	14.18	-2.89	127.26	78.57	127.26	78.57	18
Testa	(4+5)-IX-1 (-)	-85.86	12.28	-2.56	127.26	78.57	127.26	78.57	20
Testa	(4+5)-VI-1 (+)	-84.86	15.95	-1.31	127.08	78.46	127.08	78.46	17
Testa	(4+5)-VI-1 (-)	-84.86	13.85	-1.06	127.08	78.46	127.08	78.46	20
Testa	(4+5)-XII-1 (-)	-84.09	17.80	0.09	126.94	78.38	126.94	78.38	16

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 58 di 103

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
Testa	(4+5)-XII-1(+)	-84.09	20.39	-0.09	126.94	78.38	126.94	78.38	13
Testa	(4+5)-VIII-3(+)	-82.29	39.77	12.49	126.62	78.18	126.62	78.18	3.2
Testa	(4+5)-VIII-3(-)	-82.29	34.95	11.93	126.62	78.18	126.62	78.18	3.7
Testa	(4+5)-II-3(+)	-81.51	44.21	13.71	126.49	78.10	126.49	78.10	2.8
Testa	(4+5)-II-3(-)	-81.51	38.90	13.08	126.49	78.10	126.49	78.10	3.2
Testa	(4+5)-I-1(-)	-78.42	2.31	-24.80	125.93	77.76	125.93	77.76	4.1
Testa	(4+5)-I-1(+)	-78.42	2.99	-26.52	125.93	77.76	125.93	77.76	3.7
Testa	(4+5)-IV-1(+)	-76.65	9.19	-23.71	125.62	77.57	125.62	77.57	3.9
Testa	(4+5)-IV-1(-)	-76.65	7.83	-22.16	125.62	77.57	125.62	77.57	4.3
Testa	(4+5)-XI-3(+)	-76.39	60.46	21.85	125.57	77.54	125.57	77.54	1.7
Testa	(4+5)-XI-3(-)	-76.39	53.35	20.74	125.57	77.54	125.57	77.54	2.0
Testa	(4+5)-VII-1(+)	-75.84	17.79	-22.45	125.48	77.48	125.48	77.48	3.5
Testa	(4+5)-VII-1(-)	-75.84	15.49	-20.97	125.48	77.48	125.48	77.48	4.0
Testa	(4+5)-V-3(+)	-75.62	64.90	23.07	125.44	77.46	125.44	77.46	1.6
Testa	(4+5)-V-3(-)	-75.62	57.30	21.89	125.44	77.46	125.44	77.46	1.8
Testa	(4+5)-II-1(+)	-74.47	38.42	-5.49	125.23	77.34	125.23	77.34	3.9
Testa	(4+5)-II-1(-)	-74.47	33.75	-5.01	125.23	77.34	125.23	77.34	4.6
Testa	(4+5)-X-1(+)	-74.07	24.00	-19.65	125.16	77.29	125.16	77.29	3.5
Testa	(4+5)-X-1(-)	-74.07	21.00	-18.33	125.16	77.29	125.16	77.29	4.0
Testa	(4+5)-VIII-1(+)	-73.70	42.87	-4.27	125.09	77.25	125.09	77.25	3.5
Testa	(4+5)-VIII-1(-)	-73.70	37.70	-3.86	125.09	77.25	125.09	77.25	4.1
Testa	(4+5)-V-1(-)	-68.57	52.14	3.81	124.18	76.70	124.18	76.70	2.7
Testa	(4+5)-V-1(+)	-68.57	59.11	3.86	124.18	76.70	124.18	76.70	2.3
Testa	(4+5)-XI-1(-)	-67.80	56.09	4.96	124.04	76.61	124.04	76.61	2.4
Testa	(4+5)-XI-1(+)	-67.80	63.56	5.08	124.04	76.61	124.04	76.61	2.1

Zona	C.	N	MyCal	ΔMy	MzCal	ΔMz	Mry+	Mry-	Mrz+	Mrz-
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m
Piede	2(+)	-159.79	-9.14	0.53	-3.20	1.08	140.19	140.19	86.42	86.42
Piede	2(-)	-159.79	-9.14	0.00	-3.20	0.00	140.19	140.19	86.42	86.42
Piede	3(-)	-159.15	-9.08	0.00	-3.18	0.00	140.08	140.08	86.35	86.35
Piede	3(+)	-159.15	-9.08	0.52	-3.18	1.08	140.08	140.08	86.35	86.35
Piede	1(+)	-147.96	-8.28	0.45	-2.96	1.00	138.14	138.14	85.17	85.17
Piede	1(-)	-147.96	-8.28	0.00	-2.96	0.00	138.14	138.14	85.17	85.17
Piede	(4+5)-XI-4(-)	-137.94	70.33	0.00	-1.76	0.00	136.40	136.40	84.12	84.12
Piede	(4+5)-XI-4(+)	-137.94	70.33	-6.80	-1.76	0.25	136.40	136.40	84.12	84.12
Piede	(4+5)-V-4(-)	-137.16	65.16	0.00	-3.00	0.00	136.27	136.27	84.04	84.04
Piede	(4+5)-V-4(+)	-137.16	65.16	-6.31	-3.00	0.32	136.27	136.27	84.04	84.04
Piede	(4+5)-VIII-4(+)	-132.04	46.10	-4.51	-11.37	0.79	135.38	135.38	83.49	83.49
Piede	(4+5)-VIII-4(-)	-132.04	46.10	0.00	-11.37	0.00	135.38	135.38	83.49	83.49
Piede	(4+5)-X-4(+)	-131.67	22.50	-2.34	-27.59	1.70	135.31	135.31	83.46	83.46
Piede	(4+5)-X-4(-)	-131.67	22.50	0.00	-27.59	0.00	135.31	135.31	83.46	83.46
Piede	(4+5)-II-4(+)	-131.27	40.93	-4.02	-12.61	0.86	135.24	135.24	83.41	83.41
Piede	(4+5)-II-4(-)	-131.27	40.93	0.00	-12.61	0.00	135.24	135.24	83.41	83.41
Piede	(4+5)-V-2(-)	-130.12	71.76	0.00	17.09	0.00	135.04	135.04	83.29	83.29
Piede	(4+5)-V-2(+)	-130.12	71.76	-6.95	17.09	-0.80	135.04	135.04	83.29	83.29
Piede	(4+5)-VII-4(+)	-129.90	15.23	-1.65	-30.47	1.86	135.00	135.00	83.27	83.27
Piede	(4+5)-VII-4(-)	-129.90	15.23	0.00	-30.47	0.00	135.00	135.00	83.27	83.27
Piede	(4+5)-XI-2(-)	-129.35	66.60	0.00	15.84	0.00	134.91	134.91	83.21	83.21
Piede	(4+5)-XI-2(+)	-129.35	66.60	-6.45	15.84	-0.73	134.91	134.91	83.21	83.21
Piede	(4+5)-IV-4(-)	-129.09	5.28	0.00	-31.75	0.00	134.86	134.86	83.18	83.18
Piede	(4+5)-IV-4(+)	-129.09	5.28	-0.70	-31.75	1.93	134.86	134.86	83.18	83.18
Piede	(4+5)-I-4(-)	-127.32	-1.99	0.00	-34.63	0.00	134.55	134.55	83.00	83.00
Piede	(4+5)-I-4(+)	-127.32	-1.99	-0.02	-34.63	2.09	134.55	134.55	83.00	83.00
Piede	(4+5)-II-2(-)	-124.22	47.53	0.00	7.48	0.00	134.01	134.01	82.67	82.67
Piede	(4+5)-II-2(+)	-124.22	47.53	-4.65	7.48	-0.26	134.01	134.01	82.67	82.67
Piede	(4+5)-VIII-2(-)	-123.45	42.36	0.00	6.23	0.00	133.88	133.88	82.58	82.58
Piede	(4+5)-VIII-2(+)	-123.45	42.36	-4.16	6.23	-0.19	133.88	133.88	82.58	82.58
Piede	(4+5)-XII-4(+)	-121.65	18.14	-1.93	-7.06	0.55	133.56	133.56	82.39	82.39
Piede	(4+5)-XII-4(-)	-121.65	18.14	0.00	-7.06	0.00	133.56	133.56	82.39	82.39
Piede	(4+5)-VI-4(+)	-120.87	12.98	-1.44	-8.31	0.62	133.43	133.43	82.31	82.31
Piede	(4+5)-VI-4(-)	-120.87	12.98	0.00	-8.31	0.00	133.43	133.43	82.31	82.31
Piede	(4+5)-IX-4(+)	-119.88	10.87	-1.25	-9.95	0.71	133.25	133.25	82.20	82.20
Piede	(4+5)-IX-4(-)	-119.88	10.87	0.00	-9.95	0.00	133.25	133.25	82.20	82.20
Piede	(4+5)-VII-3(+)	-119.47	-14.96	1.15	-29.26	1.79	133.18	133.18	82.16	82.16
Piede	(4+5)-VII-3(-)	-119.47	-14.96	0.00	-29.26	0.00	133.18	133.18	82.16	82.16
Piede	(4+5)-III-4(-)	-119.10	5.71	0.00	-11.19	0.00	133.12	133.12	82.12	82.12
Piede	(4+5)-III-4(+)	-119.10	5.71	-0.75	-11.19	0.78	133.12	133.12	82.12	82.12
Piede	(4+5)-X-3(+)	-117.71	-22.23	1.83	-32.14	1.95	132.87	132.87	81.97	81.97
Piede	(4+5)-X-3(-)	-117.71	-22.23	0.00	-32.14	0.00	132.87	132.87	81.97	81.97
Piede	(4+5)-I-3(+)	-116.89	-32.18	2.78	-33.42	2.03	132.73	132.73	81.89	81.89
Piede	(4+5)-I-3(-)	-116.89	-32.18	0.00	-33.42	0.00	132.73	132.73	81.89	81.89
Piede	(4+5)-IV-3(+)	-115.13	-39.45	3.47	-36.30	2.19	132.42	132.42	81.70	81.70
Piede	(4+5)-IV-3(-)	-115.13	-39.45	0.00	-36.30	0.00	132.42	132.42	81.70	81.70
Piede	(4+5)-VI-2(-)	-113.83	19.57	0.00	11.78	0.00	132.19	132.19	81.56	81.56

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 59 di 103

Zona	C.	N	MyCal	ΔMy	MzCal	ΔMz	Mry+	Mry-	Mrz+	Mrz-
Piede	(4+5)-VI-2(+)	-113.83	19.57	-2.08	11.78	-0.50	132.19	132.19	81.56	81.56
Piede	(4+5)-XII-2(-)	-113.05	14.41	0.00	10.53	0.00	132.06	132.06	81.48	81.48
Piede	(4+5)-XII-2(+)	-113.05	14.41	-1.58	10.53	-0.43	132.06	132.06	81.48	81.48
Piede	(4+5)-III-2(-)	-112.06	12.30	0.00	8.90	0.00	131.88	131.88	81.37	81.37
Piede	(4+5)-III-2(+)	-112.06	12.30	-1.39	8.90	-0.34	131.88	131.88	81.37	81.37
Piede	(4+5)-IX-2(-)	-111.29	7.14	0.00	7.65	0.00	131.75	131.75	81.29	81.29
Piede	(4+5)-IX-2(+)	-111.29	7.14	-0.90	7.65	-0.27	131.75	131.75	81.29	81.29
Piede	(4+5)-IX-3(-)	-109.45	-19.32	0.00	-8.73	0.00	131.42	131.42	81.09	81.09
Piede	(4+5)-IX-3(+)	-109.45	-19.32	1.55	-8.73	0.65	131.42	131.42	81.09	81.09
Piede	(4+5)-III-3(+)	-108.68	-24.49	2.04	-9.98	0.72	131.29	131.29	81.01	81.01
Piede	(4+5)-III-3(-)	-108.68	-24.49	0.00	-9.98	0.00	131.29	131.29	81.01	81.01
Piede	(4+5)-XII-3(+)	-107.68	-26.59	2.24	-11.61	0.81	131.11	131.11	80.91	80.91
Piede	(4+5)-XII-3(-)	-107.68	-26.59	0.00	-11.61	0.00	131.11	131.11	80.91	80.91
Piede	(4+5)-VI-3(+)	-106.91	-31.76	2.73	-12.86	0.88	130.98	130.98	80.82	80.82
Piede	(4+5)-VI-3(-)	-106.91	-31.76	0.00	-12.86	0.00	130.98	130.98	80.82	80.82
Piede	(4+5)-IV-2(-)	-105.61	27.27	0.00	35.22	0.00	130.75	130.75	80.68	80.68
Piede	(4+5)-IV-2(+)	-105.61	27.27	-2.81	35.22	-1.81	130.75	130.75	80.68	80.68
Piede	(4+5)-I-2(+)	-103.84	20.00	-2.12	32.34	-1.65	130.44	130.44	80.50	80.50
Piede	(4+5)-I-2(-)	-103.84	20.00	0.00	32.34	0.00	130.44	130.44	80.50	80.50
Piede	(4+5)-X-2(+)	-103.03	10.05	-1.18	31.06	-1.58	130.29	130.29	80.41	80.41
Piede	(4+5)-X-2(-)	-103.03	10.05	0.00	31.06	0.00	130.29	130.29	80.41	80.41
Piede	(4+5)-III-1(-)	-101.63	-17.89	0.00	10.11	0.00	130.05	130.05	80.26	80.26
Piede	(4+5)-III-1(+)	-101.63	-17.89	1.41	10.11	-0.41	130.05	130.05	80.26	80.26
Piede	(4+5)-VII-2(+)	-101.26	2.78	-0.49	28.18	-1.41	129.98	129.98	80.22	80.22
Piede	(4+5)-VII-2(-)	-101.26	2.78	0.00	28.18	0.00	129.98	129.98	80.22	80.22
Piede	(4+5)-IX-1(+)	-100.86	-23.05	1.90	8.87	-0.34	129.91	129.91	80.18	80.18
Piede	(4+5)-IX-1(-)	-100.86	-23.05	0.00	8.87	0.00	129.91	129.91	80.18	80.18
Piede	(4+5)-VI-1(+)	-99.86	-25.16	2.10	7.23	-0.24	129.74	129.74	80.07	80.07
Piede	(4+5)-VI-1(-)	-99.86	-25.16	0.00	7.23	0.00	129.74	129.74	80.07	80.07
Piede	(4+5)-XII-1(-)	-99.09	-30.32	0.00	5.98	0.00	129.60	129.60	79.99	79.99
Piede	(4+5)-XII-1(+)	-99.09	-30.32	2.59	5.98	-0.17	129.60	129.60	79.99	79.99
Piede	(4+5)-VIII-3(+)	-97.29	-54.54	4.82	-7.31	0.57	129.28	129.28	79.79	79.79
Piede	(4+5)-VIII-3(-)	-97.29	-54.54	0.00	-7.31	0.00	129.28	129.28	79.79	79.79
Piede	(4+5)-II-3(+)	-96.51	-59.71	5.31	-8.56	0.64	129.14	129.14	79.71	79.71
Piede	(4+5)-II-3(-)	-96.51	-59.71	0.00	-8.56	0.00	129.14	129.14	79.71	79.71
Piede	(4+5)-I-1(-)	-93.42	-10.19	0.00	33.55	0.00	128.60	128.60	79.38	79.38
Piede	(4+5)-I-1(+)	-93.42	-10.19	0.67	33.55	-1.72	128.60	128.60	79.38	79.38
Piede	(4+5)-IV-1(+)	-91.65	-17.46	1.36	30.67	-1.55	128.28	128.28	79.19	79.19
Piede	(4+5)-IV-1(-)	-91.65	-17.46	0.00	30.67	0.00	128.28	128.28	79.19	79.19
Piede	(4+5)-XI-3(+)	-91.39	-78.78	7.11	-16.92	1.11	128.24	128.24	79.16	79.16
Piede	(4+5)-XI-3(-)	-91.39	-78.78	0.00	-16.92	0.00	128.24	128.24	79.16	79.16
Piede	(4+5)-VII-1(+)	-90.84	-27.41	2.31	29.39	-1.48	128.14	128.14	79.10	79.10
Piede	(4+5)-VII-1(-)	-90.84	-27.41	0.00	29.39	0.00	128.14	128.14	79.10	79.10
Piede	(4+5)-V-3(+)	-90.62	-83.94	7.60	-18.17	1.18	128.10	128.10	79.08	79.08
Piede	(4+5)-V-3(-)	-90.62	-83.94	0.00	-18.17	0.00	128.10	128.10	79.08	79.08
Piede	(4+5)-II-1(+)	-89.47	-53.11	4.68	11.53	-0.49	127.90	127.90	78.95	78.95
Piede	(4+5)-II-1(-)	-89.47	-53.11	0.00	11.53	0.00	127.90	127.90	78.95	78.95
Piede	(4+5)-X-1(+)	-89.07	-34.68	3.00	26.51	-1.32	127.83	127.83	78.91	78.91
Piede	(4+5)-X-1(-)	-89.07	-34.68	0.00	26.51	0.00	127.83	127.83	78.91	78.91
Piede	(4+5)-VIII-1(+)	-88.70	-58.28	5.17	10.29	-0.42	127.76	127.76	78.87	78.87
Piede	(4+5)-VIII-1(-)	-88.70	-58.28	0.00	10.29	0.00	127.76	127.76	78.87	78.87
Piede	(4+5)-V-1(-)	-83.57	-77.35	0.00	1.93	0.00	126.85	126.85	78.32	78.32
Piede	(4+5)-V-1(+)	-83.57	-77.35	6.97	1.93	0.06	126.85	126.85	78.32	78.32
Piede	(4+5)-XI-1(-)	-82.80	-82.51	0.00	0.68	0.00	126.71	126.71	78.24	78.24
Piede	(4+5)-XI-1(+)	-82.80	-82.51	7.46	0.68	0.13	126.71	126.71	78.24	78.24
Testa	2(+)	-140.29	3.51	0.00	9.85	0.00	136.81	136.81	84.37	84.37
Testa	2(-)	-140.29	3.51	-2.17	9.85	-0.32	136.81	136.81	84.37	84.37
Testa	3(-)	-139.65	3.49	-2.16	9.44	-0.30	136.70	136.70	84.30	84.30
Testa	3(+)	-139.65	3.49	0.00	9.44	0.00	136.70	136.70	84.30	84.30
Testa	1(+)	-128.46	3.21	0.00	8.36	0.00	134.75	134.75	83.12	83.12
Testa	1(-)	-128.46	3.21	-1.99	8.36	-0.26	134.75	134.75	83.12	83.12
Testa	(4+5)-XI-4(-)	-122.94	-62.88	6.80	7.07	-0.25	133.79	133.79	82.53	82.53
Testa	(4+5)-XI-4(+)	-122.94	-62.88	0.00	7.07	0.00	133.79	133.79	82.53	82.53
Testa	(4+5)-V-4(-)	-122.16	-58.44	6.31	8.29	-0.32	133.65	133.65	82.45	82.45
Testa	(4+5)-V-4(+)	-122.16	-58.44	0.00	8.29	0.00	133.65	133.65	82.45	82.45
Testa	(4+5)-VIII-4(+)	-117.04	-42.19	0.00	16.43	0.00	132.76	132.76	81.90	81.90
Testa	(4+5)-VIII-4(-)	-117.04	-42.19	4.51	16.43	-0.79	132.76	132.76	81.90	81.90
Testa	(4+5)-X-4(+)	-116.67	-23.32	0.00	31.81	0.00	132.69	132.69	81.86	81.86
Testa	(4+5)-X-4(-)	-116.67	-23.32	2.34	31.81	-1.70	132.69	132.69	81.86	81.86
Testa	(4+5)-II-4(+)	-116.27	-37.75	0.00	17.65	0.00	132.62	132.62	81.82	81.82
Testa	(4+5)-II-4(-)	-116.27	-37.75	4.02	17.65	-0.86	132.62	132.62	81.82	81.82
Testa	(4+5)-V-2(-)	-115.12	-64.22	6.95	-10.91	0.80	132.42	132.42	81.70	81.70
Testa	(4+5)-V-2(+)	-115.12	-64.22	0.00	-10.91	0.00	132.42	132.42	81.70	81.70
Testa	(4+5)-VII-4(+)	-114.90	-17.12	0.00	34.61	0.00	132.38	132.38	81.68	81.68
Testa	(4+5)-VII-4(-)	-114.90	-17.12	1.65	34.61	-1.86	132.38	132.38	81.68	81.68
Testa	(4+5)-XI-2(-)	-114.35	-59.78	6.45	-9.69	0.73	132.28	132.28	81.62	81.62

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 60 di 103

Zona	C.	N	MyCal	ΔMy	MzCal	ΔMz	Mry+	Mry-	Mrz+	Mrz-
Testa	(4+5)-XI-2(+)	-114.35	-59.78	0.00	-9.69	0.00	132.28	132.28	81.62	81.62
Testa	(4+5)-IV-4(-)	-114.09	-8.52	0.70	35.87	-1.93	132.24	132.24	81.59	81.59
Testa	(4+5)-IV-4(+)	-114.09	-8.52	0.00	35.87	0.00	132.24	132.24	81.59	81.59
Testa	(4+5)-I-4(-)	-112.32	-2.31	0.02	38.67	-2.09	131.93	131.93	81.40	81.40
Testa	(4+5)-I-4(+)	-112.32	-2.31	0.00	38.67	0.00	131.93	131.93	81.40	81.40
Testa	(4+5)-II-2(-)	-109.22	-43.53	4.65	-1.55	0.26	131.38	131.38	81.07	81.07
Testa	(4+5)-II-2(+)	-109.22	-43.53	0.00	-1.55	0.00	131.38	131.38	81.07	81.07
Testa	(4+5)-VIII-2(-)	-108.45	-39.09	4.16	-0.34	0.19	131.25	131.25	80.99	80.99
Testa	(4+5)-VIII-2(+)	-108.45	-39.09	0.00	-0.34	0.00	131.25	131.25	80.99	80.99
Testa	(4+5)-XII-4(+)	-106.65	-19.71	0.00	12.25	0.00	130.93	130.93	80.80	80.80
Testa	(4+5)-XII-4(-)	-106.65	-19.71	1.93	12.25	-0.55	130.93	130.93	80.80	80.80
Testa	(4+5)-VI-4(+)	-105.87	-15.27	0.00	13.46	0.00	130.79	130.79	80.71	80.71
Testa	(4+5)-VI-4(-)	-105.87	-15.27	1.44	13.46	-0.62	130.79	130.79	80.71	80.71
Testa	(4+5)-IX-4(+)	-104.88	-13.50	0.00	15.05	0.00	130.62	130.62	80.61	80.61
Testa	(4+5)-IX-4(-)	-104.88	-13.50	1.24	15.05	-0.71	130.62	130.62	80.61	80.61
Testa	(4+5)-VII-3(+)	-104.47	7.47	0.00	33.43	0.00	130.55	130.55	80.56	80.56
Testa	(4+5)-VII-3(-)	-104.47	7.47	-1.15	33.43	-1.79	130.55	130.55	80.56	80.56
Testa	(4+5)-III-4(-)	-104.10	-9.06	0.75	16.27	-0.78	130.48	130.48	80.52	80.52
Testa	(4+5)-III-4(+)	-104.10	-9.06	0.00	16.27	0.00	130.48	130.48	80.52	80.52
Testa	(4+5)-X-3(+)	-102.71	13.68	0.00	36.24	0.00	130.24	130.24	80.37	80.37
Testa	(4+5)-X-3(-)	-102.71	13.68	-1.83	36.24	-1.95	130.24	130.24	80.37	80.37
Testa	(4+5)-I-3(+)	-101.89	22.28	0.00	37.49	0.00	130.09	130.09	80.29	80.29
Testa	(4+5)-I-3(-)	-101.89	22.28	-2.78	37.49	-2.03	130.09	130.09	80.29	80.29
Testa	(4+5)-IV-3(+)	-100.13	28.48	0.00	40.30	0.00	129.78	129.78	80.10	80.10
Testa	(4+5)-IV-3(-)	-100.13	28.48	-3.47	40.30	-2.19	129.78	129.78	80.10	80.10
Testa	(4+5)-VI-2(-)	-98.83	-21.06	2.08	-5.74	0.50	129.55	129.55	79.96	79.96
Testa	(4+5)-VI-2(+)	-98.83	-21.06	0.00	-5.74	0.00	129.55	129.55	79.96	79.96
Testa	(4+5)-XII-2(-)	-98.05	-16.61	1.58	-4.52	0.43	129.42	129.42	79.88	79.88
Testa	(4+5)-XII-2(+)	-98.05	-16.61	0.00	-4.52	0.00	129.42	129.42	79.88	79.88
Testa	(4+5)-III-2(-)	-97.06	-14.85	1.39	-2.93	0.34	129.24	129.24	79.77	79.77
Testa	(4+5)-III-2(+)	-97.06	-14.85	0.00	-2.93	0.00	129.24	129.24	79.77	79.77
Testa	(4+5)-IX-2(-)	-96.29	-10.41	0.90	-1.71	0.27	129.10	129.10	79.69	79.69
Testa	(4+5)-IX-2(+)	-96.29	-10.41	0.00	-1.71	0.00	129.10	129.10	79.69	79.69
Testa	(4+5)-IX-3(-)	-94.45	11.08	-1.55	13.87	-0.65	128.78	128.78	79.49	79.49
Testa	(4+5)-IX-3(+)	-94.45	11.08	0.00	13.87	0.00	128.78	128.78	79.49	79.49
Testa	(4+5)-III-3(+)	-93.68	15.53	0.00	15.09	0.00	128.64	128.64	79.41	79.41
Testa	(4+5)-III-3(-)	-93.68	15.53	-2.04	15.09	-0.72	128.64	128.64	79.41	79.41
Testa	(4+5)-XII-3(+)	-92.68	17.29	0.00	16.68	0.00	128.47	128.47	79.30	79.30
Testa	(4+5)-XII-3(-)	-92.68	17.29	-2.24	16.68	-0.81	128.47	128.47	79.30	79.30
Testa	(4+5)-VI-3(+)	-91.91	21.73	0.00	17.90	0.00	128.33	128.33	79.22	79.22
Testa	(4+5)-VI-3(-)	-91.91	21.73	-2.73	17.90	-0.88	128.33	128.33	79.22	79.22
Testa	(4+5)-IV-2(-)	-90.61	-27.81	2.81	-28.14	1.81	128.10	128.10	79.08	79.08
Testa	(4+5)-IV-2(+)	-90.61	-27.81	0.00	-28.14	0.00	128.10	128.10	79.08	79.08
Testa	(4+5)-I-2(+)	-88.84	-21.60	0.00	-25.34	0.00	127.79	127.79	78.89	78.89
Testa	(4+5)-I-2(-)	-88.84	-21.60	2.12	-25.34	1.65	127.79	127.79	78.89	78.89
Testa	(4+5)-X-2(+)	-88.03	-13.00	0.00	-24.08	0.00	127.64	127.64	78.80	78.80
Testa	(4+5)-X-2(-)	-88.03	-13.00	1.18	-24.08	1.58	127.64	127.64	78.80	78.80
Testa	(4+5)-III-1(-)	-86.63	9.74	-1.41	-4.11	0.41	127.39	127.39	78.65	78.65
Testa	(4+5)-III-1(+)	-86.63	9.74	0.00	-4.11	0.00	127.39	127.39	78.65	78.65
Testa	(4+5)-VII-2(+)	-86.26	-6.79	0.00	-21.27	0.00	127.33	127.33	78.61	78.61
Testa	(4+5)-VII-2(-)	-86.26	-6.79	0.49	-21.27	1.41	127.33	127.33	78.61	78.61
Testa	(4+5)-IX-1(+)	-85.86	14.18	0.00	-2.89	0.00	127.26	127.26	78.57	78.57
Testa	(4+5)-IX-1(-)	-85.86	14.18	-1.90	-2.89	0.34	127.26	127.26	78.57	78.57
Testa	(4+5)-VI-1(+)	-84.86	15.95	0.00	-1.31	0.00	127.08	127.08	78.46	78.46
Testa	(4+5)-VI-1(-)	-84.86	15.95	-2.10	-1.31	0.24	127.08	127.08	78.46	78.46
Testa	(4+5)-XII-1(-)	-84.09	20.39	-2.59	-0.09	0.17	126.94	126.94	78.38	78.38
Testa	(4+5)-XII-1(+)	-84.09	20.39	0.00	-0.09	0.00	126.94	126.94	78.38	78.38
Testa	(4+5)-VIII-3(+)	-82.29	39.77	0.00	12.49	0.00	126.62	126.62	78.18	78.18
Testa	(4+5)-VIII-3(-)	-82.29	39.77	-4.82	12.49	-0.57	126.62	126.62	78.18	78.18
Testa	(4+5)-II-3(+)	-81.51	44.21	0.00	13.71	0.00	126.49	126.49	78.10	78.10
Testa	(4+5)-II-3(-)	-81.51	44.21	-5.31	13.71	-0.64	126.49	126.49	78.10	78.10
Testa	(4+5)-I-1(-)	-78.42	2.99	-0.67	-26.52	1.72	125.93	125.93	77.76	77.76
Testa	(4+5)-I-1(+)	-78.42	2.99	0.00	-26.52	0.00	125.93	125.93	77.76	77.76
Testa	(4+5)-IV-1(+)	-76.65	9.19	0.00	-23.71	0.00	125.62	125.62	77.57	77.57
Testa	(4+5)-IV-1(-)	-76.65	9.19	-1.36	-23.71	1.55	125.62	125.62	77.57	77.57
Testa	(4+5)-XI-3(+)	-76.39	60.46	0.00	21.85	0.00	125.57	125.57	77.54	77.54
Testa	(4+5)-XI-3(-)	-76.39	60.46	-7.11	21.85	-1.11	125.57	125.57	77.54	77.54
Testa	(4+5)-VII-1(+)	-75.84	17.79	0.00	-22.45	0.00	125.48	125.48	77.48	77.48
Testa	(4+5)-VII-1(-)	-75.84	17.79	-2.31	-22.45	1.48	125.48	125.48	77.48	77.48
Testa	(4+5)-V-3(+)	-75.62	64.90	0.00	23.07	0.00	125.44	125.44	77.46	77.46
Testa	(4+5)-V-3(-)	-75.62	64.90	-7.60	23.07	-1.18	125.44	125.44	77.46	77.46
Testa	(4+5)-II-1(+)	-74.47	38.42	0.00	-5.49	0.00	125.23	125.23	77.34	77.34
Testa	(4+5)-II-1(-)	-74.47	38.42	-4.68	-5.49	0.49	125.23	125.23	77.34	77.34
Testa	(4+5)-X-1(+)	-74.07	24.00	0.00	-19.65	0.00	125.16	125.16	77.29	77.29
Testa	(4+5)-X-1(-)	-74.07	24.00	-3.00	-19.65	1.32	125.16	125.16	77.29	77.29
Testa	(4+5)-VIII-1(+)	-73.70	42.87	0.00	-4.27	0.00	125.09	125.09	77.25	77.25

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021
Pagina 61 di 103

Zona	C.	N	MyCal	ΔMy	MzCal	ΔMz	Mry+	Mry-	Mrz+	Mrz-
Testa	(4+5)-VIII-1 (-)	-73.70	42.87	-5.17	-4.27	0.42	125.09	125.09	77.25	77.25
Testa	(4+5)-V-1 (-)	-68.57	59.11	-6.97	3.86	-0.06	124.18	124.18	76.70	76.70
Testa	(4+5)-V-1 (+)	-68.57	59.11	0.00	3.86	0.00	124.18	124.18	76.70	76.70
Testa	(4+5)-XI-1 (-)	-67.80	63.56	-7.46	5.08	-0.13	124.04	124.04	76.61	76.61
Testa	(4+5)-XI-1 (+)	-67.80	63.56	0.00	5.08	0.00	124.04	124.04	76.61	76.61

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot (θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(4+5)-IV-3	--	--	19.15	--	432.22	209.09	209.09	9.35	2.500	11
Z	(4+5)-V-3	--	--	37.21	--	460.08	373.73	373.73	9.35	2.500	10

Pilastro: 2 [2,102] Sez. R: By=50.00 cm Bz=30.00 cm L=400.00 cm Ln=400.00 cm Criterio: CLS_Pilastri_ND - Verifica a presso-flessione deviata, $\zeta_g=1.508$ [(4+5)-IV-3] : **Verificato**

Piede	AfSpigolo = 3.14	Afy = 1.54	Afz = 0.00
Testa	AfSpigolo = 3.14	Afy = 1.54	Afz = 0.00

$v_{max}=N/(fcd \cdot A)=0.069 \leq 0.65$ [Comb. (4+5)-II-4 (-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	2 (+)	-308.98	-9.38	7.70	101.61	165.18	101.61	165.18	9.2
Piede	2 (-)	-308.98	-9.95	7.72	101.61	165.18	101.61	165.18	9.1
Piede	3 (+)	-304.54	-9.38	7.59	101.17	164.46	101.17	164.46	9.3
Piede	3 (-)	-304.54	-9.96	7.61	101.17	164.46	101.17	164.46	9.2
Piede	1 (-)	-281.23	-9.01	7.03	98.85	160.64	98.85	160.64	10
Piede	1 (+)	-281.23	-8.50	7.01	98.85	160.64	98.85	160.64	10
Piede	(4+5)-II-4 (-)	-219.88	17.99	-36.51	92.64	150.43	92.64	150.43	4.9
Piede	(4+5)-II-4 (+)	-219.88	17.20	-32.96	92.64	150.43	92.64	150.43	5.5
Piede	(4+5)-VIII-2 (+)	-219.88	17.20	11.68	92.64	150.43	92.64	150.43	8.1
Piede	(4+5)-VIII-2 (-)	-219.88	17.99	12.91	92.64	150.43	92.64	150.43	7.7
Piede	(4+5)-VIII-4 (+)	-219.88	17.20	-30.23	92.64	150.43	92.64	150.43	5.8
Piede	(4+5)-VIII-4 (-)	-219.88	17.99	-33.49	92.64	150.43	92.64	150.43	5.3
Piede	(4+5)-II-2 (-)	-219.88	17.99	15.93	92.64	150.43	92.64	150.43	7.4
Piede	(4+5)-II-2 (+)	-219.88	17.20	14.41	92.64	150.43	92.64	150.43	7.8
Piede	(4+5)-V-4 (+)	-219.87	17.20	-14.39	92.64	150.43	92.64	150.43	7.8
Piede	(4+5)-V-4 (-)	-219.87	17.99	-15.91	92.64	150.43	92.64	150.43	7.4
Piede	(4+5)-XI-2 (-)	-219.87	17.99	33.51	92.64	150.43	92.64	150.43	5.3
Piede	(4+5)-XI-2 (+)	-219.87	17.20	30.25	92.64	150.43	92.64	150.43	5.8
Piede	(4+5)-XI-4 (+)	-219.87	17.20	-11.66	92.64	150.43	92.64	150.43	8.1
Piede	(4+5)-XI-4 (-)	-219.87	17.99	-12.89	92.64	150.43	92.64	150.43	7.8
Piede	(4+5)-V-2 (-)	-219.87	17.99	36.54	92.64	150.43	92.64	150.43	4.9
Piede	(4+5)-V-2 (+)	-219.87	17.20	32.98	92.64	150.43	92.64	150.43	5.5
Piede	(4+5)-I-4 (+)	-211.20	0.86	-81.73	91.75	148.96	91.75	148.96	2.4
Piede	(4+5)-I-4 (-)	-211.20	0.83	-90.50	91.75	148.96	91.75	148.96	2.0
Piede	(4+5)-VII-2 (-)	-211.20	0.83	74.24	91.75	148.96	91.75	148.96	2.8
Piede	(4+5)-VII-2 (+)	-211.20	0.86	67.07	91.75	148.96	91.75	148.96	3.3
Piede	(4+5)-III-4 (+)	-211.20	0.86	-26.47	91.75	148.96	91.75	148.96	9.7
Piede	(4+5)-III-4 (-)	-211.20	0.83	-29.31	91.75	148.96	91.75	148.96	9.1
Piede	(4+5)-IX-2 (-)	-211.20	0.83	20.11	91.75	148.96	91.75	148.96	11
Piede	(4+5)-IX-2 (+)	-211.20	0.86	18.17	91.75	148.96	91.75	148.96	12
Piede	(4+5)-IX-4 (+)	-211.20	0.86	-23.74	91.75	148.96	91.75	148.96	10
Piede	(4+5)-IX-4 (-)	-211.20	0.83	-26.28	91.75	148.96	91.75	148.96	9.7
Piede	(4+5)-III-2 (+)	-211.20	0.86	20.90	91.75	148.96	91.75	148.96	11
Piede	(4+5)-III-2 (-)	-211.20	0.83	23.14	91.75	148.96	91.75	148.96	10
Piede	(4+5)-VII-4 (-)	-211.20	0.83	-80.41	91.75	148.96	91.75	148.96	2.5
Piede	(4+5)-VII-4 (+)	-211.20	0.86	-72.63	91.75	148.96	91.75	148.96	2.9
Piede	(4+5)-I-2 (+)	-211.20	0.86	76.16	91.75	148.96	91.75	148.96	2.7
Piede	(4+5)-I-2 (-)	-211.20	0.83	84.32	91.75	148.96	91.75	148.96	2.3
Piede	(4+5)-IV-4 (-)	-211.20	0.83	-84.32	91.75	148.96	91.75	148.96	2.3
Piede	(4+5)-IV-4 (+)	-211.20	0.85	-76.16	91.75	148.96	91.75	148.96	2.7
Piede	(4+5)-X-2 (+)	-211.20	0.85	72.64	91.75	148.96	91.75	148.96	2.9
Piede	(4+5)-X-2 (-)	-211.20	0.83	80.42	91.75	148.96	91.75	148.96	2.5
Piede	(4+5)-VI-4 (+)	-211.20	0.83	-23.13	91.75	148.96	91.75	148.96	10
Piede	(4+5)-VI-4 (-)	-211.20	0.85	-20.90	91.75	148.96	91.75	148.96	11
Piede	(4+5)-XII-2 (-)	-211.20	0.83	26.29	91.75	148.96	91.75	148.96	9.7
Piede	(4+5)-XII-2 (+)	-211.20	0.85	23.74	91.75	148.96	91.75	148.96	10
Piede	(4+5)-XII-4 (+)	-211.20	0.85	-18.17	91.75	148.96	91.75	148.96	12
Piede	(4+5)-XII-4 (-)	-211.20	0.83	-20.10	91.75	148.96	91.75	148.96	11
Piede	(4+5)-VI-2 (-)	-211.20	0.83	29.32	91.75	148.96	91.75	148.96	9.1
Piede	(4+5)-VI-2 (+)	-211.20	0.85	26.47	91.75	148.96	91.75	148.96	9.7
Piede	(4+5)-X-4 (-)	-211.20	0.83	-74.23	91.75	148.96	91.75	148.96	2.8
Piede	(4+5)-X-4 (+)	-211.20	0.85	-67.06	91.75	148.96	91.75	148.96	3.3

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 62 di 103

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
Piede	(4+5)-IV-2 (-)	-211.20	0.83	90.50	91.75	148.96	91.75	148.96	2.0
Piede	(4+5)-IV-2 (+)	-211.20	0.85	81.73	91.75	148.96	91.75	148.96	2.4
Piede	(4+5)-IV-3 (-)	-203.76	-13.87	-90.50	90.98	147.70	90.98	147.70	1.7
Piede	(4+5)-IV-3 (+)	-203.76	-13.15	-81.73	90.98	147.70	90.98	147.70	2.0
Piede	(4+5)-X-1 (-)	-203.76	-13.87	74.23	90.98	147.70	90.98	147.70	2.3
Piede	(4+5)-X-1 (+)	-203.76	-13.15	67.06	90.98	147.70	90.98	147.70	2.6
Piede	(4+5)-VI-3 (+)	-203.76	-13.15	-26.47	90.98	147.70	90.98	147.70	7.2
Piede	(4+5)-VI-3 (-)	-203.76	-13.87	-29.32	90.98	147.70	90.98	147.70	6.6
Piede	(4+5)-XII-1 (+)	-203.76	-13.15	18.17	90.98	147.70	90.98	147.70	8.5
Piede	(4+5)-XII-1 (-)	-203.76	-13.87	20.10	90.98	147.70	90.98	147.70	7.9
Piede	(4+5)-XII-3 (-)	-203.76	-13.87	-26.29	90.98	147.70	90.98	147.70	7.1
Piede	(4+5)-XII-3 (+)	-203.76	-13.15	-23.74	90.98	147.70	90.98	147.70	7.6
Piede	(4+5)-VI-1 (-)	-203.76	-13.87	23.13	90.98	147.70	90.98	147.70	7.5
Piede	(4+5)-VI-1 (+)	-203.76	-13.15	20.90	90.98	147.70	90.98	147.70	8.1
Piede	(4+5)-X-3 (+)	-203.76	-13.15	-72.64	90.98	147.70	90.98	147.70	2.4
Piede	(4+5)-X-3 (-)	-203.76	-13.87	-80.42	90.98	147.70	90.98	147.70	2.0
Piede	(4+5)-IV-1 (-)	-203.76	-13.87	84.32	90.98	147.70	90.98	147.70	1.9
Piede	(4+5)-IV-1 (+)	-203.76	-13.15	76.16	90.98	147.70	90.98	147.70	2.2
Piede	(4+5)-I-3 (-)	-203.76	-13.87	-84.32	90.98	147.70	90.98	147.70	1.9
Piede	(4+5)-I-3 (+)	-203.76	-13.15	-76.16	90.98	147.70	90.98	147.70	2.2
Piede	(4+5)-VII-1 (-)	-203.76	-13.87	80.41	90.98	147.70	90.98	147.70	2.0
Piede	(4+5)-VII-1 (+)	-203.76	-13.15	72.63	90.98	147.70	90.98	147.70	2.4
Piede	(4+5)-III-3 (+)	-203.76	-13.15	-20.90	90.98	147.70	90.98	147.70	8.1
Piede	(4+5)-III-3 (-)	-203.76	-13.87	-23.14	90.98	147.70	90.98	147.70	7.5
Piede	(4+5)-IX-1 (+)	-203.76	-13.15	23.74	90.98	147.70	90.98	147.70	7.6
Piede	(4+5)-IX-1 (-)	-203.76	-13.87	26.28	90.98	147.70	90.98	147.70	7.1
Piede	(4+5)-IX-3 (-)	-203.76	-13.87	-20.11	90.98	147.70	90.98	147.70	7.9
Piede	(4+5)-IX-3 (+)	-203.76	-13.15	-18.17	90.98	147.70	90.98	147.70	8.5
Piede	(4+5)-III-1 (+)	-203.76	-13.15	26.47	90.98	147.70	90.98	147.70	7.2
Piede	(4+5)-III-1 (-)	-203.76	-13.87	29.31	90.98	147.70	90.98	147.70	6.6
Piede	(4+5)-VII-3 (-)	-203.76	-13.87	-74.24	90.98	147.70	90.98	147.70	2.3
Piede	(4+5)-VII-3 (+)	-203.76	-13.15	-67.07	90.98	147.70	90.98	147.70	2.6
Piede	(4+5)-I-1 (-)	-203.76	-13.87	90.50	90.98	147.70	90.98	147.70	1.7
Piede	(4+5)-I-1 (+)	-203.76	-13.15	81.73	90.98	147.70	90.98	147.70	2.0
Piede	(4+5)-V-3 (+)	-195.09	-29.50	-32.98	90.09	146.23	90.09	146.23	3.3
Piede	(4+5)-V-3 (-)	-195.09	-31.03	-36.54	90.09	146.23	90.09	146.23	2.9
Piede	(4+5)-XI-1 (+)	-195.09	-29.50	11.66	90.09	146.23	90.09	146.23	4.7
Piede	(4+5)-XI-1 (-)	-195.09	-31.03	12.89	90.09	146.23	90.09	146.23	4.3
Piede	(4+5)-XI-3 (-)	-195.09	-31.03	-33.51	90.09	146.23	90.09	146.23	3.1
Piede	(4+5)-XI-3 (+)	-195.09	-29.50	-30.25	90.09	146.23	90.09	146.23	3.4
Piede	(4+5)-V-1 (-)	-195.09	-31.03	15.91	90.09	146.23	90.09	146.23	4.1
Piede	(4+5)-V-1 (+)	-195.09	-29.50	14.39	90.09	146.23	90.09	146.23	4.5
Piede	(4+5)-II-3 (+)	-195.08	-29.50	-14.41	90.09	146.23	90.09	146.23	4.5
Piede	(4+5)-II-3 (-)	-195.08	-31.03	-15.93	90.09	146.23	90.09	146.23	4.1
Piede	(4+5)-VIII-1 (-)	-195.08	-31.03	33.49	90.09	146.23	90.09	146.23	3.1
Piede	(4+5)-VIII-1 (+)	-195.08	-29.50	30.23	90.09	146.23	90.09	146.23	3.4
Piede	(4+5)-VIII-3 (+)	-195.08	-29.50	-11.68	90.09	146.23	90.09	146.23	4.7
Piede	(4+5)-VIII-3 (-)	-195.08	-31.03	-12.91	90.09	146.23	90.09	146.23	4.3
Piede	(4+5)-II-1 (-)	-195.08	-31.03	36.51	90.09	146.23	90.09	146.23	2.9
Piede	(4+5)-II-1 (+)	-195.08	-29.50	32.96	90.09	146.23	90.09	146.23	3.3
Testa	2 (+)	-289.48	10.15	-7.21	99.67	162.00	99.67	162.00	9.4
Testa	2 (-)	-289.48	9.58	-7.26	99.67	162.00	99.67	162.00	9.6
Testa	3 (+)	-285.04	10.27	-7.10	99.23	161.27	99.23	161.27	9.6
Testa	3 (-)	-285.04	9.70	-7.15	99.23	161.27	99.23	161.27	9.7
Testa	1 (-)	-261.73	8.40	-6.57	96.89	157.42	96.89	157.42	11
Testa	1 (+)	-261.73	8.91	-6.52	96.89	157.42	96.89	157.42	11
Testa	(4+5)-II-4 (-)	-204.88	-8.87	29.58	91.10	147.89	91.10	147.89	7.7
Testa	(4+5)-II-4 (+)	-204.88	-9.66	33.13	91.10	147.89	91.10	147.89	6.9
Testa	(4+5)-VIII-2 (+)	-204.88	-9.66	-11.06	91.10	147.89	91.10	147.89	11
Testa	(4+5)-VIII-2 (-)	-204.88	-8.87	-9.84	91.10	147.89	91.10	147.89	12
Testa	(4+5)-VIII-4 (+)	-204.88	-9.66	30.33	91.10	147.89	91.10	147.89	7.4
Testa	(4+5)-VIII-4 (-)	-204.88	-8.87	27.07	91.10	147.89	91.10	147.89	8.1
Testa	(4+5)-II-2 (-)	-204.88	-8.87	-12.34	91.10	147.89	91.10	147.89	11
Testa	(4+5)-II-2 (+)	-204.88	-9.66	-13.87	91.10	147.89	91.10	147.89	10
Testa	(4+5)-V-4 (+)	-204.87	-9.65	13.85	91.10	147.89	91.10	147.89	10
Testa	(4+5)-V-4 (-)	-204.87	-8.86	12.33	91.10	147.89	91.10	147.89	11
Testa	(4+5)-XI-2 (-)	-204.87	-8.86	-27.09	91.10	147.89	91.10	147.89	8.1
Testa	(4+5)-XI-2 (+)	-204.87	-9.65	-30.35	91.10	147.89	91.10	147.89	7.4
Testa	(4+5)-XI-4 (+)	-204.87	-9.65	11.04	91.10	147.89	91.10	147.89	11
Testa	(4+5)-XI-4 (-)	-204.87	-8.86	9.82	91.10	147.89	91.10	147.89	12
Testa	(4+5)-V-2 (-)	-204.87	-8.86	-29.59	91.10	147.89	91.10	147.89	7.7
Testa	(4+5)-V-2 (+)	-204.87	-9.65	-33.15	91.10	147.89	91.10	147.89	6.9
Testa	(4+5)-I-4 (+)	-196.20	1.61	81.22	90.20	146.42	90.20	146.42	2.3
Testa	(4+5)-I-4 (-)	-196.20	1.59	72.45	90.20	146.42	90.20	146.42	2.8
Testa	(4+5)-VII-2 (-)	-196.20	1.59	-58.94	90.20	146.42	90.20	146.42	3.9
Testa	(4+5)-VII-2 (+)	-196.20	1.61	-66.10	90.20	146.42	90.20	146.42	3.2

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 63 di 103

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
Testa	(4+5)-III-4(+)	-196.20	1.61	26.39	90.20	146.42	90.20	146.42	9.9
Testa	(4+5)-III-4(-)	-196.20	1.59	23.54	90.20	146.42	90.20	146.42	11
Testa	(4+5)-IX-2(-)	-196.20	1.59	-15.87	90.20	146.42	90.20	146.42	13
Testa	(4+5)-IX-2(+)	-196.20	1.61	-17.81	90.20	146.42	90.20	146.42	12
Testa	(4+5)-IX-4(+)	-196.20	1.61	23.59	90.20	146.42	90.20	146.42	11
Testa	(4+5)-IX-4(-)	-196.20	1.59	21.04	90.20	146.42	90.20	146.42	11
Testa	(4+5)-III-2(+)	-196.20	1.61	-20.61	90.20	146.42	90.20	146.42	11
Testa	(4+5)-III-2(-)	-196.20	1.59	-18.38	90.20	146.42	90.20	146.42	12
Testa	(4+5)-VII-4(-)	-196.20	1.59	64.11	90.20	146.42	90.20	146.42	3.4
Testa	(4+5)-VII-4(+)	-196.20	1.61	71.88	90.20	146.42	90.20	146.42	2.8
Testa	(4+5)-I-2(+)	-196.20	1.61	-75.44	90.20	146.42	90.20	146.42	2.6
Testa	(4+5)-I-2(-)	-196.20	1.59	-67.28	90.20	146.42	90.20	146.42	3.1
Testa	(4+5)-IV-4(-)	-196.20	1.59	67.28	90.20	146.42	90.20	146.42	3.1
Testa	(4+5)-IV-4(+)	-196.20	1.61	75.44	90.20	146.42	90.20	146.42	2.6
Testa	(4+5)-X-2(+)	-196.20	1.61	-71.89	90.20	146.42	90.20	146.42	2.8
Testa	(4+5)-X-2(-)	-196.20	1.59	-64.11	90.20	146.42	90.20	146.42	3.4
Testa	(4+5)-VI-4(-)	-196.20	1.59	18.37	90.20	146.42	90.20	146.42	12
Testa	(4+5)-VI-4(+)	-196.20	1.61	20.60	90.20	146.42	90.20	146.42	11
Testa	(4+5)-XII-2(-)	-196.20	1.59	-21.05	90.20	146.42	90.20	146.42	11
Testa	(4+5)-XII-2(+)	-196.20	1.61	-23.59	90.20	146.42	90.20	146.42	11
Testa	(4+5)-XII-4(+)	-196.20	1.61	17.80	90.20	146.42	90.20	146.42	12
Testa	(4+5)-XII-4(-)	-196.20	1.59	15.87	90.20	146.42	90.20	146.42	13
Testa	(4+5)-VI-2(-)	-196.20	1.59	-23.55	90.20	146.42	90.20	146.42	11
Testa	(4+5)-VI-2(+)	-196.20	1.61	-26.40	90.20	146.42	90.20	146.42	9.9
Testa	(4+5)-X-4(-)	-196.20	1.59	58.93	90.20	146.42	90.20	146.42	3.9
Testa	(4+5)-X-4(+)	-196.20	1.61	66.10	90.20	146.42	90.20	146.42	3.2
Testa	(4+5)-IV-2(-)	-196.20	1.59	-72.46	90.20	146.42	90.20	146.42	2.8
Testa	(4+5)-IV-2(+)	-196.20	1.61	-81.23	90.20	146.42	90.20	146.42	2.3
Testa	(4+5)-IV-3(-)	-188.76	10.55	72.46	89.43	145.15	89.43	145.15	2.4
Testa	(4+5)-IV-3(+)	-188.76	11.27	81.23	89.43	145.15	89.43	145.15	2.0
Testa	(4+5)-X-1(-)	-188.76	10.55	-58.93	89.43	145.15	89.43	145.15	3.2
Testa	(4+5)-X-1(+)	-188.76	11.27	-66.10	89.43	145.15	89.43	145.15	2.7
Testa	(4+5)-VI-3(+)	-188.76	11.27	26.40	89.43	145.15	89.43	145.15	7.7
Testa	(4+5)-VI-3(-)	-188.76	10.55	23.55	89.43	145.15	89.43	145.15	8.4
Testa	(4+5)-XII-1(+)	-188.76	11.27	-17.80	89.43	145.15	89.43	145.15	9.3
Testa	(4+5)-XII-1(-)	-188.76	10.55	-15.87	89.43	145.15	89.43	145.15	9.9
Testa	(4+5)-XII-3(-)	-188.76	10.55	21.05	89.43	145.15	89.43	145.15	8.9
Testa	(4+5)-XII-3(+)	-188.76	11.27	23.59	89.43	145.15	89.43	145.15	8.2
Testa	(4+5)-VI-1(-)	-188.76	10.55	-18.37	89.43	145.15	89.43	145.15	9.4
Testa	(4+5)-VI-1(+)	-188.76	11.27	-20.60	89.43	145.15	89.43	145.15	8.8
Testa	(4+5)-X-3(+)	-188.76	11.27	71.89	89.43	145.15	89.43	145.15	2.4
Testa	(4+5)-X-3(-)	-188.76	10.55	64.11	89.43	145.15	89.43	145.15	2.8
Testa	(4+5)-IV-1(-)	-188.76	10.55	-67.28	89.43	145.15	89.43	145.15	2.6
Testa	(4+5)-IV-1(+)	-188.76	11.27	-75.44	89.43	145.15	89.43	145.15	2.2
Testa	(4+5)-I-3(-)	-188.76	10.55	67.28	89.43	145.15	89.43	145.15	2.6
Testa	(4+5)-I-3(+)	-188.76	11.27	75.44	89.43	145.15	89.43	145.15	2.2
Testa	(4+5)-VII-1(-)	-188.76	10.55	-64.11	89.43	145.15	89.43	145.15	2.8
Testa	(4+5)-VII-1(+)	-188.76	11.27	-71.88	89.43	145.15	89.43	145.15	2.4
Testa	(4+5)-III-3(+)	-188.76	11.27	20.61	89.43	145.15	89.43	145.15	8.8
Testa	(4+5)-III-3(-)	-188.76	10.55	18.38	89.43	145.15	89.43	145.15	9.4
Testa	(4+5)-IX-1(+)	-188.76	11.27	-23.59	89.43	145.15	89.43	145.15	8.2
Testa	(4+5)-IX-1(-)	-188.76	10.55	-21.04	89.43	145.15	89.43	145.15	8.9
Testa	(4+5)-IX-3(-)	-188.76	10.55	15.87	89.43	145.15	89.43	145.15	9.9
Testa	(4+5)-IX-3(+)	-188.76	11.27	17.81	89.43	145.15	89.43	145.15	9.3
Testa	(4+5)-III-1(+)	-188.76	11.27	-26.39	89.43	145.15	89.43	145.15	7.7
Testa	(4+5)-III-1(-)	-188.76	10.55	-23.54	89.43	145.15	89.43	145.15	8.4
Testa	(4+5)-VII-3(-)	-188.76	10.55	58.94	89.43	145.15	89.43	145.15	3.2
Testa	(4+5)-VII-3(+)	-188.76	11.27	66.10	89.43	145.15	89.43	145.15	2.7
Testa	(4+5)-I-1(-)	-188.76	10.55	-72.45	89.43	145.15	89.43	145.15	2.4
Testa	(4+5)-I-1(+)	-188.76	11.27	-81.22	89.43	145.15	89.43	145.15	2.0
Testa	(4+5)-V-3(+)	-180.09	22.53	33.15	88.53	143.67	88.53	143.67	4.1
Testa	(4+5)-V-3(-)	-180.09	21.00	29.59	88.53	143.67	88.53	143.67	4.7
Testa	(4+5)-XI-1(+)	-180.09	22.53	-11.04	88.53	143.67	88.53	143.67	6.5
Testa	(4+5)-XI-1(-)	-180.09	21.00	-9.82	88.53	143.67	88.53	143.67	7.3
Testa	(4+5)-XI-3(-)	-180.09	21.00	27.09	88.53	143.67	88.53	143.67	5.0
Testa	(4+5)-XI-3(+)	-180.09	22.53	30.35	88.53	143.67	88.53	143.67	4.3
Testa	(4+5)-V-1(-)	-180.09	21.00	-12.33	88.53	143.67	88.53	143.67	6.9
Testa	(4+5)-V-1(+)	-180.09	22.53	-13.85	88.53	143.67	88.53	143.67	6.2
Testa	(4+5)-II-3(+)	-180.08	22.53	13.87	88.53	143.67	88.53	143.67	6.2
Testa	(4+5)-II-3(-)	-180.08	21.00	12.34	88.53	143.67	88.53	143.67	6.9
Testa	(4+5)-VIII-1(-)	-180.08	21.00	-27.07	88.53	143.67	88.53	143.67	5.0
Testa	(4+5)-VIII-1(+)	-180.08	22.53	-30.33	88.53	143.67	88.53	143.67	4.3
Testa	(4+5)-VIII-3(+)	-180.08	22.53	11.06	88.53	143.67	88.53	143.67	6.5
Testa	(4+5)-VIII-3(-)	-180.08	21.00	9.84	88.53	143.67	88.53	143.67	7.3
Testa	(4+5)-II-1(-)	-180.08	21.00	-29.58	88.53	143.67	88.53	143.67	4.7
Testa	(4+5)-II-1(+)	-180.08	22.53	-33.13	88.53	143.67	88.53	143.67	4.1

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 64 di 103

Zona	C.	N	MyCal	ΔMy	MzCal	ΔMz	Mry+	Mry-	Mrz+	Mrz-
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m
Piede	2 (+)	-308.98	-9.95	0.57	7.72	-0.02	101.61	101.61	165.18	165.18
Piede	2 (-)	-308.98	-9.95	0.00	7.72	0.00	101.61	101.61	165.18	165.18
Piede	3 (+)	-304.54	-9.96	0.58	7.61	-0.02	101.17	101.17	164.46	164.46
Piede	3 (-)	-304.54	-9.96	0.00	7.61	0.00	101.17	101.17	164.46	164.46
Piede	1 (-)	-281.23	-9.01	0.00	7.03	0.00	98.85	98.85	160.64	160.64
Piede	1 (+)	-281.23	-9.01	0.51	7.03	-0.02	98.85	98.85	160.64	160.64
Piede	(4+5)-II-4 (-)	-219.88	17.99	0.00	-36.51	0.00	92.64	92.64	150.43	150.43
Piede	(4+5)-II-4 (+)	-219.88	17.99	-0.79	-36.51	3.56	92.64	92.64	150.43	150.43
Piede	(4+5)-VIII-2 (+)	-219.88	17.99	-0.79	12.91	-1.22	92.64	92.64	150.43	150.43
Piede	(4+5)-VIII-2 (-)	-219.88	17.99	0.00	12.91	0.00	92.64	92.64	150.43	150.43
Piede	(4+5)-VIII-4 (+)	-219.88	17.99	-0.79	-33.49	3.26	92.64	92.64	150.43	150.43
Piede	(4+5)-VIII-4 (-)	-219.88	17.99	0.00	-33.49	0.00	92.64	92.64	150.43	150.43
Piede	(4+5)-II-2 (-)	-219.88	17.99	0.00	15.93	0.00	92.64	92.64	150.43	150.43
Piede	(4+5)-II-2 (+)	-219.88	17.99	-0.79	15.93	-1.52	92.64	92.64	150.43	150.43
Piede	(4+5)-V-4 (+)	-219.87	17.99	-0.79	-15.91	1.52	92.64	92.64	150.43	150.43
Piede	(4+5)-V-4 (-)	-219.87	17.99	0.00	-15.91	0.00	92.64	92.64	150.43	150.43
Piede	(4+5)-XI-2 (-)	-219.87	17.99	0.00	33.51	0.00	92.64	92.64	150.43	150.43
Piede	(4+5)-XI-2 (+)	-219.87	17.99	-0.79	33.51	-3.26	92.64	92.64	150.43	150.43
Piede	(4+5)-XI-4 (+)	-219.87	17.99	-0.79	-12.89	1.22	92.64	92.64	150.43	150.43
Piede	(4+5)-XI-4 (-)	-219.87	17.99	0.00	-12.89	0.00	92.64	92.64	150.43	150.43
Piede	(4+5)-V-2 (-)	-219.87	17.99	0.00	36.54	0.00	92.64	92.64	150.43	150.43
Piede	(4+5)-V-2 (+)	-219.87	17.99	-0.79	36.54	-3.56	92.64	92.64	150.43	150.43
Piede	(4+5)-I-4 (+)	-211.20	0.83	0.02	-90.50	8.77	91.75	91.75	148.96	148.96
Piede	(4+5)-I-4 (-)	-211.20	0.83	0.00	-90.50	0.00	91.75	91.75	148.96	148.96
Piede	(4+5)-VII-2 (-)	-211.20	0.83	0.00	74.24	0.00	91.75	91.75	148.96	148.96
Piede	(4+5)-VII-2 (+)	-211.20	0.83	0.02	74.24	-7.17	91.75	91.75	148.96	148.96
Piede	(4+5)-III-4 (+)	-211.20	0.83	0.02	-29.31	2.84	91.75	91.75	148.96	148.96
Piede	(4+5)-III-4 (-)	-211.20	0.83	0.00	-29.31	0.00	91.75	91.75	148.96	148.96
Piede	(4+5)-IX-2 (-)	-211.20	0.83	0.00	20.11	0.00	91.75	91.75	148.96	148.96
Piede	(4+5)-IX-2 (+)	-211.20	0.83	0.02	20.11	-1.94	91.75	91.75	148.96	148.96
Piede	(4+5)-IX-4 (+)	-211.20	0.83	0.02	-26.28	2.55	91.75	91.75	148.96	148.96
Piede	(4+5)-IX-4 (-)	-211.20	0.83	0.00	-26.28	0.00	91.75	91.75	148.96	148.96
Piede	(4+5)-III-2 (+)	-211.20	0.83	0.02	23.14	-2.23	91.75	91.75	148.96	148.96
Piede	(4+5)-III-2 (-)	-211.20	0.83	0.00	23.14	0.00	91.75	91.75	148.96	148.96
Piede	(4+5)-VII-4 (-)	-211.20	0.83	0.00	-80.41	0.00	91.75	91.75	148.96	148.96
Piede	(4+5)-VII-4 (+)	-211.20	0.83	0.02	-80.41	7.78	91.75	91.75	148.96	148.96
Piede	(4+5)-I-2 (+)	-211.20	0.83	0.02	84.32	-8.16	91.75	91.75	148.96	148.96
Piede	(4+5)-I-2 (-)	-211.20	0.83	0.00	84.32	0.00	91.75	91.75	148.96	148.96
Piede	(4+5)-IV-4 (-)	-211.20	0.83	0.00	-84.32	0.00	91.75	91.75	148.96	148.96
Piede	(4+5)-IV-4 (+)	-211.20	0.83	0.02	-84.32	8.16	91.75	91.75	148.96	148.96
Piede	(4+5)-X-2 (+)	-211.20	0.83	0.02	80.42	-7.78	91.75	91.75	148.96	148.96
Piede	(4+5)-X-2 (-)	-211.20	0.83	0.00	80.42	0.00	91.75	91.75	148.96	148.96
Piede	(4+5)-VI-4 (-)	-211.20	0.83	0.00	-23.13	0.00	91.75	91.75	148.96	148.96
Piede	(4+5)-VI-4 (+)	-211.20	0.83	0.02	-23.13	2.23	91.75	91.75	148.96	148.96
Piede	(4+5)-XII-2 (-)	-211.20	0.83	0.00	26.29	0.00	91.75	91.75	148.96	148.96
Piede	(4+5)-XII-2 (+)	-211.20	0.83	0.02	26.29	-2.55	91.75	91.75	148.96	148.96
Piede	(4+5)-XII-4 (+)	-211.20	0.83	0.02	-20.10	1.94	91.75	91.75	148.96	148.96
Piede	(4+5)-XII-4 (-)	-211.20	0.83	0.00	-20.10	0.00	91.75	91.75	148.96	148.96
Piede	(4+5)-VI-2 (-)	-211.20	0.83	0.00	29.32	0.00	91.75	91.75	148.96	148.96
Piede	(4+5)-VI-2 (+)	-211.20	0.83	0.02	29.32	-2.85	91.75	91.75	148.96	148.96
Piede	(4+5)-X-4 (-)	-211.20	0.83	0.00	-74.23	0.00	91.75	91.75	148.96	148.96
Piede	(4+5)-X-4 (+)	-211.20	0.83	0.02	-74.23	7.17	91.75	91.75	148.96	148.96
Piede	(4+5)-IV-2 (-)	-211.20	0.83	0.00	90.50	0.00	91.75	91.75	148.96	148.96
Piede	(4+5)-IV-2 (+)	-211.20	0.83	0.02	90.50	-8.77	91.75	91.75	148.96	148.96
Piede	(4+5)-IV-3 (-)	-203.76	-13.87	0.00	-90.50	0.00	90.98	90.98	147.70	147.70
Piede	(4+5)-IV-3 (+)	-203.76	-13.87	0.72	-90.50	8.77	90.98	90.98	147.70	147.70
Piede	(4+5)-X-1 (-)	-203.76	-13.87	0.00	74.23	0.00	90.98	90.98	147.70	147.70
Piede	(4+5)-X-1 (+)	-203.76	-13.87	0.72	74.23	-7.17	90.98	90.98	147.70	147.70
Piede	(4+5)-VI-3 (+)	-203.76	-13.87	0.72	-29.32	2.85	90.98	90.98	147.70	147.70
Piede	(4+5)-VI-3 (-)	-203.76	-13.87	0.00	-29.32	0.00	90.98	90.98	147.70	147.70
Piede	(4+5)-XII-1 (+)	-203.76	-13.87	0.72	20.10	-1.94	90.98	90.98	147.70	147.70
Piede	(4+5)-XII-1 (-)	-203.76	-13.87	0.00	20.10	0.00	90.98	90.98	147.70	147.70
Piede	(4+5)-XII-3 (-)	-203.76	-13.87	0.00	-26.29	0.00	90.98	90.98	147.70	147.70
Piede	(4+5)-XII-3 (+)	-203.76	-13.87	0.72	-26.29	2.55	90.98	90.98	147.70	147.70
Piede	(4+5)-VI-1 (-)	-203.76	-13.87	0.00	23.13	0.00	90.98	90.98	147.70	147.70
Piede	(4+5)-VI-1 (+)	-203.76	-13.87	0.72	23.13	-2.23	90.98	90.98	147.70	147.70
Piede	(4+5)-X-3 (+)	-203.76	-13.87	0.72	-80.42	7.78	90.98	90.98	147.70	147.70
Piede	(4+5)-X-3 (-)	-203.76	-13.87	0.00	-80.42	0.00	90.98	90.98	147.70	147.70
Piede	(4+5)-IV-1 (-)	-203.76	-13.87	0.00	84.32	0.00	90.98	90.98	147.70	147.70
Piede	(4+5)-IV-1 (+)	-203.76	-13.87	0.72	84.32	-8.16	90.98	90.98	147.70	147.70
Piede	(4+5)-I-3 (-)	-203.76	-13.87	0.00	-84.32	0.00	90.98	90.98	147.70	147.70
Piede	(4+5)-I-3 (+)	-203.76	-13.87	0.72	-84.32	8.16	90.98	90.98	147.70	147.70
Piede	(4+5)-VII-1 (-)	-203.76	-13.87	0.00	80.41	0.00	90.98	90.98	147.70	147.70

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 65 di 103

Zona	C.	N	MyCal	ΔMy	MzCal	ΔMz	Mry+	Mry-	Mrz+	Mrz-
Piede	(4+5)-VII-1 (+)	-203.76	-13.87	0.72	80.41	-7.78	90.98	90.98	147.70	147.70
Piede	(4+5)-III-3 (+)	-203.76	-13.87	0.72	-23.14	2.23	90.98	90.98	147.70	147.70
Piede	(4+5)-III-3 (-)	-203.76	-13.87	0.00	-23.14	0.00	90.98	90.98	147.70	147.70
Piede	(4+5)-IX-1 (+)	-203.76	-13.87	0.72	26.28	-2.55	90.98	90.98	147.70	147.70
Piede	(4+5)-IX-1 (-)	-203.76	-13.87	0.00	26.28	0.00	90.98	90.98	147.70	147.70
Piede	(4+5)-IX-3 (-)	-203.76	-13.87	0.00	-20.11	0.00	90.98	90.98	147.70	147.70
Piede	(4+5)-IX-3 (+)	-203.76	-13.87	0.72	-20.11	1.94	90.98	90.98	147.70	147.70
Piede	(4+5)-III-1 (+)	-203.76	-13.87	0.72	29.31	-2.84	90.98	90.98	147.70	147.70
Piede	(4+5)-III-1 (-)	-203.76	-13.87	0.00	29.31	0.00	90.98	90.98	147.70	147.70
Piede	(4+5)-VII-3 (-)	-203.76	-13.87	0.00	-74.24	0.00	90.98	90.98	147.70	147.70
Piede	(4+5)-VII-3 (+)	-203.76	-13.87	0.72	-74.24	7.17	90.98	90.98	147.70	147.70
Piede	(4+5)-I-1 (-)	-203.76	-13.87	0.00	90.50	0.00	90.98	90.98	147.70	147.70
Piede	(4+5)-I-1 (+)	-203.76	-13.87	0.72	90.50	-8.77	90.98	90.98	147.70	147.70
Piede	(4+5)-V-3 (+)	-195.09	-31.03	1.53	-36.54	3.56	90.09	90.09	146.23	146.23
Piede	(4+5)-V-3 (-)	-195.09	-31.03	0.00	-36.54	0.00	90.09	90.09	146.23	146.23
Piede	(4+5)-XI-1 (+)	-195.09	-31.03	1.53	12.89	-1.22	90.09	90.09	146.23	146.23
Piede	(4+5)-XI-1 (-)	-195.09	-31.03	0.00	12.89	0.00	90.09	90.09	146.23	146.23
Piede	(4+5)-XI-3 (-)	-195.09	-31.03	0.00	-33.51	0.00	90.09	90.09	146.23	146.23
Piede	(4+5)-XI-3 (+)	-195.09	-31.03	1.53	-33.51	3.26	90.09	90.09	146.23	146.23
Piede	(4+5)-V-1 (-)	-195.09	-31.03	0.00	15.91	0.00	90.09	90.09	146.23	146.23
Piede	(4+5)-V-1 (+)	-195.09	-31.03	1.53	15.91	-1.52	90.09	90.09	146.23	146.23
Piede	(4+5)-II-3 (+)	-195.08	-31.03	1.53	-15.93	1.52	90.09	90.09	146.23	146.23
Piede	(4+5)-II-3 (-)	-195.08	-31.03	0.00	-15.93	0.00	90.09	90.09	146.23	146.23
Piede	(4+5)-VIII-1 (-)	-195.08	-31.03	0.00	33.49	0.00	90.09	90.09	146.23	146.23
Piede	(4+5)-VIII-1 (+)	-195.08	-31.03	1.53	33.49	-3.26	90.09	90.09	146.23	146.23
Piede	(4+5)-VIII-3 (+)	-195.08	-31.03	1.53	-12.91	1.22	90.09	90.09	146.23	146.23
Piede	(4+5)-VIII-3 (-)	-195.08	-31.03	0.00	-12.91	0.00	90.09	90.09	146.23	146.23
Piede	(4+5)-II-1 (-)	-195.08	-31.03	0.00	36.51	0.00	90.09	90.09	146.23	146.23
Piede	(4+5)-II-1 (+)	-195.08	-31.03	1.53	36.51	-3.56	90.09	90.09	146.23	146.23
Testa	2 (+)	-289.48	10.15	0.00	-7.24	0.02	99.67	99.67	162.00	162.00
Testa	2 (-)	-289.48	10.15	-0.57	-7.24	-0.02	99.67	99.67	162.00	162.00
Testa	3 (+)	-285.04	10.27	0.00	-7.13	0.02	99.23	99.23	161.27	161.27
Testa	3 (-)	-285.04	10.27	-0.58	-7.13	-0.02	99.23	99.23	161.27	161.27
Testa	1 (-)	-261.73	8.91	-0.51	-6.54	-0.02	96.89	96.89	157.42	157.42
Testa	1 (+)	-261.73	8.91	0.00	-6.54	0.02	96.89	96.89	157.42	157.42
Testa	(4+5)-II-4 (-)	-204.88	-9.66	0.79	33.13	-3.56	91.10	91.10	147.89	147.89
Testa	(4+5)-II-4 (+)	-204.88	-9.66	0.00	33.13	0.00	91.10	91.10	147.89	147.89
Testa	(4+5)-VIII-2 (+)	-204.88	-9.66	0.00	-11.06	0.00	91.10	91.10	147.89	147.89
Testa	(4+5)-VIII-2 (-)	-204.88	-9.66	0.79	-11.06	1.22	91.10	91.10	147.89	147.89
Testa	(4+5)-VIII-4 (+)	-204.88	-9.66	0.00	30.33	0.00	91.10	91.10	147.89	147.89
Testa	(4+5)-VIII-4 (-)	-204.88	-9.66	0.79	30.33	-3.26	91.10	91.10	147.89	147.89
Testa	(4+5)-II-2 (-)	-204.88	-9.66	0.79	-13.87	1.52	91.10	91.10	147.89	147.89
Testa	(4+5)-II-2 (+)	-204.88	-9.66	0.00	-13.87	0.00	91.10	91.10	147.89	147.89
Testa	(4+5)-V-4 (+)	-204.87	-9.65	0.00	13.85	0.00	91.10	91.10	147.89	147.89
Testa	(4+5)-V-4 (-)	-204.87	-9.65	0.79	13.85	-1.52	91.10	91.10	147.89	147.89
Testa	(4+5)-XI-2 (-)	-204.87	-9.65	0.79	-30.35	3.26	91.10	91.10	147.89	147.89
Testa	(4+5)-XI-2 (+)	-204.87	-9.65	0.00	-30.35	0.00	91.10	91.10	147.89	147.89
Testa	(4+5)-XI-4 (+)	-204.87	-9.65	0.00	11.04	0.00	91.10	91.10	147.89	147.89
Testa	(4+5)-XI-4 (-)	-204.87	-9.65	0.79	11.04	-1.22	91.10	91.10	147.89	147.89
Testa	(4+5)-V-2 (-)	-204.87	-9.65	0.79	-33.15	3.56	91.10	91.10	147.89	147.89
Testa	(4+5)-V-2 (+)	-204.87	-9.65	0.00	-33.15	0.00	91.10	91.10	147.89	147.89
Testa	(4+5)-I-4 (+)	-196.20	1.61	0.00	81.22	0.00	90.20	90.20	146.42	146.42
Testa	(4+5)-I-4 (-)	-196.20	1.61	-0.02	81.22	-8.77	90.20	90.20	146.42	146.42
Testa	(4+5)-VII-2 (-)	-196.20	1.61	-0.02	-66.10	7.17	90.20	90.20	146.42	146.42
Testa	(4+5)-VII-2 (+)	-196.20	1.61	0.00	-66.10	0.00	90.20	90.20	146.42	146.42
Testa	(4+5)-III-4 (+)	-196.20	1.61	0.00	26.39	0.00	90.20	90.20	146.42	146.42
Testa	(4+5)-III-4 (-)	-196.20	1.61	-0.02	26.39	-2.84	90.20	90.20	146.42	146.42
Testa	(4+5)-IX-2 (-)	-196.20	1.61	-0.02	-17.81	1.94	90.20	90.20	146.42	146.42
Testa	(4+5)-IX-2 (+)	-196.20	1.61	0.00	-17.81	0.00	90.20	90.20	146.42	146.42
Testa	(4+5)-IX-4 (+)	-196.20	1.61	0.00	23.59	0.00	90.20	90.20	146.42	146.42
Testa	(4+5)-IX-4 (-)	-196.20	1.61	-0.02	23.59	-2.55	90.20	90.20	146.42	146.42
Testa	(4+5)-III-2 (+)	-196.20	1.61	0.00	-20.61	0.00	90.20	90.20	146.42	146.42
Testa	(4+5)-III-2 (-)	-196.20	1.61	-0.02	-20.61	2.23	90.20	90.20	146.42	146.42
Testa	(4+5)-VII-4 (-)	-196.20	1.61	-0.02	71.88	-7.78	90.20	90.20	146.42	146.42
Testa	(4+5)-VII-4 (+)	-196.20	1.61	0.00	71.88	0.00	90.20	90.20	146.42	146.42
Testa	(4+5)-I-2 (+)	-196.20	1.61	0.00	-75.44	0.00	90.20	90.20	146.42	146.42
Testa	(4+5)-I-2 (-)	-196.20	1.61	-0.02	-75.44	8.16	90.20	90.20	146.42	146.42
Testa	(4+5)-IV-4 (-)	-196.20	1.61	-0.02	75.44	-8.16	90.20	90.20	146.42	146.42
Testa	(4+5)-IV-4 (+)	-196.20	1.61	0.00	75.44	0.00	90.20	90.20	146.42	146.42
Testa	(4+5)-X-2 (+)	-196.20	1.61	0.00	-71.89	0.00	90.20	90.20	146.42	146.42
Testa	(4+5)-X-2 (-)	-196.20	1.61	-0.02	-71.89	7.78	90.20	90.20	146.42	146.42
Testa	(4+5)-VI-4 (-)	-196.20	1.61	-0.02	20.60	-2.23	90.20	90.20	146.42	146.42
Testa	(4+5)-VI-4 (+)	-196.20	1.61	0.00	20.60	0.00	90.20	90.20	146.42	146.42
Testa	(4+5)-XII-2 (-)	-196.20	1.61	-0.02	-23.59	2.55	90.20	90.20	146.42	146.42
Testa	(4+5)-XII-2 (+)	-196.20	1.61	0.00	-23.59	0.00	90.20	90.20	146.42	146.42
Testa	(4+5)-XII-4 (+)	-196.20	1.61	0.00	17.80	0.00	90.20	90.20	146.42	146.42

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021
Pagina 66 di 103

Zona	C.	N	MyCal	ΔMy	MzCal	ΔMz	Mry+	Mry-	Mrz+	Mrz-
Testa	(4+5)-XII-4 (-)	-196.20	1.61	-0.02	17.80	-1.94	90.20	90.20	146.42	146.42
Testa	(4+5)-VI-2 (-)	-196.20	1.61	-0.02	-26.40	2.85	90.20	90.20	146.42	146.42
Testa	(4+5)-VI-2 (+)	-196.20	1.61	0.00	-26.40	0.00	90.20	90.20	146.42	146.42
Testa	(4+5)-X-4 (-)	-196.20	1.61	-0.02	66.10	-7.17	90.20	90.20	146.42	146.42
Testa	(4+5)-X-4 (+)	-196.20	1.61	0.00	66.10	0.00	90.20	90.20	146.42	146.42
Testa	(4+5)-IV-2 (-)	-196.20	1.61	-0.02	-81.23	8.77	90.20	90.20	146.42	146.42
Testa	(4+5)-IV-2 (+)	-196.20	1.61	0.00	-81.23	0.00	90.20	90.20	146.42	146.42
Testa	(4+5)-IV-3 (-)	-188.76	11.27	-0.72	81.23	-8.77	89.43	89.43	145.15	145.15
Testa	(4+5)-IV-3 (+)	-188.76	11.27	0.00	81.23	0.00	89.43	89.43	145.15	145.15
Testa	(4+5)-X-1 (-)	-188.76	11.27	-0.72	-66.10	7.17	89.43	89.43	145.15	145.15
Testa	(4+5)-X-1 (+)	-188.76	11.27	0.00	-66.10	0.00	89.43	89.43	145.15	145.15
Testa	(4+5)-VI-3 (+)	-188.76	11.27	0.00	26.40	0.00	89.43	89.43	145.15	145.15
Testa	(4+5)-VI-3 (-)	-188.76	11.27	-0.72	26.40	-2.85	89.43	89.43	145.15	145.15
Testa	(4+5)-XII-1 (+)	-188.76	11.27	0.00	-17.80	0.00	89.43	89.43	145.15	145.15
Testa	(4+5)-XII-1 (-)	-188.76	11.27	-0.72	-17.80	1.94	89.43	89.43	145.15	145.15
Testa	(4+5)-XII-3 (-)	-188.76	11.27	-0.72	23.59	-2.55	89.43	89.43	145.15	145.15
Testa	(4+5)-XII-3 (+)	-188.76	11.27	0.00	23.59	0.00	89.43	89.43	145.15	145.15
Testa	(4+5)-VI-1 (-)	-188.76	11.27	-0.72	-20.60	2.23	89.43	89.43	145.15	145.15
Testa	(4+5)-VI-1 (+)	-188.76	11.27	0.00	-20.60	0.00	89.43	89.43	145.15	145.15
Testa	(4+5)-X-3 (+)	-188.76	11.27	0.00	71.89	0.00	89.43	89.43	145.15	145.15
Testa	(4+5)-X-3 (-)	-188.76	11.27	-0.72	71.89	-7.78	89.43	89.43	145.15	145.15
Testa	(4+5)-IV-1 (-)	-188.76	11.27	-0.72	-75.44	8.16	89.43	89.43	145.15	145.15
Testa	(4+5)-IV-1 (+)	-188.76	11.27	0.00	-75.44	0.00	89.43	89.43	145.15	145.15
Testa	(4+5)-I-3 (-)	-188.76	11.27	-0.72	75.44	-8.16	89.43	89.43	145.15	145.15
Testa	(4+5)-I-3 (+)	-188.76	11.27	0.00	75.44	0.00	89.43	89.43	145.15	145.15
Testa	(4+5)-VII-1 (-)	-188.76	11.27	-0.72	-71.88	7.78	89.43	89.43	145.15	145.15
Testa	(4+5)-VII-1 (+)	-188.76	11.27	0.00	-71.88	0.00	89.43	89.43	145.15	145.15
Testa	(4+5)-III-3 (+)	-188.76	11.27	0.00	20.61	0.00	89.43	89.43	145.15	145.15
Testa	(4+5)-III-3 (-)	-188.76	11.27	-0.72	20.61	-2.23	89.43	89.43	145.15	145.15
Testa	(4+5)-IX-1 (+)	-188.76	11.27	0.00	-23.59	0.00	89.43	89.43	145.15	145.15
Testa	(4+5)-IX-1 (-)	-188.76	11.27	-0.72	-23.59	2.55	89.43	89.43	145.15	145.15
Testa	(4+5)-IX-3 (-)	-188.76	11.27	-0.72	17.81	-1.94	89.43	89.43	145.15	145.15
Testa	(4+5)-IX-3 (+)	-188.76	11.27	0.00	17.81	0.00	89.43	89.43	145.15	145.15
Testa	(4+5)-III-1 (+)	-188.76	11.27	0.00	-26.39	0.00	89.43	89.43	145.15	145.15
Testa	(4+5)-III-1 (-)	-188.76	11.27	-0.72	-26.39	2.84	89.43	89.43	145.15	145.15
Testa	(4+5)-VII-3 (-)	-188.76	11.27	-0.72	66.10	-7.17	89.43	89.43	145.15	145.15
Testa	(4+5)-VII-3 (+)	-188.76	11.27	0.00	66.10	0.00	89.43	89.43	145.15	145.15
Testa	(4+5)-I-1 (-)	-188.76	11.27	-0.72	-81.22	8.77	89.43	89.43	145.15	145.15
Testa	(4+5)-I-1 (+)	-188.76	11.27	0.00	-81.22	0.00	89.43	89.43	145.15	145.15
Testa	(4+5)-V-3 (+)	-180.09	22.53	0.00	33.15	0.00	88.53	88.53	143.67	143.67
Testa	(4+5)-V-3 (-)	-180.09	22.53	-1.53	33.15	-3.56	88.53	88.53	143.67	143.67
Testa	(4+5)-XI-1 (+)	-180.09	22.53	0.00	-11.04	0.00	88.53	88.53	143.67	143.67
Testa	(4+5)-XI-1 (-)	-180.09	22.53	-1.53	-11.04	1.22	88.53	88.53	143.67	143.67
Testa	(4+5)-XI-3 (-)	-180.09	22.53	-1.53	30.35	-3.26	88.53	88.53	143.67	143.67
Testa	(4+5)-XI-3 (+)	-180.09	22.53	0.00	30.35	0.00	88.53	88.53	143.67	143.67
Testa	(4+5)-V-1 (-)	-180.09	22.53	-1.53	-13.85	1.52	88.53	88.53	143.67	143.67
Testa	(4+5)-V-1 (+)	-180.09	22.53	0.00	-13.85	0.00	88.53	88.53	143.67	143.67
Testa	(4+5)-II-3 (+)	-180.08	22.53	0.00	13.87	0.00	88.53	88.53	143.67	143.67
Testa	(4+5)-II-3 (-)	-180.08	22.53	-1.53	13.87	-1.52	88.53	88.53	143.67	143.67
Testa	(4+5)-VIII-1 (-)	-180.08	22.53	-1.53	-30.33	3.26	88.53	88.53	143.67	143.67
Testa	(4+5)-VIII-1 (+)	-180.08	22.53	0.00	-30.33	0.00	88.53	88.53	143.67	143.67
Testa	(4+5)-VIII-3 (+)	-180.08	22.53	0.00	11.06	0.00	88.53	88.53	143.67	143.67
Testa	(4+5)-VIII-3 (-)	-180.08	22.53	-1.53	11.06	-1.22	88.53	88.53	143.67	143.67
Testa	(4+5)-II-1 (-)	-180.08	22.53	-1.53	-33.13	3.56	88.53	88.53	143.67	143.67
Testa	(4+5)-II-1 (+)	-180.08	22.53	0.00	-33.13	0.00	88.53	88.53	143.67	143.67

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot (θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(4+5)-IV-2	--	--	42.93	--	477.07	373.73	373.73	9.35	2.500	8.7
Z	(4+5)-II-1	--	--	13.39	--	442.73	209.09	209.09	9.35	2.500	16

Pilastro: 3 [3,103] Sez. R: By=30.00 cm Bz=50.00 cm L=400.00 cm Ln=400.00 cm Criterio: CLS_Pilastri_ND - Verifica a presso-flessione deviata, $\zeta_E=1.336$ [(4+5)-II-1] : **Verificato**

Piede	AfSpigolo = 3.14	Afy = 0.00	Afz = 1.54
Testa	AfSpigolo = 3.14	Afy = 0.00	Afz = 1.54

$v_{max}=N/(fcd*A)=0.043 \leq 0.65$ [Comb. (4+5)-VIII-2(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	2(+)	-159.79	-8.62	2.11	140.19	86.42	140.19	86.42	18
Piede	2(-)	-159.79	-9.14	3.20	140.19	86.42	140.19	86.42	17

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 67 di 103

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
Piede	3(+)	-159.15	-8.56	2.10	140.08	86.35	140.08	86.35	18
Piede	3(-)	-159.15	-9.08	3.18	140.08	86.35	140.08	86.35	17
Piede	1(-)	-147.96	-8.28	2.96	138.14	85.17	138.14	85.17	18
Piede	1(+)	-147.96	-7.82	1.96	138.14	85.17	138.14	85.17	19
Piede	(4+5)-VIII-2(+)	-137.92	63.51	1.51	136.40	84.12	136.40	84.12	2.8
Piede	(4+5)-VIII-2(-)	-137.92	70.31	1.77	136.40	84.12	136.40	84.12	2.4
Piede	(4+5)-II-2(+)	-137.15	58.84	2.69	136.27	84.03	136.27	84.03	3.0
Piede	(4+5)-II-2(-)	-137.15	65.15	3.01	136.27	84.03	136.27	84.03	2.6
Piede	(4+5)-XI-2(-)	-132.05	46.08	11.38	135.38	83.50	135.38	83.50	3.5
Piede	(4+5)-XI-2(+)	-132.05	41.57	10.58	135.38	83.50	135.38	83.50	4.1
Piede	(4+5)-VII-2(+)	-131.66	20.16	25.90	135.31	83.46	135.31	83.46	3.7
Piede	(4+5)-VII-2(-)	-131.66	22.50	27.59	135.31	83.46	135.31	83.46	3.3
Piede	(4+5)-V-2(+)	-131.27	36.90	11.76	135.24	83.41	135.24	83.41	4.5
Piede	(4+5)-V-2(-)	-131.27	40.91	12.62	135.24	83.41	135.24	83.41	3.9
Piede	(4+5)-II-4(+)	-130.10	64.80	-16.28	135.04	83.29	135.04	83.29	2.1
Piede	(4+5)-II-4(-)	-130.10	71.75	-17.08	135.04	83.29	135.04	83.29	1.8
Piede	(4+5)-X-2(+)	-129.90	13.57	28.62	135.01	83.27	135.01	83.27	3.6
Piede	(4+5)-X-2(-)	-129.90	15.23	30.48	135.01	83.27	135.01	83.27	3.3
Piede	(4+5)-VIII-4(+)	-129.33	60.13	-15.10	134.90	83.21	134.90	83.21	2.3
Piede	(4+5)-VIII-4(-)	-129.33	66.58	-15.83	134.90	83.21	134.90	83.21	2.0
Piede	(4+5)-I-2(-)	-129.08	5.28	31.75	134.86	83.18	134.86	83.18	3.5
Piede	(4+5)-I-2(+)	-129.08	4.57	29.82	134.86	83.18	134.86	83.18	3.9
Piede	(4+5)-IV-2(+)	-127.32	-2.01	32.54	134.55	83.00	134.55	83.00	3.5
Piede	(4+5)-IV-2(-)	-127.32	-2.00	34.64	134.55	83.00	134.55	83.00	3.2
Piede	(4+5)-V-4(-)	-124.23	47.51	-7.47	134.01	82.67	134.01	82.67	3.6
Piede	(4+5)-V-4(+)	-124.23	42.86	-7.21	134.01	82.67	134.01	82.67	4.1
Piede	(4+5)-XI-4(+)	-123.46	38.18	-6.03	133.88	82.59	133.88	82.59	5.1
Piede	(4+5)-XI-4(-)	-123.46	42.34	-6.22	133.88	82.59	133.88	82.59	4.3
Piede	(4+5)-IX-2(-)	-121.64	18.14	7.07	133.56	82.39	133.56	82.39	12
Piede	(4+5)-IX-2(+)	-121.64	16.21	6.51	133.56	82.39	133.56	82.39	13
Piede	(4+5)-III-2(+)	-120.87	11.53	7.69	133.43	82.31	133.43	82.31	14
Piede	(4+5)-III-2(-)	-120.87	12.97	8.31	133.43	82.31	133.43	82.31	13
Piede	(4+5)-XII-2(-)	-119.88	10.87	9.95	133.25	82.21	133.25	82.21	13
Piede	(4+5)-XII-2(+)	-119.88	9.62	9.23	133.25	82.21	133.25	82.21	14
Piede	(4+5)-X-1(-)	-119.47	-14.96	29.25	133.18	82.16	133.18	82.16	3.3
Piede	(4+5)-X-1(+)	-119.47	-13.81	27.46	133.18	82.16	133.18	82.16	3.7
Piede	(4+5)-VI-2(+)	-119.11	5.70	11.20	133.12	82.12	133.12	82.12	13
Piede	(4+5)-VI-2(-)	-119.11	4.95	10.41	133.12	82.12	133.12	82.12	14
Piede	(4+5)-VII-1(-)	-117.71	-22.23	32.14	132.87	81.97	132.87	81.97	2.7
Piede	(4+5)-VII-1(+)	-117.71	-20.39	30.18	132.87	81.97	132.87	81.97	2.9
Piede	(4+5)-IV-1(-)	-116.89	-32.18	33.41	132.73	81.89	132.73	81.89	2.2
Piede	(4+5)-IV-1(+)	-116.89	-29.40	31.39	132.73	81.89	132.73	81.89	2.5
Piede	(4+5)-I-1(-)	-115.13	-39.45	36.29	132.42	81.70	132.42	81.70	1.9
Piede	(4+5)-I-1(+)	-115.13	-35.98	34.11	132.42	81.70	132.42	81.70	2.1
Piede	(4+5)-III-4(+)	-113.82	17.49	-11.28	132.19	81.56	132.19	81.56	8.9
Piede	(4+5)-III-4(-)	-113.82	19.57	-11.78	132.19	81.56	132.19	81.56	7.9
Piede	(4+5)-IX-4(+)	-113.05	14.40	-10.53	132.06	81.48	132.06	81.48	11
Piede	(4+5)-IX-4(-)	-113.05	12.82	-10.10	132.06	81.48	132.06	81.48	12
Piede	(4+5)-VI-4(+)	-112.06	10.91	-8.56	131.88	81.37	131.88	81.37	14
Piede	(4+5)-VI-4(-)	-112.06	12.30	-8.89	131.88	81.37	131.88	81.37	13
Piede	(4+5)-XII-4(-)	-111.29	7.13	-7.65	131.75	81.29	131.75	81.29	17
Piede	(4+5)-XII-4(+)	-111.29	6.24	-7.38	131.75	81.29	131.75	81.29	17
Piede	(4+5)-XII-1(-)	-109.45	-19.31	8.73	131.42	81.09	131.42	81.09	9.6
Piede	(4+5)-XII-1(+)	-109.45	-17.76	8.08	131.42	81.09	131.42	81.09	11
Piede	(4+5)-VI-1(+)	-108.67	-22.44	9.26	131.29	81.01	131.29	81.01	8.0
Piede	(4+5)-VI-1(-)	-108.67	-24.48	9.97	131.29	81.01	131.29	81.01	7.0
Piede	(4+5)-IX-1(+)	-107.69	-24.34	10.80	131.11	80.91	131.11	80.91	6.7
Piede	(4+5)-IX-1(-)	-107.69	-26.58	11.61	131.11	80.91	131.11	80.91	5.8
Piede	(4+5)-III-1(-)	-106.91	-31.75	12.86	130.98	80.82	130.98	80.82	4.6
Piede	(4+5)-III-1(+)	-106.91	-29.02	11.98	130.98	80.82	130.98	80.82	5.2
Piede	(4+5)-I-4(+)	-105.61	24.45	-33.40	130.75	80.68	130.75	80.68	2.4
Piede	(4+5)-I-4(-)	-105.61	27.27	-35.22	130.75	80.68	130.75	80.68	2.2
Piede	(4+5)-IV-4(-)	-103.84	19.99	-32.33	130.44	80.50	130.44	80.50	2.6
Piede	(4+5)-IV-4(+)	-103.84	17.87	-30.69	130.44	80.50	130.44	80.50	2.8
Piede	(4+5)-VII-4(-)	-103.03	10.04	-31.06	130.29	80.41	130.29	80.41	3.1
Piede	(4+5)-VII-4(+)	-103.03	8.87	-29.48	130.29	80.41	130.29	80.41	3.3
Piede	(4+5)-VI-3(+)	-101.63	-16.47	-9.71	130.05	80.26	130.05	80.26	9.8
Piede	(4+5)-VI-3(-)	-101.63	-17.88	-10.12	130.05	80.26	130.05	80.26	9.0
Piede	(4+5)-X-4(-)	-101.26	2.77	-28.17	129.98	80.22	129.98	80.22	3.8
Piede	(4+5)-X-4(+)	-101.26	2.29	-26.76	129.98	80.22	129.98	80.22	4.2
Piede	(4+5)-XII-3(+)	-100.86	-21.15	-8.53	129.91	80.18	129.91	80.18	8.6
Piede	(4+5)-XII-3(-)	-100.86	-23.05	-8.87	129.91	80.18	129.91	80.18	7.6
Piede	(4+5)-III-3(-)	-99.87	-25.15	-7.23	129.74	80.07	129.74	80.07	7.4
Piede	(4+5)-III-3(+)	-99.87	-23.05	-6.99	129.74	80.07	129.74	80.07	8.4
Piede	(4+5)-IX-3(+)	-99.10	-27.73	-5.81	129.60	79.99	129.60	79.99	7.0
Piede	(4+5)-IX-3(-)	-99.10	-30.32	-5.99	129.60	79.99	129.60	79.99	6.1

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 68 di 103

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
Piede	(4+5)-XI-1 (-)	-97.28	-54.52	7.30	129.28	79.79	129.28	79.79	2.7
Piede	(4+5)-XI-1 (+)	-97.28	-49.71	6.73	129.28	79.79	129.28	79.79	3.0
Piede	(4+5)-V-1 (-)	-96.51	-59.69	8.55	129.14	79.71	129.14	79.71	2.3
Piede	(4+5)-V-1 (+)	-96.51	-54.39	7.91	129.14	79.71	129.14	79.71	2.6
Piede	(4+5)-IV-3 (-)	-93.41	-10.19	-33.56	128.60	79.38	128.60	79.38	2.7
Piede	(4+5)-IV-3 (+)	-93.41	-9.51	-31.84	128.60	79.38	128.60	79.38	2.9
Piede	(4+5)-I-3 (-)	-91.65	-17.46	-30.67	128.28	79.19	128.28	79.19	2.7
Piede	(4+5)-I-3 (+)	-91.65	-16.10	-29.12	128.28	79.19	128.28	79.19	2.9
Piede	(4+5)-VIII-1 (-)	-91.41	-78.76	16.91	128.24	79.16	128.24	79.16	1.5
Piede	(4+5)-VIII-1 (+)	-91.41	-71.65	15.80	128.24	79.16	128.24	79.16	1.7
Piede	(4+5)-X-3 (-)	-90.83	-27.41	-29.40	128.14	79.10	128.14	79.10	2.5
Piede	(4+5)-X-3 (+)	-90.83	-25.10	-27.92	128.14	79.10	128.14	79.10	2.7
Piede	(4+5)-II-1 (+)	-90.63	-76.33	16.98	128.10	79.08	128.10	79.08	1.6
Piede	(4+5)-II-1 (-)	-90.63	-83.93	18.16	128.10	79.08	128.10	79.08	1.4
Piede	(4+5)-V-3 (+)	-89.46	-48.42	-11.06	127.90	78.95	127.90	78.95	2.8
Piede	(4+5)-V-3 (-)	-89.46	-53.09	-11.54	127.90	78.95	127.90	78.95	2.5
Piede	(4+5)-VII-3 (-)	-89.07	-34.68	-26.51	127.83	78.91	127.83	78.91	2.4
Piede	(4+5)-VII-3 (+)	-89.07	-31.68	-25.20	127.83	78.91	127.83	78.91	2.6
Piede	(4+5)-XI-3 (-)	-88.69	-58.26	-10.30	127.76	78.87	127.76	78.87	2.3
Piede	(4+5)-XI-3 (+)	-88.69	-53.10	-9.88	127.76	78.87	127.76	78.87	2.5
Piede	(4+5)-X-3 (-)	-83.59	-77.33	-1.94	126.85	78.32	126.85	78.32	1.8
Piede	(4+5)-II-3 (+)	-83.59	-70.36	-1.99	126.85	78.32	126.85	78.32	2.0
Piede	(4+5)-VIII-3 (-)	-82.82	-82.50	-0.69	126.72	78.24	126.72	78.24	1.6
Piede	(4+5)-VIII-3 (+)	-82.82	-75.04	-0.81	126.72	78.24	126.72	78.24	1.8
Testa	2 (+)	-140.29	3.51	-9.85	136.81	84.37	136.81	84.37	15
Testa	2 (-)	-140.29	1.33	-9.53	136.81	84.37	136.81	84.37	15
Testa	3 (+)	-139.65	3.49	-9.44	136.70	84.30	136.70	84.30	15
Testa	3 (-)	-139.65	1.33	-9.14	136.70	84.30	136.70	84.30	16
Testa	1 (-)	-128.46	1.22	-8.10	134.75	83.12	134.75	83.12	17
Testa	1 (+)	-128.46	3.21	-8.36	134.75	83.12	134.75	83.12	17
Testa	(4+5)-VIII-2 (+)	-122.92	-62.87	-7.09	133.79	82.53	133.79	82.53	2.5
Testa	(4+5)-VIII-2 (-)	-122.92	-56.07	-6.83	133.79	82.53	133.79	82.53	2.9
Testa	(4+5)-II-2 (+)	-122.15	-58.43	-8.30	133.65	82.45	133.65	82.45	2.6
Testa	(4+5)-II-2 (-)	-122.15	-52.11	-7.98	133.65	82.45	133.65	82.45	3.1
Testa	(4+5)-XI-2 (-)	-117.05	-37.66	-15.64	132.76	81.90	132.76	81.90	3.6
Testa	(4+5)-XI-2 (+)	-117.05	-42.17	-16.44	132.76	81.90	132.76	81.90	3.2
Testa	(4+5)-VII-2 (+)	-116.66	-23.32	-31.81	132.69	81.86	132.69	81.86	2.6
Testa	(4+5)-VII-2 (-)	-116.66	-20.98	-30.11	132.69	81.86	132.69	81.86	2.9
Testa	(4+5)-V-2 (+)	-116.27	-37.73	-17.66	132.62	81.82	132.62	81.82	3.4
Testa	(4+5)-V-2 (-)	-116.27	-33.71	-16.79	132.62	81.82	132.62	81.82	3.9
Testa	(4+5)-II-4 (+)	-115.10	-64.21	10.90	132.42	81.70	132.42	81.70	2.2
Testa	(4+5)-II-4 (-)	-115.10	-57.27	10.10	132.42	81.70	132.42	81.70	2.5
Testa	(4+5)-X-2 (+)	-114.90	-17.11	-34.61	132.38	81.68	132.38	81.68	2.6
Testa	(4+5)-X-2 (-)	-114.90	-15.46	-32.75	132.38	81.68	132.38	81.68	2.8
Testa	(4+5)-VIII-4 (+)	-114.33	-59.77	9.68	132.28	81.61	132.28	81.61	2.4
Testa	(4+5)-VIII-4 (-)	-114.33	-53.32	8.95	132.28	81.61	132.28	81.61	2.8
Testa	(4+5)-I-2 (-)	-114.08	-7.81	-33.94	132.24	81.59	132.24	81.59	2.9
Testa	(4+5)-I-2 (+)	-114.08	-8.51	-35.87	132.24	81.59	132.24	81.59	2.7
Testa	(4+5)-IV-2 (+)	-112.32	-2.31	-38.68	131.93	81.40	131.93	81.40	2.6
Testa	(4+5)-IV-2 (-)	-112.32	-2.29	-36.58	131.93	81.40	131.93	81.40	2.8
Testa	(4+5)-V-4 (-)	-109.23	-38.87	1.29	131.39	81.07	131.39	81.07	5.2
Testa	(4+5)-V-4 (+)	-109.23	-43.52	1.55	131.39	81.07	131.39	81.07	4.3
Testa	(4+5)-XI-4 (+)	-108.46	-39.07	0.33	131.25	80.99	131.25	80.99	5.2
Testa	(4+5)-XI-4 (-)	-108.46	-34.92	0.14	131.25	80.99	131.25	80.99	6.4
Testa	(4+5)-IX-2 (-)	-106.64	-17.77	-11.70	130.93	80.79	130.93	80.79	8.3
Testa	(4+5)-IX-2 (+)	-106.64	-19.71	-12.25	130.93	80.79	130.93	80.79	7.4
Testa	(4+5)-III-2 (+)	-105.87	-15.27	-13.47	130.79	80.71	130.79	80.71	7.9
Testa	(4+5)-III-2 (-)	-105.87	-13.82	-12.84	130.79	80.71	130.79	80.71	8.8
Testa	(4+5)-XII-2 (-)	-104.88	-12.25	-14.34	130.62	80.61	130.62	80.61	8.2
Testa	(4+5)-XII-2 (+)	-104.88	-13.50	-15.05	130.62	80.61	130.62	80.61	7.4
Testa	(4+5)-X-1 (-)	-104.47	6.32	-31.64	130.55	80.56	130.55	80.56	3.2
Testa	(4+5)-X-1 (+)	-104.47	7.46	-33.43	130.55	80.56	130.55	80.56	2.9
Testa	(4+5)-VI-2 (-)	-104.11	-8.30	-15.49	130.48	80.52	130.48	80.52	8.4
Testa	(4+5)-VI-2 (+)	-104.11	-9.06	-16.27	130.48	80.52	130.48	80.52	7.7
Testa	(4+5)-VII-1 (-)	-102.71	11.84	-34.28	130.24	80.37	130.24	80.37	2.6
Testa	(4+5)-VII-1 (+)	-102.71	13.67	-36.23	130.24	80.37	130.24	80.37	2.4
Testa	(4+5)-IV-1 (-)	-101.89	19.49	-35.46	130.09	80.29	130.09	80.29	2.3
Testa	(4+5)-IV-1 (+)	-101.89	22.27	-37.49	130.09	80.29	130.09	80.29	2.1
Testa	(4+5)-I-1 (-)	-100.13	25.01	-38.11	129.78	80.10	129.78	80.10	2.0
Testa	(4+5)-I-1 (+)	-100.13	28.48	-40.30	129.78	80.10	129.78	80.10	1.8
Testa	(4+5)-III-4 (+)	-98.82	-21.05	5.74	129.55	79.96	129.55	79.96	10
Testa	(4+5)-III-4 (-)	-98.82	-18.98	5.24	129.55	79.96	129.55	79.96	12
Testa	(4+5)-IX-4 (-)	-98.05	-15.03	4.09	129.42	79.88	129.42	79.88	16
Testa	(4+5)-IX-4 (+)	-98.05	-16.61	4.52	129.42	79.88	129.42	79.88	14
Testa	(4+5)-VI-4 (+)	-97.06	-14.84	2.93	129.24	79.77	129.24	79.77	17
Testa	(4+5)-VI-4 (-)	-97.06	-13.46	2.59	129.24	79.77	129.24	79.77	18

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 69 di 103

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
Testa	(4+5)-XII-4 (-)	-96.29	-9.51	1.44	129.10	79.69	129.10	79.69	24
Testa	(4+5)-XII-4 (+)	-96.29	-10.40	1.71	129.10	79.69	129.10	79.69	22
Testa	(4+5)-XII-1 (-)	-94.45	9.53	-13.22	128.78	79.49	128.78	79.49	9.4
Testa	(4+5)-XII-1 (+)	-94.45	11.08	-13.87	128.78	79.49	128.78	79.49	8.3
Testa	(4+5)-VI-1 (+)	-93.67	15.52	-15.09	128.64	79.41	128.64	79.41	6.4
Testa	(4+5)-VI-1 (-)	-93.67	13.48	-14.37	128.64	79.41	128.64	79.41	7.3
Testa	(4+5)-IX-1 (+)	-92.69	17.29	-16.67	128.47	79.30	128.47	79.30	5.4
Testa	(4+5)-IX-1 (-)	-92.69	15.05	-15.87	128.47	79.30	128.47	79.30	6.1
Testa	(4+5)-III-1 (-)	-91.91	19.00	-17.01	128.33	79.22	128.33	79.22	5.0
Testa	(4+5)-III-1 (+)	-91.91	21.73	-17.89	128.33	79.22	128.33	79.22	4.4
Testa	(4+5)-I-4 (+)	-90.61	-27.80	28.14	128.10	79.08	128.10	79.08	2.6
Testa	(4+5)-I-4 (-)	-90.61	-24.99	26.33	128.10	79.08	128.10	79.08	2.8
Testa	(4+5)-IV-4 (-)	-88.84	-19.47	23.69	127.79	78.89	127.79	78.89	3.4
Testa	(4+5)-IV-4 (+)	-88.84	-21.59	25.33	127.79	78.89	127.79	78.89	3.1
Testa	(4+5)-VII-4 (-)	-88.03	-11.82	22.50	127.64	78.80	127.64	78.80	4.2
Testa	(4+5)-VII-4 (+)	-88.03	-13.00	24.08	127.64	78.80	127.64	78.80	3.8
Testa	(4+5)-VI-3 (+)	-86.63	9.73	4.12	127.39	78.65	127.39	78.65	20
Testa	(4+5)-VI-3 (-)	-86.63	8.32	3.71	127.39	78.65	127.39	78.65	23
Testa	(4+5)-X-4 (-)	-86.26	-6.30	19.86	127.33	78.61	127.33	78.61	5.5
Testa	(4+5)-X-4 (+)	-86.26	-6.79	21.27	127.33	78.61	127.33	78.61	4.9
Testa	(4+5)-XII-3 (+)	-85.86	14.18	2.90	127.26	78.57	127.26	78.57	18
Testa	(4+5)-XII-3 (-)	-85.86	12.27	2.56	127.26	78.57	127.26	78.57	20
Testa	(4+5)-III-3 (-)	-84.87	13.84	1.07	127.08	78.46	127.08	78.46	20
Testa	(4+5)-III-3 (+)	-84.87	15.94	1.31	127.08	78.46	127.08	78.46	17
Testa	(4+5)-IX-3 (+)	-84.10	20.38	0.09	126.94	78.38	126.94	78.38	13
Testa	(4+5)-IX-3 (-)	-84.10	17.79	-0.08	126.94	78.38	126.94	78.38	16
Testa	(4+5)-XI-1 (-)	-82.28	34.94	-11.92	126.62	78.18	126.62	78.18	3.7
Testa	(4+5)-XI-1 (+)	-82.28	39.75	-12.48	126.62	78.18	126.62	78.18	3.2
Testa	(4+5)-V-1 (-)	-81.51	38.89	-13.07	126.48	78.10	126.48	78.10	3.2
Testa	(4+5)-V-1 (+)	-81.51	44.19	-13.70	126.48	78.10	126.48	78.10	2.8
Testa	(4+5)-IV-3 (-)	-78.41	2.31	24.80	125.93	77.76	125.93	77.76	4.1
Testa	(4+5)-IV-3 (+)	-78.41	2.98	26.52	125.93	77.76	125.93	77.76	3.7
Testa	(4+5)-I-3 (-)	-76.65	7.83	22.16	125.62	77.57	125.62	77.57	4.3
Testa	(4+5)-I-3 (+)	-76.65	9.19	23.71	125.62	77.57	125.62	77.57	3.9
Testa	(4+5)-VIII-1 (-)	-76.41	53.34	-20.73	125.58	77.55	125.58	77.55	2.0
Testa	(4+5)-VIII-1 (+)	-76.41	60.45	-21.84	125.58	77.55	125.58	77.55	1.7
Testa	(4+5)-X-3 (-)	-75.83	15.48	20.98	125.48	77.48	125.48	77.48	4.0
Testa	(4+5)-X-3 (+)	-75.83	17.79	22.46	125.48	77.48	125.48	77.48	3.5
Testa	(4+5)-II-1 (+)	-75.63	64.89	-23.06	125.44	77.46	125.44	77.46	1.6
Testa	(4+5)-II-1 (-)	-75.63	57.29	-21.88	125.44	77.46	125.44	77.46	1.8
Testa	(4+5)-V-3 (+)	-74.46	38.41	5.50	125.23	77.34	125.23	77.34	3.9
Testa	(4+5)-V-3 (-)	-74.46	33.73	5.01	125.23	77.34	125.23	77.34	4.6
Testa	(4+5)-VII-3 (-)	-74.07	21.00	18.33	125.16	77.29	125.16	77.29	4.0
Testa	(4+5)-VII-3 (+)	-74.07	24.00	19.65	125.16	77.29	125.16	77.29	3.5
Testa	(4+5)-XI-3 (-)	-73.69	37.68	3.87	125.09	77.25	125.09	77.25	4.1
Testa	(4+5)-XI-3 (+)	-73.69	42.85	4.28	125.09	77.25	125.09	77.25	3.5
Testa	(4+5)-II-3 (-)	-68.59	52.13	-3.80	124.18	76.70	124.18	76.70	2.7
Testa	(4+5)-II-3 (+)	-68.59	59.10	-3.85	124.18	76.70	124.18	76.70	2.3
Testa	(4+5)-VIII-3 (-)	-67.82	56.09	-4.95	124.05	76.62	124.05	76.62	2.4
Testa	(4+5)-VIII-3 (+)	-67.82	63.54	-5.07	124.05	76.62	124.05	76.62	2.1

Zona	C.	N	MyCal	ΔMy	MzCal	ΔMz	Mry+	Mry-	Mrz+	Mrz-
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m
Piede	2 (+)	-159.79	-9.14	0.53	3.20	-1.08	140.19	140.19	86.42	86.42
Piede	2 (-)	-159.79	-9.14	0.00	3.20	0.00	140.19	140.19	86.42	86.42
Piede	3 (+)	-159.15	-9.08	0.52	3.18	-1.08	140.08	140.08	86.35	86.35
Piede	3 (-)	-159.15	-9.08	0.00	3.18	0.00	140.08	140.08	86.35	86.35
Piede	1 (-)	-147.96	-8.28	0.00	2.96	0.00	138.14	138.14	85.17	85.17
Piede	1 (+)	-147.96	-8.28	0.45	2.96	-1.00	138.14	138.14	85.17	85.17
Piede	(4+5)-VIII-2 (+)	-137.92	70.31	-6.80	1.77	-0.25	136.40	136.40	84.12	84.12
Piede	(4+5)-VIII-2 (-)	-137.92	70.31	0.00	1.77	0.00	136.40	136.40	84.12	84.12
Piede	(4+5)-II-2 (+)	-137.15	65.15	-6.31	3.01	-0.32	136.27	136.27	84.03	84.03
Piede	(4+5)-II-2 (-)	-137.15	65.15	0.00	3.01	0.00	136.27	136.27	84.03	84.03
Piede	(4+5)-XI-2 (-)	-132.05	46.08	0.00	11.38	0.00	135.38	135.38	83.50	83.50
Piede	(4+5)-XI-2 (+)	-132.05	46.08	-4.51	11.38	-0.79	135.38	135.38	83.50	83.50
Piede	(4+5)-VII-2 (+)	-131.66	22.50	-2.34	27.59	-1.70	135.31	135.31	83.46	83.46
Piede	(4+5)-VII-2 (-)	-131.66	22.50	0.00	27.59	0.00	135.31	135.31	83.46	83.46
Piede	(4+5)-V-2 (+)	-131.27	40.91	-4.02	12.62	-0.87	135.24	135.24	83.41	83.41
Piede	(4+5)-V-2 (-)	-131.27	40.91	0.00	12.62	0.00	135.24	135.24	83.41	83.41
Piede	(4+5)-II-4 (+)	-130.10	71.75	-6.94	-17.08	0.80	135.04	135.04	83.29	83.29
Piede	(4+5)-II-4 (-)	-130.10	71.75	0.00	-17.08	0.00	135.04	135.04	83.29	83.29
Piede	(4+5)-X-2 (+)	-129.90	15.23	-1.65	30.48	-1.86	135.01	135.01	83.27	83.27
Piede	(4+5)-X-2 (-)	-129.90	15.23	0.00	30.48	0.00	135.01	135.01	83.27	83.27
Piede	(4+5)-VIII-4 (+)	-129.33	66.58	-6.45	-15.83	0.73	134.90	134.90	83.21	83.21
Piede	(4+5)-VIII-4 (-)	-129.33	66.58	0.00	-15.83	0.00	134.90	134.90	83.21	83.21

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 70 di 103

Zona	C.	N	MyCal	ΔMy	MzCal	ΔMz	Mry+	Mry-	Mrz+	Mrz-
Piede	(4+5)-I-2 (-)	-129.08	5.28	0.00	31.75	0.00	134.86	134.86	83.18	83.18
Piede	(4+5)-I-2 (+)	-129.08	5.28	-0.70	31.75	-1.93	134.86	134.86	83.18	83.18
Piede	(4+5)-IV-2 (+)	-127.32	-2.00	-0.02	34.64	-2.09	134.55	134.55	83.00	83.00
Piede	(4+5)-IV-2 (-)	-127.32	-2.00	0.00	34.64	0.00	134.55	134.55	83.00	83.00
Piede	(4+5)-V-4 (-)	-124.23	47.51	0.00	-7.47	0.00	134.01	134.01	82.67	82.67
Piede	(4+5)-V-4 (+)	-124.23	47.51	-4.65	-7.47	0.26	134.01	134.01	82.67	82.67
Piede	(4+5)-XI-4 (+)	-123.46	42.34	-4.16	-6.22	0.19	133.88	133.88	82.59	82.59
Piede	(4+5)-XI-4 (-)	-123.46	42.34	0.00	-6.22	0.00	133.88	133.88	82.59	82.59
Piede	(4+5)-IX-2 (-)	-121.64	18.14	0.00	7.07	0.00	133.56	133.56	82.39	82.39
Piede	(4+5)-IX-2 (+)	-121.64	18.14	-1.93	7.07	-0.55	133.56	133.56	82.39	82.39
Piede	(4+5)-III-2 (+)	-120.87	12.97	-1.44	8.31	-0.62	133.43	133.43	82.31	82.31
Piede	(4+5)-III-2 (-)	-120.87	12.97	0.00	8.31	0.00	133.43	133.43	82.31	82.31
Piede	(4+5)-XII-2 (-)	-119.88	10.87	0.00	9.95	0.00	133.25	133.25	82.21	82.21
Piede	(4+5)-XII-2 (+)	-119.88	10.87	-1.24	9.95	-0.71	133.25	133.25	82.21	82.21
Piede	(4+5)-X-1 (-)	-119.47	-14.96	0.00	29.25	0.00	133.18	133.18	82.16	82.16
Piede	(4+5)-X-1 (+)	-119.47	-14.96	1.15	29.25	-1.79	133.18	133.18	82.16	82.16
Piede	(4+5)-VI-2 (-)	-119.11	5.70	0.00	11.20	0.00	133.12	133.12	82.12	82.12
Piede	(4+5)-VI-2 (+)	-119.11	5.70	-0.75	11.20	-0.78	133.12	133.12	82.12	82.12
Piede	(4+5)-VII-1 (-)	-117.71	-22.23	0.00	32.14	0.00	132.87	132.87	81.97	81.97
Piede	(4+5)-VII-1 (+)	-117.71	-22.23	1.83	32.14	-1.95	132.87	132.87	81.97	81.97
Piede	(4+5)-IV-1 (-)	-116.89	-32.18	0.00	33.41	0.00	132.73	132.73	81.89	81.89
Piede	(4+5)-IV-1 (+)	-116.89	-32.18	2.78	33.41	-2.03	132.73	132.73	81.89	81.89
Piede	(4+5)-I-1 (-)	-115.13	-39.45	0.00	36.29	0.00	132.42	132.42	81.70	81.70
Piede	(4+5)-I-1 (+)	-115.13	-39.45	3.47	36.29	-2.19	132.42	132.42	81.70	81.70
Piede	(4+5)-III-4 (+)	-113.82	19.57	-2.07	-11.78	0.50	132.19	132.19	81.56	81.56
Piede	(4+5)-III-4 (-)	-113.82	19.57	0.00	-11.78	0.00	132.19	132.19	81.56	81.56
Piede	(4+5)-IX-4 (-)	-113.05	14.40	0.00	-10.53	0.00	132.06	132.06	81.48	81.48
Piede	(4+5)-IX-4 (+)	-113.05	14.40	-1.58	-10.53	0.43	132.06	132.06	81.48	81.48
Piede	(4+5)-VI-4 (+)	-112.06	12.30	-1.39	-8.89	0.34	131.88	131.88	81.37	81.37
Piede	(4+5)-VI-4 (-)	-112.06	12.30	0.00	-8.89	0.00	131.88	131.88	81.37	81.37
Piede	(4+5)-XII-4 (-)	-111.29	7.13	0.00	-7.65	0.00	131.75	131.75	81.29	81.29
Piede	(4+5)-XII-4 (+)	-111.29	7.13	-0.90	-7.65	0.27	131.75	131.75	81.29	81.29
Piede	(4+5)-XII-1 (-)	-109.45	-19.31	0.00	8.73	0.00	131.42	131.42	81.09	81.09
Piede	(4+5)-XII-1 (+)	-109.45	-19.31	1.55	8.73	-0.65	131.42	131.42	81.09	81.09
Piede	(4+5)-VI-1 (+)	-108.67	-24.48	2.04	9.97	-0.72	131.29	131.29	81.01	81.01
Piede	(4+5)-VI-1 (-)	-108.67	-24.48	0.00	9.97	0.00	131.29	131.29	81.01	81.01
Piede	(4+5)-IX-1 (+)	-107.69	-26.58	2.24	11.61	-0.81	131.11	131.11	80.91	80.91
Piede	(4+5)-IX-1 (-)	-107.69	-26.58	0.00	11.61	0.00	131.11	131.11	80.91	80.91
Piede	(4+5)-III-1 (-)	-106.91	-31.75	0.00	12.86	0.00	130.98	130.98	80.82	80.82
Piede	(4+5)-III-1 (+)	-106.91	-31.75	2.73	12.86	-0.88	130.98	130.98	80.82	80.82
Piede	(4+5)-I-4 (+)	-105.61	27.27	-2.81	-35.22	1.81	130.75	130.75	80.68	80.68
Piede	(4+5)-I-4 (-)	-105.61	27.27	0.00	-35.22	0.00	130.75	130.75	80.68	80.68
Piede	(4+5)-IV-4 (-)	-103.84	19.99	0.00	-32.33	0.00	130.44	130.44	80.50	80.50
Piede	(4+5)-IV-4 (+)	-103.84	19.99	-2.12	-32.33	1.65	130.44	130.44	80.50	80.50
Piede	(4+5)-VII-4 (-)	-103.03	10.04	0.00	-31.06	0.00	130.29	130.29	80.41	80.41
Piede	(4+5)-VII-4 (+)	-103.03	10.04	-1.18	-31.06	1.58	130.29	130.29	80.41	80.41
Piede	(4+5)-VI-3 (+)	-101.63	-17.88	1.41	-10.12	0.41	130.05	130.05	80.26	80.26
Piede	(4+5)-VI-3 (-)	-101.63	-17.88	0.00	-10.12	0.00	130.05	130.05	80.26	80.26
Piede	(4+5)-X-4 (-)	-101.26	2.77	0.00	-28.17	0.00	129.98	129.98	80.22	80.22
Piede	(4+5)-X-4 (+)	-101.26	2.77	-0.49	-28.17	1.41	129.98	129.98	80.22	80.22
Piede	(4+5)-XII-3 (+)	-100.86	-23.05	1.90	-8.87	0.34	129.91	129.91	80.18	80.18
Piede	(4+5)-XII-3 (-)	-100.86	-23.05	0.00	-8.87	0.00	129.91	129.91	80.18	80.18
Piede	(4+5)-III-3 (-)	-99.87	-25.15	0.00	-7.23	0.00	129.74	129.74	80.07	80.07
Piede	(4+5)-III-3 (+)	-99.87	-25.15	2.10	-7.23	0.24	129.74	129.74	80.07	80.07
Piede	(4+5)-IX-3 (+)	-99.10	-30.32	2.59	-5.99	0.17	129.60	129.60	79.99	79.99
Piede	(4+5)-IX-3 (-)	-99.10	-30.32	0.00	-5.99	0.00	129.60	129.60	79.99	79.99
Piede	(4+5)-XI-1 (-)	-97.28	-54.52	0.00	7.30	0.00	129.28	129.28	79.79	79.79
Piede	(4+5)-XI-1 (+)	-97.28	-54.52	4.82	7.30	-0.57	129.28	129.28	79.79	79.79
Piede	(4+5)-V-1 (-)	-96.51	-59.69	0.00	8.55	0.00	129.14	129.14	79.71	79.71
Piede	(4+5)-V-1 (+)	-96.51	-59.69	5.31	8.55	-0.64	129.14	129.14	79.71	79.71
Piede	(4+5)-IV-3 (-)	-93.41	-10.19	0.00	-33.56	0.00	128.60	128.60	79.38	79.38
Piede	(4+5)-IV-3 (+)	-93.41	-10.19	0.67	-33.56	1.72	128.60	128.60	79.38	79.38
Piede	(4+5)-I-3 (-)	-91.65	-17.46	0.00	-30.67	0.00	128.28	128.28	79.19	79.19
Piede	(4+5)-I-3 (+)	-91.65	-17.46	1.36	-30.67	1.55	128.28	128.28	79.19	79.19
Piede	(4+5)-VII-1 (-)	-91.41	-78.76	0.00	16.91	0.00	128.24	128.24	79.16	79.16
Piede	(4+5)-VII-1 (+)	-91.41	-78.76	7.11	16.91	-1.11	128.24	128.24	79.16	79.16
Piede	(4+5)-X-3 (-)	-90.83	-27.41	0.00	-29.40	0.00	128.14	128.14	79.10	79.10
Piede	(4+5)-X-3 (+)	-90.83	-27.41	2.31	-29.40	1.48	128.14	128.14	79.10	79.10
Piede	(4+5)-II-1 (+)	-90.63	-83.93	7.60	18.16	-1.18	128.10	128.10	79.08	79.08
Piede	(4+5)-II-1 (-)	-90.63	-83.93	0.00	18.16	0.00	128.10	128.10	79.08	79.08
Piede	(4+5)-V-3 (+)	-89.46	-53.09	4.67	-11.54	0.49	127.90	127.90	78.95	78.95
Piede	(4+5)-V-3 (-)	-89.46	-53.09	0.00	-11.54	0.00	127.90	127.90	78.95	78.95
Piede	(4+5)-VII-3 (-)	-89.07	-34.68	0.00	-26.51	0.00	127.83	127.83	78.91	78.91
Piede	(4+5)-VII-3 (+)	-89.07	-34.68	3.00	-26.51	1.32	127.83	127.83	78.91	78.91
Piede	(4+5)-XI-3 (-)	-88.69	-58.26	0.00	-10.30	0.00	127.76	127.76	78.87	78.87
Piede	(4+5)-XI-3 (+)	-88.69	-58.26	5.16	-10.30	0.42	127.76	127.76	78.87	78.87

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 71 di 103

Zona	C.	N	MyCal	ΔMy	MzCal	ΔMz	Mry+	Mry-	Mrz+	Mrz-
Piede	(4+5)-II-3 (-)	-83.59	-77.33	0.00	-1.94	0.00	126.85	126.85	78.32	78.32
Piede	(4+5)-II-3 (+)	-83.59	-77.33	6.97	-1.94	-0.05	126.85	126.85	78.32	78.32
Piede	(4+5)-VIII-3 (-)	-82.82	-82.50	0.00	-0.69	0.00	126.72	126.72	78.24	78.24
Piede	(4+5)-VIII-3 (+)	-82.82	-82.50	7.46	-0.69	-0.13	126.72	126.72	78.24	78.24
Testa	2 (+)	-140.29	3.51	0.00	-9.85	0.00	136.81	136.81	84.37	84.37
Testa	2 (-)	-140.29	3.51	-2.17	-9.85	0.32	136.81	136.81	84.37	84.37
Testa	3 (+)	-139.65	3.49	0.00	-9.44	0.00	136.70	136.70	84.30	84.30
Testa	3 (-)	-139.65	3.49	-2.16	-9.44	0.30	136.70	136.70	84.30	84.30
Testa	1 (-)	-128.46	3.21	-1.99	-8.36	0.26	134.75	134.75	83.12	83.12
Testa	1 (+)	-128.46	3.21	0.00	-8.36	0.00	134.75	134.75	83.12	83.12
Testa	(4+5)-VIII-2 (+)	-122.92	-62.87	0.00	-7.09	0.00	133.79	133.79	82.53	82.53
Testa	(4+5)-VIII-2 (-)	-122.92	-62.87	6.80	-7.09	0.25	133.79	133.79	82.53	82.53
Testa	(4+5)-II-2 (+)	-122.15	-58.43	0.00	-8.30	0.00	133.65	133.65	82.45	82.45
Testa	(4+5)-II-2 (-)	-122.15	-58.43	6.31	-8.30	0.32	133.65	133.65	82.45	82.45
Testa	(4+5)-XI-2 (-)	-117.05	-42.17	4.51	-16.44	0.79	132.76	132.76	81.90	81.90
Testa	(4+5)-XI-2 (+)	-117.05	-42.17	0.00	-16.44	0.00	132.76	132.76	81.90	81.90
Testa	(4+5)-VII-2 (+)	-116.66	-23.32	0.00	-31.81	0.00	132.69	132.69	81.86	81.86
Testa	(4+5)-VII-2 (-)	-116.66	-23.32	2.34	-31.81	1.70	132.69	132.69	81.86	81.86
Testa	(4+5)-V-2 (+)	-116.27	-37.73	0.00	-17.66	0.00	132.62	132.62	81.82	81.82
Testa	(4+5)-V-2 (-)	-116.27	-37.73	4.02	-17.66	0.87	132.62	132.62	81.82	81.82
Testa	(4+5)-II-4 (+)	-115.10	-64.21	0.00	10.90	0.00	132.42	132.42	81.70	81.70
Testa	(4+5)-II-4 (-)	-115.10	-64.21	6.94	10.90	-0.80	132.42	132.42	81.70	81.70
Testa	(4+5)-X-2 (+)	-114.90	-17.11	0.00	-34.61	0.00	132.38	132.38	81.68	81.68
Testa	(4+5)-X-2 (-)	-114.90	-17.11	1.65	-34.61	1.86	132.38	132.38	81.68	81.68
Testa	(4+5)-VIII-4 (+)	-114.33	-59.77	0.00	9.68	0.00	132.28	132.28	81.61	81.61
Testa	(4+5)-VIII-4 (-)	-114.33	-59.77	6.45	9.68	-0.73	132.28	132.28	81.61	81.61
Testa	(4+5)-I-2 (-)	-114.08	-8.51	0.70	-35.87	1.93	132.24	132.24	81.59	81.59
Testa	(4+5)-I-2 (+)	-114.08	-8.51	0.00	-35.87	0.00	132.24	132.24	81.59	81.59
Testa	(4+5)-IV-2 (+)	-112.32	-2.31	0.00	-38.68	0.00	131.93	131.93	81.40	81.40
Testa	(4+5)-IV-2 (-)	-112.32	-2.31	0.02	-38.68	2.09	131.93	131.93	81.40	81.40
Testa	(4+5)-V-4 (-)	-109.23	-43.52	4.65	1.55	-0.26	131.39	131.39	81.07	81.07
Testa	(4+5)-V-4 (+)	-109.23	-43.52	0.00	1.55	0.00	131.39	131.39	81.07	81.07
Testa	(4+5)-XI-4 (+)	-108.46	-39.07	0.00	0.33	0.00	131.25	131.25	80.99	80.99
Testa	(4+5)-XI-4 (-)	-108.46	-39.07	4.16	0.33	-0.19	131.25	131.25	80.99	80.99
Testa	(4+5)-IX-2 (-)	-106.64	-19.71	1.93	-12.25	0.55	130.93	130.93	80.79	80.79
Testa	(4+5)-IX-2 (+)	-106.64	-19.71	0.00	-12.25	0.00	130.93	130.93	80.79	80.79
Testa	(4+5)-III-2 (+)	-105.87	-15.27	0.00	-13.47	0.00	130.79	130.79	80.71	80.71
Testa	(4+5)-III-2 (-)	-105.87	-15.27	1.44	-13.47	0.62	130.79	130.79	80.71	80.71
Testa	(4+5)-XII-2 (-)	-104.88	-13.50	1.24	-15.05	0.71	130.62	130.62	80.61	80.61
Testa	(4+5)-XII-2 (+)	-104.88	-13.50	0.00	-15.05	0.00	130.62	130.62	80.61	80.61
Testa	(4+5)-X-1 (-)	-104.47	7.46	-1.15	-33.43	1.79	130.55	130.55	80.56	80.56
Testa	(4+5)-X-1 (+)	-104.47	7.46	0.00	-33.43	0.00	130.55	130.55	80.56	80.56
Testa	(4+5)-VI-2 (-)	-104.11	-9.06	0.75	-16.27	0.78	130.48	130.48	80.52	80.52
Testa	(4+5)-VI-2 (+)	-104.11	-9.06	0.00	-16.27	0.00	130.48	130.48	80.52	80.52
Testa	(4+5)-VII-1 (-)	-102.71	13.67	-1.83	-36.23	1.95	130.24	130.24	80.37	80.37
Testa	(4+5)-VII-1 (+)	-102.71	13.67	0.00	-36.23	0.00	130.24	130.24	80.37	80.37
Testa	(4+5)-IV-1 (-)	-101.89	22.27	-2.78	-37.49	2.03	130.09	130.09	80.29	80.29
Testa	(4+5)-IV-1 (+)	-101.89	22.27	0.00	-37.49	0.00	130.09	130.09	80.29	80.29
Testa	(4+5)-I-1 (-)	-100.13	28.48	-3.47	-40.30	2.19	129.78	129.78	80.10	80.10
Testa	(4+5)-I-1 (+)	-100.13	28.48	0.00	-40.30	0.00	129.78	129.78	80.10	80.10
Testa	(4+5)-III-4 (+)	-98.82	-21.05	0.00	5.74	0.00	129.55	129.55	79.96	79.96
Testa	(4+5)-III-4 (-)	-98.82	-21.05	2.07	5.74	-0.50	129.55	129.55	79.96	79.96
Testa	(4+5)-IX-4 (-)	-98.05	-16.61	1.58	4.52	-0.43	129.42	129.42	79.88	79.88
Testa	(4+5)-IX-4 (+)	-98.05	-16.61	0.00	4.52	0.00	129.42	129.42	79.88	79.88
Testa	(4+5)-VI-4 (+)	-97.06	-14.84	0.00	2.93	0.00	129.24	129.24	79.77	79.77
Testa	(4+5)-VI-4 (-)	-97.06	-14.84	1.39	2.93	-0.34	129.24	129.24	79.77	79.77
Testa	(4+5)-XII-4 (-)	-96.29	-10.40	0.90	1.71	-0.27	129.10	129.10	79.69	79.69
Testa	(4+5)-XII-4 (+)	-96.29	-10.40	0.00	1.71	0.00	129.10	129.10	79.69	79.69
Testa	(4+5)-XII-1 (-)	-94.45	11.08	-1.55	-13.87	0.65	128.78	128.78	79.49	79.49
Testa	(4+5)-XII-1 (+)	-94.45	11.08	0.00	-13.87	0.00	128.78	128.78	79.49	79.49
Testa	(4+5)-VI-1 (+)	-93.67	15.52	0.00	-15.09	0.00	128.64	128.64	79.41	79.41
Testa	(4+5)-VI-1 (-)	-93.67	15.52	-2.04	-15.09	0.72	128.64	128.64	79.41	79.41
Testa	(4+5)-IX-1 (+)	-92.69	17.29	0.00	-16.67	0.00	128.47	128.47	79.30	79.30
Testa	(4+5)-IX-1 (-)	-92.69	17.29	-2.24	-16.67	0.81	128.47	128.47	79.30	79.30
Testa	(4+5)-III-1 (-)	-91.91	21.73	-2.73	-17.89	0.88	128.33	128.33	79.22	79.22
Testa	(4+5)-III-1 (+)	-91.91	21.73	0.00	-17.89	0.00	128.33	128.33	79.22	79.22
Testa	(4+5)-I-4 (+)	-90.61	-27.80	0.00	28.14	0.00	128.10	128.10	79.08	79.08
Testa	(4+5)-I-4 (-)	-90.61	-27.80	2.81	28.14	-1.81	128.10	128.10	79.08	79.08
Testa	(4+5)-IV-4 (-)	-88.84	-21.59	2.12	25.33	-1.65	127.79	127.79	78.89	78.89
Testa	(4+5)-IV-4 (+)	-88.84	-21.59	0.00	25.33	0.00	127.79	127.79	78.89	78.89
Testa	(4+5)-VII-4 (-)	-88.03	-13.00	1.18	24.08	-1.58	127.64	127.64	78.80	78.80
Testa	(4+5)-VII-4 (+)	-88.03	-13.00	0.00	24.08	0.00	127.64	127.64	78.80	78.80
Testa	(4+5)-VI-3 (+)	-86.63	9.73	0.00	4.12	0.00	127.39	127.39	78.65	78.65
Testa	(4+5)-VI-3 (-)	-86.63	9.73	-1.41	4.12	-0.41	127.39	127.39	78.65	78.65
Testa	(4+5)-X-4 (-)	-86.26	-6.79	0.49	21.27	-1.41	127.33	127.33	78.61	78.61
Testa	(4+5)-X-4 (+)	-86.26	-6.79	0.00	21.27	0.00	127.33	127.33	78.61	78.61

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 72 di 103

Zona	C.	N	MyCal	ΔMy	MzCal	ΔMz	Mry+	Mry-	Mrz+	Mrz-
Testa	(4+5)-XII-3(+)	-85.86	14.18	0.00	2.90	0.00	127.26	127.26	78.57	78.57
Testa	(4+5)-XII-3(-)	-85.86	14.18	-1.90	2.90	-0.34	127.26	127.26	78.57	78.57
Testa	(4+5)-III-3(-)	-84.87	15.94	-2.10	1.31	-0.24	127.08	127.08	78.46	78.46
Testa	(4+5)-III-3(+)	-84.87	15.94	0.00	1.31	0.00	127.08	127.08	78.46	78.46
Testa	(4+5)-IX-3(+)	-84.10	20.38	0.00	0.09	0.00	126.94	126.94	78.38	78.38
Testa	(4+5)-IX-3(-)	-84.10	20.38	-2.59	0.09	-0.17	126.94	126.94	78.38	78.38
Testa	(4+5)-XI-1(-)	-82.28	39.75	-4.82	-12.48	0.57	126.62	126.62	78.18	78.18
Testa	(4+5)-XI-1(+)	-82.28	39.75	0.00	-12.48	0.00	126.62	126.62	78.18	78.18
Testa	(4+5)-V-1(-)	-81.51	44.19	-5.31	-13.70	0.64	126.48	126.48	78.10	78.10
Testa	(4+5)-V-1(+)	-81.51	44.19	0.00	-13.70	0.00	126.48	126.48	78.10	78.10
Testa	(4+5)-IV-3(-)	-78.41	2.98	-0.67	26.52	-1.72	125.93	125.93	77.76	77.76
Testa	(4+5)-IV-3(+)	-78.41	2.98	0.00	26.52	0.00	125.93	125.93	77.76	77.76
Testa	(4+5)-I-3(-)	-76.65	9.19	-1.36	23.71	-1.55	125.62	125.62	77.57	77.57
Testa	(4+5)-I-3(+)	-76.65	9.19	0.00	23.71	0.00	125.62	125.62	77.57	77.57
Testa	(4+5)-VIII-1(-)	-76.41	60.45	-7.11	-21.84	1.11	125.58	125.58	77.55	77.55
Testa	(4+5)-VIII-1(+)	-76.41	60.45	0.00	-21.84	0.00	125.58	125.58	77.55	77.55
Testa	(4+5)-X-3(-)	-75.83	17.79	-2.31	22.46	-1.48	125.48	125.48	77.48	77.48
Testa	(4+5)-X-3(+)	-75.83	17.79	0.00	22.46	0.00	125.48	125.48	77.48	77.48
Testa	(4+5)-II-1(+)	-75.63	64.89	0.00	-23.06	0.00	125.44	125.44	77.46	77.46
Testa	(4+5)-II-1(-)	-75.63	64.89	-7.60	-23.06	1.18	125.44	125.44	77.46	77.46
Testa	(4+5)-V-3(+)	-74.46	38.41	0.00	5.50	0.00	125.23	125.23	77.34	77.34
Testa	(4+5)-V-3(-)	-74.46	38.41	-4.67	5.50	-0.49	125.23	125.23	77.34	77.34
Testa	(4+5)-VII-3(-)	-74.07	24.00	-3.00	19.65	-1.32	125.16	125.16	77.29	77.29
Testa	(4+5)-VII-3(+)	-74.07	24.00	0.00	19.65	0.00	125.16	125.16	77.29	77.29
Testa	(4+5)-XI-3(-)	-73.69	42.85	-5.16	4.28	-0.42	125.09	125.09	77.25	77.25
Testa	(4+5)-XI-3(+)	-73.69	42.85	0.00	4.28	0.00	125.09	125.09	77.25	77.25
Testa	(4+5)-II-3(-)	-68.59	59.10	-6.97	-3.85	0.05	124.18	124.18	76.70	76.70
Testa	(4+5)-II-3(+)	-68.59	59.10	0.00	-3.85	0.00	124.18	124.18	76.70	76.70
Testa	(4+5)-VIII-3(-)	-67.82	63.54	-7.46	-5.07	0.13	124.05	124.05	76.62	76.62
Testa	(4+5)-VIII-3(+)	-67.82	63.54	0.00	-5.07	0.00	124.05	124.05	76.62	76.62

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrzd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(4+5)-I-1	--	--	19.15	--	432.22	209.09	209.09	9.35	2.500	11
Z	(4+5)-II-1	--	--	37.20	--	460.08	373.73	373.73	9.35	2.500	10

Pilastro: 4 [4,104] Sez. R: By=30.00 cm Bz=50.00 cm L=400.00 cm Ln=400.00 cm Criterio: CLS_Pilastri_ND - Verifica a presso-flessione deviata, $\zeta_E=1.320$ [(4+5)-XI-4] : **Verificato**

Piede	AfSpigolo = 3.14	Afy = 0.00	Afz = 1.54
Testa	AfSpigolo = 3.14	Afy = 0.00	Afz = 1.54

$v_{max}=N/(fcd*A)=0.043 \leq 0.65$ [Comb. (4+5)-V-3(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	2(+)	-158.93	9.08	-2.10	140.04	86.33	140.04	86.33	18
Piede	2(-)	-158.93	9.64	-3.18	140.04	86.33	140.04	86.33	17
Piede	3(+)	-158.29	9.03	-2.09	139.93	86.26	139.93	86.26	18
Piede	3(-)	-158.29	9.57	-3.17	139.93	86.26	139.93	86.26	17
Piede	1(-)	-147.16	8.73	2.95	138.01	85.09	138.01	85.09	18
Piede	1(+)	-147.16	8.25	2.93	138.01	85.09	138.01	85.09	19
Piede	(4+5)-V-3(-)	-137.40	-71.49	-0.38	136.31	84.06	136.31	84.06	2.3
Piede	(4+5)-V-3(+)	-137.40	-64.60	-0.20	136.31	84.06	136.31	84.06	2.7
Piede	(4+5)-XI-3(+)	-136.64	-59.79	-1.43	136.18	83.98	136.18	83.98	3.0
Piede	(4+5)-XI-3(-)	-136.64	-66.18	-1.68	136.18	83.98	136.18	83.98	2.6
Piede	(4+5)-II-3(-)	-131.26	-46.89	-6.28	135.24	83.41	135.24	83.41	3.9
Piede	(4+5)-II-3(+)	-131.26	-42.31	-5.77	135.24	83.41	135.24	83.41	4.6
Piede	(4+5)-IV-3(-)	-131.04	-23.38	-26.07	135.20	83.39	135.20	83.39	3.5
Piede	(4+5)-IV-3(+)	-131.04	-20.95	-24.46	135.20	83.39	135.20	83.39	3.9
Piede	(4+5)-VIII-3(+)	-130.50	-37.51	-7.00	135.11	83.33	135.11	83.33	5.2
Piede	(4+5)-VIII-3(-)	-130.50	-41.58	-7.59	135.11	83.33	135.11	83.33	4.4
Piede	(4+5)-XI-1(+)	-129.60	-65.55	17.28	134.95	83.24	134.95	83.24	2.0
Piede	(4+5)-XI-1(-)	-129.60	-72.55	18.14	134.95	83.24	134.95	83.24	1.8
Piede	(4+5)-I-3(+)	-129.19	-14.27	-26.13	134.88	83.19	134.88	83.19	4.1
Piede	(4+5)-I-3(-)	-129.19	-16.00	-27.84	134.88	83.19	134.88	83.19	3.6
Piede	(4+5)-V-1(-)	-128.84	-67.24	16.83	134.82	83.16	134.82	83.16	2.0
Piede	(4+5)-V-1(+)	-128.84	-60.75	16.05	134.82	83.16	134.82	83.16	2.2
Piede	(4+5)-X-3(+)	-128.51	-4.93	-28.56	134.76	83.12	134.76	83.12	4.2
Piede	(4+5)-X-3(-)	-128.51	-5.68	-30.43	134.76	83.12	134.76	83.12	3.7
Piede	(4+5)-VII-3(+)	-126.66	1.76	-30.23	134.44	82.93	134.44	82.93	4.0
Piede	(4+5)-VII-3(-)	-126.66	1.70	-32.20	134.44	82.93	134.44	82.93	3.6
Piede	(4+5)-VIII-1(+)	-123.46	-43.27	11.71	133.88	82.59	133.88	82.59	3.6

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 73 di 103

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
Piede	(4+5)-VIII-1 (-)	-123.46	-47.95	12.23	133.88	82.59	133.88	82.59	3.1
Piede	(4+5)-II-1 (-)	-122.70	-42.64	10.93	133.75	82.51	133.75	82.51	3.7
Piede	(4+5)-II-1 (+)	-122.70	-38.46	10.48	133.75	82.51	133.75	82.51	4.3
Piede	(4+5)-VI-3 (-)	-121.05	-18.43	-6.00	133.46	82.33	133.46	82.33	12
Piede	(4+5)-VI-3 (+)	-121.05	-16.46	-5.50	133.46	82.33	133.46	82.33	13
Piede	(4+5)-XII-3 (-)	-120.29	-13.12	-7.30	133.33	82.25	133.33	82.25	14
Piede	(4+5)-XII-3 (+)	-120.29	-11.66	-6.73	133.33	82.25	133.33	82.25	15
Piede	(4+5)-III-3 (+)	-119.21	-9.78	-7.17	133.14	82.13	133.14	82.13	15
Piede	(4+5)-III-3 (-)	-119.21	-11.05	-7.77	133.14	82.13	133.14	82.13	14
Piede	(4+5)-I-4 (+)	-118.86	13.62	-27.33	133.08	82.10	133.08	82.10	3.7
Piede	(4+5)-I-4 (-)	-118.86	14.72	-29.12	133.08	82.10	133.08	82.10	3.3
Piede	(4+5)-IX-3 (+)	-118.45	-4.97	-8.41	133.00	82.05	133.00	82.05	16
Piede	(4+5)-IX-3 (-)	-118.45	-5.74	-9.08	133.00	82.05	133.00	82.05	15
Piede	(4+5)-IV-4 (-)	-117.02	22.10	-30.89	132.75	81.90	132.75	81.90	2.8
Piede	(4+5)-IV-4 (+)	-117.02	20.31	-29.00	132.75	81.90	132.75	81.90	3.1
Piede	(4+5)-VII-4 (-)	-116.33	32.42	-33.47	132.63	81.83	132.63	81.83	2.2
Piede	(4+5)-VII-4 (+)	-116.33	29.64	-31.44	132.63	81.83	132.63	81.83	2.5
Piede	(4+5)-X-4 (-)	-114.49	39.80	-35.24	132.31	81.63	132.31	81.63	1.9
Piede	(4+5)-X-4 (+)	-114.49	36.33	-33.11	132.31	81.63	132.31	81.63	2.1
Piede	(4+5)-XII-1 (+)	-113.25	-17.42	11.98	132.09	81.50	132.09	81.50	8.5
Piede	(4+5)-XII-1 (-)	-113.25	-19.49	12.51	132.09	81.50	132.09	81.50	7.6
Piede	(4+5)-VI-1 (+)	-112.49	-12.62	10.74	131.96	81.42	131.96	81.42	11
Piede	(4+5)-VI-1 (-)	-112.49	-14.18	11.21	131.96	81.42	131.96	81.42	10
Piede	(4+5)-IX-1 (+)	-111.41	-10.74	10.31	131.77	81.30	131.77	81.30	12
Piede	(4+5)-IX-1 (-)	-111.41	-12.11	10.74	131.77	81.30	131.77	81.30	11
Piede	(4+5)-III-1 (+)	-110.65	-5.93	9.07	131.63	81.22	131.63	81.22	16
Piede	(4+5)-III-1 (-)	-110.65	-6.80	9.44	131.63	81.22	131.63	81.22	15
Piede	(4+5)-III-4 (+)	-108.88	18.11	-8.38	131.32	81.03	131.32	81.03	10
Piede	(4+5)-III-4 (-)	-108.88	19.67	-9.05	131.32	81.03	131.32	81.03	9.2
Piede	(4+5)-IX-4 (+)	-108.12	22.92	-9.61	131.19	80.95	131.19	80.95	7.7
Piede	(4+5)-IX-4 (-)	-108.12	24.98	-10.35	131.19	80.95	131.19	80.95	6.7
Piede	(4+5)-VI-4 (+)	-107.04	24.79	-10.05	131.00	80.84	131.00	80.84	6.8
Piede	(4+5)-VI-4 (-)	-107.04	27.05	-10.82	131.00	80.84	131.00	80.84	6.0
Piede	(4+5)-XII-4 (-)	-106.28	32.36	-12.12	130.87	80.76	130.87	80.76	4.6
Piede	(4+5)-XII-4 (+)	-106.28	29.60	-11.28	130.87	80.76	130.87	80.76	5.3
Piede	(4+5)-X-1 (-)	-105.04	-26.92	35.64	130.65	80.62	130.65	80.62	2.1
Piede	(4+5)-X-1 (+)	-105.04	-24.15	33.81	130.65	80.62	130.65	80.62	2.3
Piede	(4+5)-VII-1 (+)	-103.20	-17.46	32.13	130.32	80.43	130.32	80.43	2.7
Piede	(4+5)-VII-1 (-)	-103.20	-19.54	33.87	130.32	80.43	130.32	80.43	2.5
Piede	(4+5)-IV-1 (-)	-102.51	-9.23	31.28	130.20	80.35	130.20	80.35	3.1
Piede	(4+5)-IV-1 (+)	-102.51	-8.13	29.70	130.20	80.35	130.20	80.35	3.3
Piede	(4+5)-IX-2 (-)	-101.08	18.61	9.47	129.95	80.20	129.95	80.20	9.1
Piede	(4+5)-IX-2 (+)	-101.08	17.15	9.10	129.95	80.20	129.95	80.20	9.9
Piede	(4+5)-I-1 (+)	-100.67	-1.44	28.03	129.88	80.16	129.88	80.16	3.9
Piede	(4+5)-I-1 (-)	-100.67	-1.85	29.51	129.88	80.16	129.88	80.16	3.6
Piede	(4+5)-III-2 (+)	-100.32	21.96	7.87	129.82	80.12	129.82	80.12	8.6
Piede	(4+5)-III-2 (-)	-100.32	23.92	8.16	129.82	80.12	129.82	80.12	7.6
Piede	(4+5)-XII-2 (-)	-99.24	25.99	7.70	129.62	80.00	129.62	80.00	7.0
Piede	(4+5)-XII-2 (+)	-99.24	23.84	7.43	129.62	80.00	129.62	80.00	7.9
Piede	(4+5)-VI-2 (+)	-98.48	28.64	6.20	129.49	79.92	129.49	79.92	6.5
Piede	(4+5)-VI-2 (-)	-98.48	31.30	6.39	129.49	79.92	129.49	79.92	5.7
Piede	(4+5)-II-4 (+)	-96.83	50.64	-9.78	129.20	79.74	129.20	79.74	2.8
Piede	(4+5)-II-4 (-)	-96.83	55.51	-10.53	129.20	79.74	129.20	79.74	2.5
Piede	(4+5)-VIII-4 (-)	-96.07	60.82	-11.84	129.07	79.66	129.07	79.66	2.2
Piede	(4+5)-VIII-4 (+)	-96.07	55.45	-11.01	129.07	79.66	129.07	79.66	2.4
Piede	(4+5)-VII-2 (+)	-92.87	10.42	30.93	128.50	79.32	128.50	79.32	2.9
Piede	(4+5)-VII-2 (-)	-92.87	11.18	32.59	128.50	79.32	128.50	79.32	2.7
Piede	(4+5)-X-2 (+)	-91.02	17.11	29.26	128.17	79.12	128.17	79.12	2.8
Piede	(4+5)-X-2 (-)	-91.02	18.56	30.82	128.17	79.12	128.17	79.12	2.6
Piede	(4+5)-V-4 (-)	-90.69	80.12	-16.44	128.11	79.09	128.11	79.09	1.5
Piede	(4+5)-V-4 (+)	-90.69	72.93	-15.36	128.11	79.09	128.11	79.09	1.7
Piede	(4+5)-I-2 (+)	-90.34	26.45	26.82	128.05	79.05	128.05	79.05	2.7
Piede	(4+5)-I-2 (-)	-90.34	28.87	28.24	128.05	79.05	128.05	79.05	2.5
Piede	(4+5)-XI-4 (+)	-89.93	77.73	-16.59	127.98	79.00	127.98	79.00	1.5
Piede	(4+5)-XI-4 (-)	-89.93	85.42	-17.74	127.98	79.00	127.98	79.00	1.4
Piede	(4+5)-VIII-2 (+)	-89.03	49.69	7.70	127.82	78.91	127.82	78.91	2.9
Piede	(4+5)-VIII-2 (-)	-89.03	54.45	7.98	127.82	78.91	127.82	78.91	2.6
Piede	(4+5)-IV-2 (+)	-88.49	33.13	25.15	127.72	78.85	127.72	78.85	2.6
Piede	(4+5)-IV-2 (-)	-88.49	36.25	26.47	127.72	78.85	127.72	78.85	2.4
Piede	(4+5)-II-2 (-)	-88.27	59.76	6.67	127.68	78.83	127.68	78.83	2.3
Piede	(4+5)-II-2 (+)	-88.27	54.49	6.46	127.68	78.83	127.68	78.83	2.6
Piede	(4+5)-XI-2 (+)	-82.89	71.97	2.12	126.73	78.25	126.73	78.25	1.9
Piede	(4+5)-XI-2 (-)	-82.89	79.05	2.07	126.73	78.25	126.73	78.25	1.7
Piede	(4+5)-V-2 (+)	-82.13	76.77	0.89	126.60	78.16	126.60	78.16	1.8
Piede	(4+5)-V-2 (-)	-82.13	84.36	0.77	126.60	78.16	126.60	78.16	1.6
Testa	2 (+)	-139.43	-3.49	9.03	136.66	84.28	136.66	84.28	15

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 74 di 103

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
Testa	2 (-)	-139.43	-1.32	8.76	136.66	84.28	136.66	84.28	16
Testa	3 (+)	-138.79	-3.47	8.62	136.55	84.21	136.55	84.21	16
Testa	3 (-)	-138.79	-1.32	8.37	136.55	84.21	136.55	84.21	17
Testa	1 (-)	-127.66	-1.21	7.38	134.61	83.03	134.61	83.03	18
Testa	1 (+)	-127.66	-3.19	7.59	134.61	83.03	134.61	83.03	18
Testa	(4+5)-V-3 (-)	-122.40	56.58	5.77	133.69	82.47	133.69	82.47	2.9
Testa	(4+5)-V-3 (+)	-122.40	63.47	5.95	133.69	82.47	133.69	82.47	2.5
Testa	(4+5)-XI-3 (+)	-121.64	58.96	7.22	133.56	82.39	133.56	82.39	2.6
Testa	(4+5)-XI-3 (-)	-121.64	52.57	6.97	133.56	82.39	133.56	82.39	3.1
Testa	(4+5)-II-3 (-)	-116.26	38.10	11.14	132.62	81.82	132.62	81.82	4.1
Testa	(4+5)-II-3 (+)	-116.26	42.68	11.65	132.62	81.82	132.62	81.82	3.5
Testa	(4+5)-IV-3 (-)	-116.04	21.73	28.92	132.58	81.80	132.58	81.80	3.0
Testa	(4+5)-IV-3 (+)	-116.04	24.16	30.54	132.58	81.80	132.58	81.80	2.7
Testa	(4+5)-VIII-3 (+)	-115.50	38.16	12.92	132.49	81.74	132.49	81.74	3.9
Testa	(4+5)-VIII-3 (-)	-115.50	34.09	12.34	132.49	81.74	132.49	81.74	4.5
Testa	(4+5)-XI-1 (+)	-114.60	64.45	-11.74	132.33	81.64	132.33	81.64	2.1
Testa	(4+5)-XI-1 (-)	-114.60	57.46	-10.89	132.33	81.64	132.33	81.64	2.5
Testa	(4+5)-I-3 (+)	-114.19	17.92	32.25	132.26	81.60	132.26	81.60	2.8
Testa	(4+5)-I-3 (-)	-114.19	16.19	30.53	132.26	81.60	132.26	81.60	3.0
Testa	(4+5)-V-1 (-)	-113.84	53.44	-9.69	132.20	81.56	132.20	81.56	2.8
Testa	(4+5)-V-1 (+)	-113.84	59.94	-10.47	132.20	81.56	132.20	81.56	2.4
Testa	(4+5)-X-3 (+)	-113.51	9.11	34.78	132.14	81.53	132.14	81.53	2.8
Testa	(4+5)-X-3 (-)	-113.51	8.35	32.91	132.14	81.53	132.14	81.53	3.0
Testa	(4+5)-VII-3 (+)	-111.66	2.87	36.49	131.81	81.33	131.81	81.33	2.8
Testa	(4+5)-VII-3 (-)	-111.66	2.81	34.52	131.81	81.33	131.81	81.33	3.0
Testa	(4+5)-VIII-1 (+)	-108.46	43.66	-6.04	131.25	80.99	131.25	80.99	3.9
Testa	(4+5)-VIII-1 (-)	-108.46	38.98	-5.52	131.25	80.99	131.25	80.99	4.6
Testa	(4+5)-II-1 (-)	-107.70	34.97	-4.32	131.12	80.91	131.12	80.91	5.6
Testa	(4+5)-II-1 (+)	-107.70	39.14	-4.77	131.12	80.91	131.12	80.91	4.6
Testa	(4+5)-VI-3 (-)	-106.05	18.07	10.89	130.83	80.73	130.83	80.73	8.6
Testa	(4+5)-VI-3 (+)	-106.05	20.03	11.38	130.83	80.73	130.83	80.73	7.7
Testa	(4+5)-XII-3 (-)	-105.29	14.06	12.08	130.69	80.65	130.69	80.65	9.3
Testa	(4+5)-XII-3 (+)	-105.29	15.52	12.65	130.69	80.65	130.69	80.65	8.4
Testa	(4+5)-III-3 (+)	-104.21	13.80	13.09	130.50	80.53	130.50	80.53	8.6
Testa	(4+5)-III-3 (-)	-104.21	12.53	12.50	130.50	80.53	130.50	80.53	9.4
Testa	(4+5)-I-4 (+)	-103.86	-6.84	33.48	130.44	80.50	130.44	80.50	2.9
Testa	(4+5)-I-4 (-)	-103.86	-5.73	31.69	130.44	80.50	130.44	80.50	3.2
Testa	(4+5)-IX-3 (+)	-103.45	9.28	14.36	130.37	80.45	130.37	80.45	9.1
Testa	(4+5)-IX-3 (-)	-103.45	8.51	13.69	130.37	80.45	130.37	80.45	9.9
Testa	(4+5)-IV-4 (-)	-102.02	-11.28	33.30	130.12	80.30	130.12	80.30	2.7
Testa	(4+5)-IV-4 (+)	-102.02	-13.07	35.19	130.12	80.30	130.12	80.30	2.5
Testa	(4+5)-VII-4 (-)	-101.33	-19.11	35.69	129.99	80.23	129.99	80.23	2.3
Testa	(4+5)-VII-4 (+)	-101.33	-21.89	37.72	129.99	80.23	129.99	80.23	2.1
Testa	(4+5)-X-4 (-)	-99.49	-24.66	37.30	129.67	80.03	129.67	80.03	2.1
Testa	(4+5)-X-4 (+)	-99.49	-28.13	39.43	129.67	80.03	129.67	80.03	1.9
Testa	(4+5)-XII-1 (+)	-98.25	21.02	-6.31	129.45	79.90	129.45	79.90	9.7
Testa	(4+5)-XII-1 (-)	-98.25	18.95	-5.77	129.45	79.90	129.45	79.90	11
Testa	(4+5)-VI-1 (+)	-97.49	16.50	-5.04	129.32	79.82	129.32	79.82	14
Testa	(4+5)-VI-1 (-)	-97.49	14.93	-4.57	129.32	79.82	129.32	79.82	15
Testa	(4+5)-IX-1 (+)	-96.41	14.78	-4.60	129.13	79.70	129.13	79.70	15
Testa	(4+5)-IX-1 (-)	-96.41	13.40	-4.16	129.13	79.70	129.13	79.70	17
Testa	(4+5)-III-1 (+)	-95.65	10.26	-3.33	128.99	79.62	128.99	79.62	21
Testa	(4+5)-III-1 (-)	-95.65	9.39	-2.96	128.99	79.62	128.99	79.62	22
Testa	(4+5)-III-4 (+)	-93.88	-10.96	14.33	128.68	79.43	128.68	79.43	8.0
Testa	(4+5)-III-4 (-)	-93.88	-9.39	13.66	128.68	79.43	128.68	79.43	9.0
Testa	(4+5)-IX-4 (+)	-93.12	-15.47	15.60	128.54	79.35	128.54	79.35	6.2
Testa	(4+5)-IX-4 (-)	-93.12	-13.41	14.86	128.54	79.35	128.54	79.35	7.0
Testa	(4+5)-VI-4 (+)	-92.04	-17.20	16.04	128.35	79.23	128.35	79.23	5.7
Testa	(4+5)-VI-4 (-)	-92.04	-14.94	15.27	128.35	79.23	128.35	79.23	6.4
Testa	(4+5)-XII-4 (-)	-91.28	-18.95	16.47	128.22	79.15	128.22	79.15	5.2
Testa	(4+5)-XII-4 (+)	-91.28	-21.71	17.31	128.22	79.15	128.22	79.15	4.6
Testa	(4+5)-X-1 (-)	-90.04	24.65	-26.60	128.00	79.02	128.00	79.02	2.8
Testa	(4+5)-X-1 (+)	-90.04	27.43	-28.43	128.00	79.02	128.00	79.02	2.5
Testa	(4+5)-VII-1 (+)	-88.20	21.19	-26.72	127.67	78.82	127.67	78.82	2.9
Testa	(4+5)-VII-1 (-)	-88.20	19.11	-24.99	127.67	78.82	127.67	78.82	3.3
Testa	(4+5)-IV-1 (-)	-87.51	11.27	-22.60	127.55	78.74	127.55	78.74	4.2
Testa	(4+5)-IV-1 (+)	-87.51	12.38	-24.19	127.55	78.74	127.55	78.74	3.8
Testa	(4+5)-IX-2 (-)	-86.08	-8.52	-3.00	127.30	78.59	127.30	78.59	24
Testa	(4+5)-IX-2 (+)	-86.08	-9.98	-3.36	127.30	78.59	127.30	78.59	21
Testa	(4+5)-I-1 (+)	-85.67	6.14	-22.48	127.22	78.55	127.22	78.55	4.6
Testa	(4+5)-I-1 (-)	-85.67	5.73	-20.99	127.22	78.55	127.22	78.55	5.1
Testa	(4+5)-III-2 (+)	-85.32	-14.49	-2.09	127.16	78.51	127.16	78.51	18
Testa	(4+5)-III-2 (-)	-85.32	-12.53	-1.80	127.16	78.51	127.16	78.51	21
Testa	(4+5)-XII-2 (-)	-84.24	-14.06	-1.39	126.97	78.39	126.97	78.39	19
Testa	(4+5)-XII-2 (+)	-84.24	-16.22	-1.65	126.97	78.39	126.97	78.39	17
Testa	(4+5)-VI-2 (+)	-83.48	-20.73	-0.38	126.84	78.31	126.84	78.31	13

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 75 di 103

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
Testa	(4+5)-VI-2 (-)	-83.48	-18.07	-0.19	126.84	78.31	126.84	78.31	16
Testa	(4+5)-II-4 (+)	-81.83	-39.84	15.77	126.54	78.13	126.54	78.13	2.9
Testa	(4+5)-II-4 (-)	-81.83	-34.97	15.02	126.54	78.13	126.54	78.13	3.4
Testa	(4+5)-VIII-4 (-)	-81.07	-38.98	16.21	126.41	78.05	126.41	78.05	2.9
Testa	(4+5)-VIII-4 (+)	-81.07	-44.36	17.04	126.41	78.05	126.41	78.05	2.6
Testa	(4+5)-VII-2 (+)	-77.87	-3.57	-25.49	125.84	77.70	125.84	77.70	3.9
Testa	(4+5)-VII-2 (-)	-77.87	-2.81	-23.83	125.84	77.70	125.84	77.70	4.3
Testa	(4+5)-X-2 (+)	-76.02	-9.80	-23.78	125.51	77.51	125.51	77.51	3.8
Testa	(4+5)-X-2 (-)	-76.02	-8.36	-22.22	125.51	77.51	125.51	77.51	4.2
Testa	(4+5)-V-4 (-)	-75.69	-53.45	20.39	125.45	77.47	125.45	77.47	2.0
Testa	(4+5)-V-4 (+)	-75.69	-60.63	21.47	125.45	77.47	125.45	77.47	1.7
Testa	(4+5)-I-2 (+)	-75.34	-18.62	-21.25	125.39	77.43	125.39	77.43	3.7
Testa	(4+5)-I-2 (-)	-75.34	-16.19	-19.83	125.39	77.43	125.39	77.43	4.1
Testa	(4+5)-XI-4 (+)	-74.93	-65.15	22.74	125.31	77.39	125.31	77.39	1.6
Testa	(4+5)-XI-4 (-)	-74.93	-57.46	21.58	125.31	77.39	125.31	77.39	1.8
Testa	(4+5)-VIII-2 (+)	-74.03	-38.86	-1.92	125.15	77.29	125.15	77.29	4.2
Testa	(4+5)-VIII-2 (-)	-74.03	-34.09	-1.64	125.15	77.29	125.15	77.29	5.1
Testa	(4+5)-IV-2 (+)	-73.49	-24.86	-19.53	125.06	77.23	125.06	77.23	3.5
Testa	(4+5)-IV-2 (-)	-73.49	-21.74	-18.22	125.06	77.23	125.06	77.23	3.9
Testa	(4+5)-II-2 (-)	-73.27	-38.11	-0.44	125.02	77.21	125.02	77.21	4.4
Testa	(4+5)-II-2 (+)	-73.27	-43.38	-0.65	125.02	77.21	125.02	77.21	3.6
Testa	(4+5)-XI-2 (+)	-67.89	-59.65	3.78	124.06	76.62	124.06	76.62	2.3
Testa	(4+5)-XI-2 (-)	-67.89	-52.57	3.73	124.06	76.62	124.06	76.62	2.6
Testa	(4+5)-V-2 (+)	-67.13	-64.17	5.05	123.92	76.54	123.92	76.54	2.0
Testa	(4+5)-V-2 (-)	-67.13	-56.58	4.93	123.92	76.54	123.92	76.54	2.4

Zona	C.	N	MyCal	ΔMy	MzCal	ΔMz	Mry+	Mry-	Mrz+	Mrz-
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m
Piede	2 (+)	-158.93	9.64	-0.55	-3.18	1.08	140.04	140.04	86.33	86.33
Piede	2 (-)	-158.93	9.64	0.00	-3.18	0.00	140.04	140.04	86.33	86.33
Piede	3 (+)	-158.29	9.57	-0.55	-3.17	1.07	139.93	139.93	86.26	86.26
Piede	3 (-)	-158.29	9.57	0.00	-3.17	0.00	139.93	139.93	86.26	86.26
Piede	1 (-)	-147.16	8.73	0.00	2.94	0.01	138.01	138.01	85.09	85.09
Piede	1 (+)	-147.16	8.73	-0.48	2.94	-0.01	138.01	138.01	85.09	85.09
Piede	(4+5)-V-3 (-)	-137.40	-71.49	0.00	-0.38	0.00	136.31	136.31	84.06	84.06
Piede	(4+5)-V-3 (+)	-137.40	-71.49	6.89	-0.38	0.18	136.31	136.31	84.06	84.06
Piede	(4+5)-XI-3 (+)	-136.64	-66.18	6.39	-1.68	0.25	136.18	136.18	83.98	83.98
Piede	(4+5)-XI-3 (-)	-136.64	-66.18	0.00	-1.68	0.00	136.18	136.18	83.98	83.98
Piede	(4+5)-II-3 (-)	-131.26	-46.89	0.00	-6.28	0.00	135.24	135.24	83.41	83.41
Piede	(4+5)-II-3 (+)	-131.26	-46.89	4.57	-6.28	0.51	135.24	135.24	83.41	83.41
Piede	(4+5)-IV-3 (-)	-131.04	-23.38	0.00	-26.07	0.00	135.20	135.20	83.39	83.39
Piede	(4+5)-IV-3 (+)	-131.04	-23.38	2.43	-26.07	1.62	135.20	135.20	83.39	83.39
Piede	(4+5)-VIII-3 (+)	-130.50	-41.58	4.07	-7.59	0.59	135.11	135.11	83.33	83.33
Piede	(4+5)-VIII-3 (-)	-130.50	-41.58	0.00	-7.59	0.00	135.11	135.11	83.33	83.33
Piede	(4+5)-XI-1 (+)	-129.60	-72.55	7.00	18.14	-0.85	134.95	134.95	83.24	83.24
Piede	(4+5)-XI-1 (-)	-129.60	-72.55	0.00	18.14	0.00	134.95	134.95	83.24	83.24
Piede	(4+5)-I-3 (+)	-129.19	-16.00	1.73	-27.84	1.72	134.88	134.88	83.19	83.19
Piede	(4+5)-I-3 (-)	-129.19	-16.00	0.00	-27.84	0.00	134.88	134.88	83.19	83.19
Piede	(4+5)-V-1 (-)	-128.84	-67.24	0.00	16.83	0.00	134.82	134.82	83.16	83.16
Piede	(4+5)-V-1 (+)	-128.84	-67.24	6.50	16.83	-0.78	134.82	134.82	83.16	83.16
Piede	(4+5)-X-3 (+)	-128.51	-5.68	0.76	-30.43	1.86	134.76	134.76	83.12	83.12
Piede	(4+5)-X-3 (-)	-128.51	-5.68	0.00	-30.43	0.00	134.76	134.76	83.12	83.12
Piede	(4+5)-VII-3 (+)	-126.66	1.70	0.06	-32.20	1.96	134.44	134.44	82.93	82.93
Piede	(4+5)-VII-3 (-)	-126.66	1.70	0.00	-32.20	0.00	134.44	134.44	82.93	82.93
Piede	(4+5)-VIII-1 (+)	-123.46	-47.95	4.68	12.23	-0.52	133.88	133.88	82.59	82.59
Piede	(4+5)-VIII-1 (-)	-123.46	-47.95	0.00	12.23	0.00	133.88	133.88	82.59	82.59
Piede	(4+5)-II-1 (-)	-122.70	-42.64	0.00	10.93	0.00	133.75	133.75	82.51	82.51
Piede	(4+5)-II-1 (+)	-122.70	-42.64	4.18	10.93	-0.45	133.75	133.75	82.51	82.51
Piede	(4+5)-VI-3 (-)	-121.05	-18.43	0.00	-6.00	0.00	133.46	133.46	82.33	82.33
Piede	(4+5)-VI-3 (+)	-121.05	-18.43	1.96	-6.00	0.50	133.46	133.46	82.33	82.33
Piede	(4+5)-XII-3 (-)	-120.29	-13.12	0.00	-7.30	0.00	133.33	133.33	82.25	82.25
Piede	(4+5)-XII-3 (+)	-120.29	-13.12	1.46	-7.30	0.57	133.33	133.33	82.25	82.25
Piede	(4+5)-III-3 (+)	-119.21	-11.05	1.27	-7.77	0.60	133.14	133.14	82.13	82.13
Piede	(4+5)-III-3 (-)	-119.21	-11.05	0.00	-7.77	0.00	133.14	133.14	82.13	82.13
Piede	(4+5)-I-4 (+)	-118.86	14.72	-1.10	-29.12	1.79	133.08	133.08	82.10	82.10
Piede	(4+5)-I-4 (-)	-118.86	14.72	0.00	-29.12	0.00	133.08	133.08	82.10	82.10
Piede	(4+5)-IX-3 (+)	-118.45	-5.74	0.77	-9.08	0.67	133.00	133.00	82.05	82.05
Piede	(4+5)-IX-3 (-)	-118.45	-5.74	0.00	-9.08	0.00	133.00	133.00	82.05	82.05
Piede	(4+5)-IV-4 (-)	-117.02	22.10	0.00	-30.89	0.00	132.75	132.75	81.90	81.90
Piede	(4+5)-IV-4 (+)	-117.02	22.10	-1.80	-30.89	1.89	132.75	132.75	81.90	81.90
Piede	(4+5)-VII-4 (-)	-116.33	32.42	0.00	-33.47	0.00	132.63	132.63	81.83	81.83
Piede	(4+5)-VII-4 (+)	-116.33	32.42	-2.77	-33.47	2.03	132.63	132.63	81.83	81.83
Piede	(4+5)-X-4 (-)	-114.49	39.80	0.00	-35.24	0.00	132.31	132.31	81.63	81.63
Piede	(4+5)-X-4 (+)	-114.49	39.80	-3.47	-35.24	2.13	132.31	132.31	81.63	81.63
Piede	(4+5)-XII-1 (+)	-113.25	-19.49	2.07	12.51	-0.54	132.09	132.09	81.50	81.50

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 76 di 103

Zona	C.	N	MyCal	ΔMy	MzCal	ΔMz	Mry+	Mry-	Mrz+	Mrz-
Piede	(4+5)-XII-1 (-)	-113.25	-19.49	0.00	12.51	0.00	132.09	132.09	81.50	81.50
Piede	(4+5)-VI-1 (+)	-112.49	-14.18	1.57	11.21	-0.46	131.96	131.96	81.42	81.42
Piede	(4+5)-VI-1 (-)	-112.49	-14.18	0.00	11.21	0.00	131.96	131.96	81.42	81.42
Piede	(4+5)-IX-1 (+)	-111.41	-12.11	1.37	10.74	-0.44	131.77	131.77	81.30	81.30
Piede	(4+5)-IX-1 (-)	-111.41	-12.11	0.00	10.74	0.00	131.77	131.77	81.30	81.30
Piede	(4+5)-III-1 (+)	-110.65	-6.80	0.87	9.44	-0.36	131.63	131.63	81.22	81.22
Piede	(4+5)-III-1 (-)	-110.65	-6.80	0.00	9.44	0.00	131.63	131.63	81.22	81.22
Piede	(4+5)-III-4 (+)	-108.88	19.67	-1.56	-9.05	0.67	131.32	131.32	81.03	81.03
Piede	(4+5)-III-4 (-)	-108.88	19.67	0.00	-9.05	0.00	131.32	131.32	81.03	81.03
Piede	(4+5)-IX-4 (+)	-108.12	24.98	-2.07	-10.35	0.74	131.19	131.19	80.95	80.95
Piede	(4+5)-IX-4 (-)	-108.12	24.98	0.00	-10.35	0.00	131.19	131.19	80.95	80.95
Piede	(4+5)-VI-4 (+)	-107.04	27.05	-2.26	-10.82	0.77	131.00	131.00	80.84	80.84
Piede	(4+5)-VI-4 (-)	-107.04	27.05	0.00	-10.82	0.00	131.00	131.00	80.84	80.84
Piede	(4+5)-XII-4 (-)	-106.28	32.36	0.00	-12.12	0.00	130.87	130.87	80.76	80.76
Piede	(4+5)-XII-4 (+)	-106.28	32.36	-2.76	-12.12	0.84	130.87	130.87	80.76	80.76
Piede	(4+5)-X-1 (-)	-105.04	-26.92	0.00	35.64	0.00	130.65	130.65	80.62	80.62
Piede	(4+5)-X-1 (+)	-105.04	-26.92	2.78	35.64	-1.83	130.65	130.65	80.62	80.62
Piede	(4+5)-VII-1 (+)	-103.20	-19.54	2.08	33.87	-1.73	130.32	130.32	80.43	80.43
Piede	(4+5)-VII-1 (-)	-103.20	-19.54	0.00	33.87	0.00	130.32	130.32	80.43	80.43
Piede	(4+5)-IV-1 (-)	-102.51	-9.23	0.00	31.28	0.00	130.20	130.20	80.35	80.35
Piede	(4+5)-IV-1 (+)	-102.51	-9.23	1.10	31.28	-1.59	130.20	130.20	80.35	80.35
Piede	(4+5)-IX-2 (-)	-101.08	18.61	0.00	9.47	0.00	129.95	129.95	80.20	80.20
Piede	(4+5)-IX-2 (+)	-101.08	18.61	-1.46	9.47	-0.37	129.95	129.95	80.20	80.20
Piede	(4+5)-I-1 (+)	-100.67	-1.85	0.41	29.51	-1.49	129.88	129.88	80.16	80.16
Piede	(4+5)-I-1 (-)	-100.67	-1.85	0.00	29.51	0.00	129.88	129.88	80.16	80.16
Piede	(4+5)-III-2 (+)	-100.32	23.92	-1.96	8.16	-0.29	129.82	129.82	80.12	80.12
Piede	(4+5)-III-2 (-)	-100.32	23.92	0.00	8.16	0.00	129.82	129.82	80.12	80.12
Piede	(4+5)-II-2 (-)	-99.24	25.99	0.00	7.70	0.00	129.62	129.62	80.00	80.00
Piede	(4+5)-XII-2 (+)	-99.24	25.99	-2.16	7.70	-0.27	129.62	129.62	80.00	80.00
Piede	(4+5)-VI-2 (+)	-98.48	31.30	-2.66	6.39	-0.19	129.49	129.49	79.92	79.92
Piede	(4+5)-VI-2 (-)	-98.48	31.30	0.00	6.39	0.00	129.49	129.49	79.92	79.92
Piede	(4+5)-II-4 (+)	-96.83	55.51	-4.87	-10.53	0.75	129.20	129.20	79.74	79.74
Piede	(4+5)-II-4 (-)	-96.83	55.51	0.00	-10.53	0.00	129.20	129.20	79.74	79.74
Piede	(4+5)-VIII-4 (-)	-96.07	60.82	0.00	-11.84	0.00	129.07	129.07	79.66	79.66
Piede	(4+5)-VIII-4 (+)	-96.07	60.82	-5.37	-11.84	0.83	129.07	129.07	79.66	79.66
Piede	(4+5)-VII-2 (+)	-92.87	11.18	-0.75	32.59	-1.66	128.50	128.50	79.32	79.32
Piede	(4+5)-VII-2 (-)	-92.87	11.18	0.00	32.59	0.00	128.50	128.50	79.32	79.32
Piede	(4+5)-X-2 (+)	-91.02	18.56	-1.45	30.82	-1.56	128.17	128.17	79.12	79.12
Piede	(4+5)-X-2 (-)	-91.02	18.56	0.00	30.82	0.00	128.17	128.17	79.12	79.12
Piede	(4+5)-V-4 (-)	-90.69	80.12	0.00	-16.44	0.00	128.11	128.11	79.09	79.09
Piede	(4+5)-V-4 (+)	-90.69	80.12	-7.19	-16.44	1.08	128.11	128.11	79.09	79.09
Piede	(4+5)-I-2 (+)	-90.34	28.87	-2.43	28.24	-1.41	128.05	128.05	79.05	79.05
Piede	(4+5)-I-2 (-)	-90.34	28.87	0.00	28.24	0.00	128.05	128.05	79.05	79.05
Piede	(4+5)-XI-4 (+)	-89.93	85.42	-7.69	-17.74	1.16	127.98	127.98	79.00	79.00
Piede	(4+5)-XI-4 (-)	-89.93	85.42	0.00	-17.74	0.00	127.98	127.98	79.00	79.00
Piede	(4+5)-VIII-2 (+)	-89.03	54.45	-4.77	7.98	-0.28	127.82	127.82	78.91	78.91
Piede	(4+5)-VIII-2 (-)	-89.03	54.45	0.00	7.98	0.00	127.82	127.82	78.91	78.91
Piede	(4+5)-IV-2 (+)	-88.49	36.25	-3.12	26.47	-1.31	127.72	127.72	78.85	78.85
Piede	(4+5)-IV-2 (-)	-88.49	36.25	0.00	26.47	0.00	127.72	127.72	78.85	78.85
Piede	(4+5)-II-2 (-)	-88.27	59.76	0.00	6.67	0.00	127.68	127.68	78.83	78.83
Piede	(4+5)-II-2 (+)	-88.27	59.76	-5.27	6.67	-0.21	127.68	127.68	78.83	78.83
Piede	(4+5)-XI-2 (+)	-82.89	79.05	-7.08	2.07	0.05	126.73	126.73	78.25	78.25
Piede	(4+5)-XI-2 (-)	-82.89	79.05	0.00	2.07	0.00	126.73	126.73	78.25	78.25
Piede	(4+5)-V-2 (+)	-82.13	84.36	-7.59	0.77	0.12	126.60	126.60	78.16	78.16
Piede	(4+5)-V-2 (-)	-82.13	84.36	0.00	0.77	0.00	126.60	126.60	78.16	78.16
Testa	2 (+)	-139.43	-3.49	0.00	9.03	0.00	136.66	136.66	84.28	84.28
Testa	2 (-)	-139.43	-3.49	2.16	9.03	-0.27	136.66	136.66	84.28	84.28
Testa	3 (+)	-138.79	-3.47	0.00	8.62	0.00	136.55	136.55	84.21	84.21
Testa	3 (-)	-138.79	-3.47	2.15	8.62	-0.25	136.55	136.55	84.21	84.21
Testa	1 (-)	-127.66	-3.19	1.98	7.59	-0.21	134.61	134.61	83.03	83.03
Testa	1 (+)	-127.66	-3.19	0.00	7.59	0.00	134.61	134.61	83.03	83.03
Testa	(4+5)-V-3 (-)	-122.40	63.47	-6.89	5.95	-0.18	133.69	133.69	82.47	82.47
Testa	(4+5)-V-3 (+)	-122.40	63.47	0.00	5.95	0.00	133.69	133.69	82.47	82.47
Testa	(4+5)-XI-3 (+)	-121.64	58.96	0.00	7.22	0.00	133.56	133.56	82.39	82.39
Testa	(4+5)-XI-3 (-)	-121.64	58.96	-6.39	7.22	-0.25	133.56	133.56	82.39	82.39
Testa	(4+5)-II-3 (-)	-116.26	42.68	-4.57	11.65	-0.51	132.62	132.62	81.82	81.82
Testa	(4+5)-II-3 (+)	-116.26	42.68	0.00	11.65	0.00	132.62	132.62	81.82	81.82
Testa	(4+5)-IV-3 (-)	-116.04	24.16	-2.43	30.54	-1.62	132.58	132.58	81.80	81.80
Testa	(4+5)-IV-3 (+)	-116.04	24.16	0.00	30.54	0.00	132.58	132.58	81.80	81.80
Testa	(4+5)-VIII-3 (+)	-115.50	38.16	0.00	12.92	0.00	132.49	132.49	81.74	81.74
Testa	(4+5)-VIII-3 (-)	-115.50	38.16	-4.07	12.92	-0.59	132.49	132.49	81.74	81.74
Testa	(4+5)-XI-1 (+)	-114.60	64.45	0.00	-11.74	0.00	132.33	132.33	81.64	81.64
Testa	(4+5)-XI-1 (-)	-114.60	64.45	-7.00	-11.74	0.85	132.33	132.33	81.64	81.64
Testa	(4+5)-I-3 (+)	-114.19	17.92	0.00	32.25	0.00	132.26	132.26	81.60	81.60
Testa	(4+5)-I-3 (-)	-114.19	17.92	-1.73	32.25	-1.72	132.26	132.26	81.60	81.60
Testa	(4+5)-V-1 (-)	-113.84	59.94	-6.50	-10.47	0.78	132.20	132.20	81.56	81.56

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 77 di 103

Zona	C.	N	MyCal	ΔMy	MzCal	ΔMz	Mry+	Mry-	Mrz+	Mrz-
Testa	(4+5)-V-1 (+)	-113.84	59.94	0.00	-10.47	0.00	132.20	132.20	81.56	81.56
Testa	(4+5)-X-3 (+)	-113.51	9.11	0.00	34.78	0.00	132.14	132.14	81.53	81.53
Testa	(4+5)-X-3 (-)	-113.51	9.11	-0.76	34.78	-1.86	132.14	132.14	81.53	81.53
Testa	(4+5)-VII-3 (+)	-111.66	2.87	0.00	36.49	0.00	131.81	131.81	81.33	81.33
Testa	(4+5)-VII-3 (-)	-111.66	2.87	-0.06	36.49	-1.96	131.81	131.81	81.33	81.33
Testa	(4+5)-VIII-1 (+)	-108.46	43.66	0.00	-6.04	0.00	131.25	131.25	80.99	80.99
Testa	(4+5)-VIII-1 (-)	-108.46	43.66	-4.68	-6.04	0.52	131.25	131.25	80.99	80.99
Testa	(4+5)-II-1 (-)	-107.70	39.14	-4.18	-4.77	0.45	131.12	131.12	80.91	80.91
Testa	(4+5)-II-1 (+)	-107.70	39.14	0.00	-4.77	0.00	131.12	131.12	80.91	80.91
Testa	(4+5)-VI-3 (-)	-106.05	20.03	-1.96	11.38	-0.50	130.83	130.83	80.73	80.73
Testa	(4+5)-VI-3 (+)	-106.05	20.03	0.00	11.38	0.00	130.83	130.83	80.73	80.73
Testa	(4+5)-XII-3 (-)	-105.29	15.52	-1.46	12.65	-0.57	130.69	130.69	80.65	80.65
Testa	(4+5)-XII-3 (+)	-105.29	15.52	0.00	12.65	0.00	130.69	130.69	80.65	80.65
Testa	(4+5)-III-3 (+)	-104.21	13.80	0.00	13.09	0.00	130.50	130.50	80.53	80.53
Testa	(4+5)-III-3 (-)	-104.21	13.80	-1.27	13.09	-0.60	130.50	130.50	80.53	80.53
Testa	(4+5)-I-4 (+)	-103.86	-6.84	0.00	33.48	0.00	130.44	130.44	80.50	80.50
Testa	(4+5)-I-4 (-)	-103.86	-6.84	1.10	33.48	-1.79	130.44	130.44	80.50	80.50
Testa	(4+5)-IX-3 (+)	-103.45	9.28	0.00	14.36	0.00	130.37	130.37	80.45	80.45
Testa	(4+5)-IX-3 (-)	-103.45	9.28	-0.77	14.36	-0.67	130.37	130.37	80.45	80.45
Testa	(4+5)-IV-4 (-)	-102.02	-13.07	1.80	35.19	-1.89	130.12	130.12	80.30	80.30
Testa	(4+5)-IV-4 (+)	-102.02	-13.07	0.00	35.19	0.00	130.12	130.12	80.30	80.30
Testa	(4+5)-VII-4 (-)	-101.33	-21.89	2.77	37.72	-2.03	129.99	129.99	80.23	80.23
Testa	(4+5)-VII-4 (+)	-101.33	-21.89	0.00	37.72	0.00	129.99	129.99	80.23	80.23
Testa	(4+5)-X-4 (-)	-99.49	-28.13	3.47	39.43	-2.13	129.67	129.67	80.03	80.03
Testa	(4+5)-X-4 (+)	-99.49	-28.13	0.00	39.43	0.00	129.67	129.67	80.03	80.03
Testa	(4+5)-XII-1 (+)	-98.25	21.02	0.00	-6.31	0.00	129.45	129.45	79.90	79.90
Testa	(4+5)-XII-1 (-)	-98.25	21.02	-2.07	-6.31	0.54	129.45	129.45	79.90	79.90
Testa	(4+5)-IX-1 (+)	-97.49	16.50	0.00	-5.04	0.00	129.32	129.32	79.82	79.82
Testa	(4+5)-VI-1 (-)	-97.49	16.50	-1.57	-5.04	0.46	129.32	129.32	79.82	79.82
Testa	(4+5)-IX-1 (-)	-96.41	14.78	0.00	-4.60	0.00	129.13	129.13	79.70	79.70
Testa	(4+5)-IX-1 (+)	-96.41	14.78	-1.37	-4.60	0.44	129.13	129.13	79.70	79.70
Testa	(4+5)-III-1 (+)	-95.65	10.26	0.00	-3.33	0.00	128.99	128.99	79.62	79.62
Testa	(4+5)-III-1 (-)	-95.65	10.26	-0.87	-3.33	0.36	128.99	128.99	79.62	79.62
Testa	(4+5)-III-4 (+)	-93.88	-10.96	0.00	14.33	0.00	128.68	128.68	79.43	79.43
Testa	(4+5)-III-4 (-)	-93.88	-10.96	1.56	14.33	-0.67	128.68	128.68	79.43	79.43
Testa	(4+5)-IX-4 (+)	-93.12	-15.47	0.00	15.60	0.00	128.54	128.54	79.35	79.35
Testa	(4+5)-IX-4 (-)	-93.12	-15.47	2.07	15.60	-0.74	128.54	128.54	79.35	79.35
Testa	(4+5)-VI-4 (+)	-92.04	-17.20	0.00	16.04	0.00	128.35	128.35	79.23	79.23
Testa	(4+5)-VI-4 (-)	-92.04	-17.20	2.26	16.04	-0.77	128.35	128.35	79.23	79.23
Testa	(4+5)-XII-4 (-)	-91.28	-21.71	2.76	17.31	-0.84	128.22	128.22	79.15	79.15
Testa	(4+5)-XII-4 (+)	-91.28	-21.71	0.00	17.31	0.00	128.22	128.22	79.15	79.15
Testa	(4+5)-X-1 (-)	-90.04	27.43	-2.78	-28.43	1.83	128.00	128.00	79.02	79.02
Testa	(4+5)-X-1 (+)	-90.04	27.43	0.00	-28.43	0.00	128.00	128.00	79.02	79.02
Testa	(4+5)-VII-1 (+)	-88.20	21.19	0.00	-26.72	0.00	127.67	127.67	78.82	78.82
Testa	(4+5)-VII-1 (-)	-88.20	21.19	-2.08	-26.72	1.73	127.67	127.67	78.82	78.82
Testa	(4+5)-IV-1 (-)	-87.51	12.38	-1.10	-24.19	1.59	127.55	127.55	78.74	78.74
Testa	(4+5)-IV-1 (+)	-87.51	12.38	0.00	-24.19	0.00	127.55	127.55	78.74	78.74
Testa	(4+5)-IX-2 (-)	-86.08	-9.98	1.46	-3.36	0.37	127.30	127.30	78.59	78.59
Testa	(4+5)-IX-2 (+)	-86.08	-9.98	0.00	-3.36	0.00	127.30	127.30	78.59	78.59
Testa	(4+5)-I-1 (+)	-85.67	6.14	0.00	-22.48	0.00	127.22	127.22	78.55	78.55
Testa	(4+5)-I-1 (-)	-85.67	6.14	-0.41	-22.48	1.49	127.22	127.22	78.55	78.55
Testa	(4+5)-III-2 (+)	-85.32	-14.49	0.00	-2.09	0.00	127.16	127.16	78.51	78.51
Testa	(4+5)-III-2 (-)	-85.32	-14.49	1.96	-2.09	0.29	127.16	127.16	78.51	78.51
Testa	(4+5)-XII-2 (-)	-84.24	-16.22	2.16	-1.65	0.27	126.97	126.97	78.39	78.39
Testa	(4+5)-XII-2 (+)	-84.24	-16.22	0.00	-1.65	0.00	126.97	126.97	78.39	78.39
Testa	(4+5)-VI-2 (+)	-83.48	-20.73	0.00	-0.38	0.00	126.84	126.84	78.31	78.31
Testa	(4+5)-VI-2 (-)	-83.48	-20.73	2.66	-0.38	0.19	126.84	126.84	78.31	78.31
Testa	(4+5)-II-4 (+)	-81.83	-39.84	0.00	15.77	0.00	126.54	126.54	78.13	78.13
Testa	(4+5)-II-4 (-)	-81.83	-39.84	4.87	15.77	-0.75	126.54	126.54	78.13	78.13
Testa	(4+5)-VIII-4 (-)	-81.07	-44.36	5.37	17.04	-0.83	126.41	126.41	78.05	78.05
Testa	(4+5)-VIII-4 (+)	-81.07	-44.36	0.00	17.04	0.00	126.41	126.41	78.05	78.05
Testa	(4+5)-VII-2 (+)	-77.87	-3.57	0.00	-25.49	0.00	125.84	125.84	77.70	77.70
Testa	(4+5)-VII-2 (-)	-77.87	-3.57	0.75	-25.49	1.66	125.84	125.84	77.70	77.70
Testa	(4+5)-X-2 (+)	-76.02	-9.80	0.00	-23.78	0.00	125.51	125.51	77.51	77.51
Testa	(4+5)-X-2 (-)	-76.02	-9.80	1.45	-23.78	1.56	125.51	125.51	77.51	77.51
Testa	(4+5)-V-4 (-)	-75.69	-60.63	7.19	21.47	-1.08	125.45	125.45	77.47	77.47
Testa	(4+5)-V-4 (+)	-75.69	-60.63	0.00	21.47	0.00	125.45	125.45	77.47	77.47
Testa	(4+5)-I-2 (+)	-75.34	-18.62	0.00	-21.25	0.00	125.39	125.39	77.43	77.43
Testa	(4+5)-I-2 (-)	-75.34	-18.62	2.43	-21.25	1.41	125.39	125.39	77.43	77.43
Testa	(4+5)-XI-4 (+)	-74.93	-65.15	0.00	22.74	0.00	125.31	125.31	77.39	77.39
Testa	(4+5)-XI-4 (-)	-74.93	-65.15	7.69	22.74	-1.16	125.31	125.31	77.39	77.39
Testa	(4+5)-VIII-2 (+)	-74.03	-38.86	0.00	-1.92	0.00	125.15	125.15	77.29	77.29
Testa	(4+5)-VIII-2 (-)	-74.03	-38.86	4.77	-1.92	0.28	125.15	125.15	77.29	77.29
Testa	(4+5)-IV-2 (+)	-73.49	-24.86	0.00	-19.53	0.00	125.06	125.06	77.23	77.23
Testa	(4+5)-IV-2 (-)	-73.49	-24.86	3.12	-19.53	1.31	125.06	125.06	77.23	77.23
Testa	(4+5)-II-2 (-)	-73.27	-43.38	5.27	-0.65	0.21	125.02	125.02	77.21	77.21

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021
Pagina 78 di 103

Zona	C.	N	MyCal	ΔMy	MzCal	ΔMz	Mry+	Mry-	Mrz+	Mrz-
Testa	(4+5)-II-2(+)	-73.27	-43.38	0.00	-0.65	0.00	125.02	125.02	77.21	77.21
Testa	(4+5)-XI-2(+)	-67.89	-59.65	0.00	3.78	0.00	124.06	124.06	76.62	76.62
Testa	(4+5)-XI-2(-)	-67.89	-59.65	7.08	3.78	-0.05	124.06	124.06	76.62	76.62
Testa	(4+5)-V-2(+)	-67.13	-64.17	0.00	5.05	0.00	123.92	123.92	76.54	76.54
Testa	(4+5)-V-2(-)	-67.13	-64.17	7.59	5.05	-0.12	123.92	123.92	76.54	76.54

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrzd	Vrzd	Vrd	Ast/m	cot (θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(4+5)-X-4	--	--	18.67	--	432.14	209.09	209.09	9.35	2.500	11
Z	(4+5)-XI-4	--	--	37.64	--	459.98	373.73	373.73	9.35	2.500	9.9

Pilastro: 5 [5,105] Sez. R: By=50.00 cm Bz=30.00 cm L=400.00 cm Ln=400.00 cm Criterio: CLS_Pilastri_ND - Verifica a presso-flessione deviata, $\zeta_g=1.531$ [(4+5)-VII-2] : **Verificato**

Piede	AfSpigolo = 3.14	Afy = 1.54	Afz = 0.00
Testa	AfSpigolo = 3.14	Afy = 1.54	Afz = 0.00

$v_{max}=N/(fcd*A)=0.069 \leq 0.65$ [Comb. (4+5)-VIII-3(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	2(+)	-310.75	8.74	7.74	101.78	165.47	101.78	165.47	9.3
Piede	2(-)	-310.75	9.28	7.77	101.78	165.47	101.78	165.47	9.2
Piede	3(+)	-306.31	8.74	7.63	101.34	164.75	101.34	164.75	9.4
Piede	3(-)	-306.31	9.29	7.66	101.34	164.75	101.34	164.75	9.2
Piede	1(-)	-282.87	8.40	7.07	99.01	160.91	99.01	160.91	10
Piede	1(+)	-282.87	7.91	7.05	99.01	160.91	99.01	160.91	10
Piede	(4+5)-II-1(+)	-221.94	-17.82	11.36	92.85	150.77	92.85	150.77	7.9
Piede	(4+5)-II-1(-)	-221.94	-18.63	12.54	92.85	150.77	92.85	150.77	7.6
Piede	(4+5)-VIII-3(+)	-221.94	-17.82	-32.61	92.85	150.77	92.85	150.77	5.4
Piede	(4+5)-VIII-3(-)	-221.94	-18.63	-36.13	92.85	150.77	92.85	150.77	4.9
Piede	(4+5)-II-3(-)	-221.94	-18.63	-32.97	92.85	150.77	92.85	150.77	5.2
Piede	(4+5)-II-3(+)	-221.94	-17.82	-29.76	92.85	150.77	92.85	150.77	5.8
Piede	(4+5)-VIII-1(-)	-221.94	-18.63	15.70	92.85	150.77	92.85	150.77	7.3
Piede	(4+5)-VIII-1(+)	-221.94	-17.82	14.20	92.85	150.77	92.85	150.77	7.6
Piede	(4+5)-V-1(+)	-221.93	-17.81	29.78	92.85	150.77	92.85	150.77	5.8
Piede	(4+5)-V-1(-)	-221.93	-18.63	33.00	92.85	150.77	92.85	150.77	5.2
Piede	(4+5)-XI-3(+)	-221.93	-17.81	-14.18	92.85	150.77	92.85	150.77	7.6
Piede	(4+5)-XI-3(-)	-221.93	-18.63	-15.68	92.85	150.77	92.85	150.77	7.3
Piede	(4+5)-XI-1(-)	-221.93	-18.63	36.15	92.85	150.77	92.85	150.77	4.9
Piede	(4+5)-XI-1(+)	-221.93	-17.81	32.63	92.85	150.77	92.85	150.77	5.4
Piede	(4+5)-V-3(-)	-221.93	-18.63	-12.52	92.85	150.77	92.85	150.77	7.6
Piede	(4+5)-V-3(+)	-221.93	-17.81	-11.34	92.85	150.77	92.85	150.77	7.9
Piede	(4+5)-I-1(+)	-212.68	-1.36	72.80	91.90	149.21	91.90	149.21	2.9
Piede	(4+5)-I-1(-)	-212.68	-1.36	65.78	91.90	149.21	91.90	149.21	3.5
Piede	(4+5)-VII-3(-)	-212.68	-1.36	-89.44	91.90	149.21	91.90	149.21	2.1
Piede	(4+5)-VII-3(+)	-212.68	-1.36	-80.78	91.90	149.21	91.90	149.21	2.4
Piede	(4+5)-III-1(+)	-212.68	-1.36	17.80	91.90	149.21	91.90	149.21	12
Piede	(4+5)-III-1(-)	-212.68	-1.36	19.69	91.90	149.21	91.90	149.21	11
Piede	(4+5)-IX-3(-)	-212.68	-1.36	-28.98	91.90	149.21	91.90	149.21	9.1
Piede	(4+5)-IX-3(+)	-212.68	-1.36	-26.17	91.90	149.21	91.90	149.21	9.7
Piede	(4+5)-IX-1(-)	-212.68	-1.36	22.85	91.90	149.21	91.90	149.21	10
Piede	(4+5)-IX-1(+)	-212.68	-1.36	20.64	91.90	149.21	91.90	149.21	11
Piede	(4+5)-III-3(+)	-212.68	-1.36	-23.32	91.90	149.21	91.90	149.21	10
Piede	(4+5)-III-3(-)	-212.68	-1.36	-25.82	91.90	149.21	91.90	149.21	9.8
Piede	(4+5)-VII-1(+)	-212.68	-1.36	75.26	91.90	149.21	91.90	149.21	2.7
Piede	(4+5)-VII-1(-)	-212.68	-1.36	83.31	91.90	149.21	91.90	149.21	2.3
Piede	(4+5)-I-3(-)	-212.68	-1.36	-78.93	91.90	149.21	91.90	149.21	2.5
Piede	(4+5)-I-3(+)	-212.68	-1.36	-71.30	91.90	149.21	91.90	149.21	3.0
Piede	(4+5)-X-3(-)	-212.68	-1.36	-83.31	91.90	149.21	91.90	149.21	2.3
Piede	(4+5)-X-3(+)	-212.68	-1.36	-75.25	91.90	149.21	91.90	149.21	2.8
Piede	(4+5)-IV-1(+)	-212.68	-1.36	71.31	91.90	149.21	91.90	149.21	3.0
Piede	(4+5)-IV-1(-)	-212.68	-1.36	78.94	91.90	149.21	91.90	149.21	2.5
Piede	(4+5)-XII-3(+)	-212.68	-1.36	-20.64	91.90	149.21	91.90	149.21	11
Piede	(4+5)-XII-3(-)	-212.68	-1.36	-22.84	91.90	149.21	91.90	149.21	10
Piede	(4+5)-VI-1(+)	-212.68	-1.36	23.33	91.90	149.21	91.90	149.21	10
Piede	(4+5)-VI-1(-)	-212.68	-1.36	25.83	91.90	149.21	91.90	149.21	9.8
Piede	(4+5)-XII-1(-)	-212.68	-1.36	28.98	91.90	149.21	91.90	149.21	9.1
Piede	(4+5)-XII-1(+)	-212.68	-1.36	26.17	91.90	149.21	91.90	149.21	9.7
Piede	(4+5)-VI-3(-)	-212.68	-1.36	-19.69	91.90	149.21	91.90	149.21	11
Piede	(4+5)-VI-3(+)	-212.68	-1.36	-17.79	91.90	149.21	91.90	149.21	12
Piede	(4+5)-IV-3(+)	-212.68	-1.36	-65.77	91.90	149.21	91.90	149.21	3.5
Piede	(4+5)-IV-3(-)	-212.68	-1.36	-72.79	91.90	149.21	91.90	149.21	2.9

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 79 di 103

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
Piede	(4+5)-X-1(+)	-212.68	-1.36	80.78	91.90	149.21	91.90	149.21	2.4
Piede	(4+5)-X-1(-)	-212.68	-1.36	89.45	91.90	149.21	91.90	149.21	2.1
Piede	(4+5)-X-4(-)	-204.76	13.45	-89.45	91.08	147.87	91.08	147.87	1.8
Piede	(4+5)-X-4(+)	-204.76	12.75	-80.78	91.08	147.87	91.08	147.87	2.1
Piede	(4+5)-IV-2(+)	-204.76	12.75	65.77	91.08	147.87	91.08	147.87	2.7
Piede	(4+5)-IV-2(-)	-204.76	13.44	72.79	91.08	147.87	91.08	147.87	2.4
Piede	(4+5)-VI-2(+)	-204.76	12.75	17.79	91.08	147.87	91.08	147.87	8.6
Piede	(4+5)-VI-2(-)	-204.76	13.45	19.69	91.08	147.87	91.08	147.87	8.1
Piede	(4+5)-XII-4(-)	-204.76	13.45	-28.98	91.08	147.87	91.08	147.87	6.8
Piede	(4+5)-XII-4(+)	-204.76	12.75	-26.17	91.08	147.87	91.08	147.87	7.4
Piede	(4+5)-VI-4(+)	-204.76	12.75	-23.33	91.08	147.87	91.08	147.87	7.8
Piede	(4+5)-VI-4(-)	-204.76	13.45	-25.83	91.08	147.87	91.08	147.87	7.3
Piede	(4+5)-XII-2(+)	-204.76	12.75	20.64	91.08	147.87	91.08	147.87	8.2
Piede	(4+5)-XII-2(-)	-204.76	13.45	22.84	91.08	147.87	91.08	147.87	7.7
Piede	(4+5)-IV-4(+)	-204.76	12.75	-71.31	91.08	147.87	91.08	147.87	2.4
Piede	(4+5)-IV-4(-)	-204.76	13.45	-78.94	91.08	147.87	91.08	147.87	2.1
Piede	(4+5)-X-2(-)	-204.76	13.45	83.31	91.08	147.87	91.08	147.87	2.0
Piede	(4+5)-X-2(+)	-204.76	12.75	75.25	91.08	147.87	91.08	147.87	2.3
Piede	(4+5)-I-2(+)	-204.75	12.75	71.30	91.08	147.87	91.08	147.87	2.5
Piede	(4+5)-I-2(-)	-204.75	13.45	78.93	91.08	147.87	91.08	147.87	2.1
Piede	(4+5)-VII-4(-)	-204.75	13.45	-83.31	91.08	147.87	91.08	147.87	2.0
Piede	(4+5)-VII-4(+)	-204.75	12.75	-75.26	91.08	147.87	91.08	147.87	2.3
Piede	(4+5)-III-2(-)	-204.75	13.45	25.82	91.08	147.87	91.08	147.87	7.3
Piede	(4+5)-III-2(+)	-204.75	12.75	23.32	91.08	147.87	91.08	147.87	7.7
Piede	(4+5)-IX-4(-)	-204.75	13.45	-22.85	91.08	147.87	91.08	147.87	7.7
Piede	(4+5)-IX-4(+)	-204.75	12.75	-20.64	91.08	147.87	91.08	147.87	8.2
Piede	(4+5)-IX-2(-)	-204.75	13.45	28.98	91.08	147.87	91.08	147.87	6.8
Piede	(4+5)-IX-2(+)	-204.75	12.75	26.17	91.08	147.87	91.08	147.87	7.4
Piede	(4+5)-III-4(-)	-204.75	13.45	-19.69	91.08	147.87	91.08	147.87	8.1
Piede	(4+5)-III-4(+)	-204.75	12.75	-17.80	91.08	147.87	91.08	147.87	8.6
Piede	(4+5)-VII-2(-)	-204.75	13.45	89.44	91.08	147.87	91.08	147.87	1.8
Piede	(4+5)-VII-2(+)	-204.75	12.75	80.78	91.08	147.87	91.08	147.87	2.1
Piede	(4+5)-I-4(+)	-204.75	12.75	-65.78	91.08	147.87	91.08	147.87	2.7
Piede	(4+5)-I-4(-)	-204.75	13.45	-72.80	91.08	147.87	91.08	147.87	2.4
Piede	(4+5)-V-2(+)	-195.51	29.20	11.34	90.13	146.30	90.13	146.30	4.8
Piede	(4+5)-V-2(-)	-195.51	30.71	12.52	90.13	146.30	90.13	146.30	4.4
Piede	(4+5)-XI-4(+)	-195.51	29.20	-32.63	90.13	146.30	90.13	146.30	3.3
Piede	(4+5)-XI-4(-)	-195.51	30.71	-36.15	90.13	146.30	90.13	146.30	3.0
Piede	(4+5)-XI-2(-)	-195.51	30.71	15.68	90.13	146.30	90.13	146.30	4.2
Piede	(4+5)-XI-2(+)	-195.51	29.20	14.18	90.13	146.30	90.13	146.30	4.6
Piede	(4+5)-V-4(+)	-195.51	29.20	-29.78	90.13	146.30	90.13	146.30	3.5
Piede	(4+5)-V-4(-)	-195.51	30.71	-33.00	90.13	146.30	90.13	146.30	3.1
Piede	(4+5)-VIII-4(+)	-195.50	29.20	-14.20	90.13	146.30	90.13	146.30	4.6
Piede	(4+5)-VIII-4(-)	-195.50	30.72	-15.70	90.13	146.30	90.13	146.30	4.2
Piede	(4+5)-II-2(-)	-195.50	30.72	32.97	90.13	146.30	90.13	146.30	3.1
Piede	(4+5)-II-2(+)	-195.50	29.20	29.76	90.13	146.30	90.13	146.30	3.5
Piede	(4+5)-VIII-2(-)	-195.50	30.72	36.13	90.13	146.30	90.13	146.30	3.0
Piede	(4+5)-VIII-2(+)	-195.50	29.20	32.61	90.13	146.30	90.13	146.30	3.3
Piede	(4+5)-II-4(+)	-195.50	29.20	-11.36	90.13	146.30	90.13	146.30	4.8
Piede	(4+5)-II-4(-)	-195.50	30.72	-12.54	90.13	146.30	90.13	146.30	4.4
Testa	2(+)	-291.25	-9.82	-7.26	99.85	162.29	99.85	162.29	9.5
Testa	2(-)	-291.25	-9.27	-7.31	99.85	162.29	99.85	162.29	9.6
Testa	3(+)	-286.81	-9.94	-7.15	99.40	161.56	99.40	161.56	9.6
Testa	3(-)	-286.81	-9.39	-7.20	99.40	161.56	99.40	161.56	9.8
Testa	1(-)	-263.37	-8.12	-6.61	97.05	157.69	97.05	157.69	11
Testa	1(+)	-263.37	-8.60	-6.56	97.05	157.69	97.05	157.69	11
Testa	(4+5)-II-1(+)	-206.94	9.82	-10.66	91.31	148.24	91.31	148.24	11
Testa	(4+5)-II-1(-)	-206.94	9.01	-9.48	91.31	148.24	91.31	148.24	12
Testa	(4+5)-VIII-3(+)	-206.94	9.82	32.80	91.31	148.24	91.31	148.24	7.0
Testa	(4+5)-VIII-3(-)	-206.94	9.01	29.28	91.31	148.24	91.31	148.24	7.7
Testa	(4+5)-II-3(-)	-206.94	9.01	26.67	91.31	148.24	91.31	148.24	8.1
Testa	(4+5)-II-3(+)	-206.94	9.82	29.88	91.31	148.24	91.31	148.24	7.4
Testa	(4+5)-VIII-1(-)	-206.94	9.01	-12.09	91.31	148.24	91.31	148.24	11
Testa	(4+5)-VIII-1(+)	-206.94	9.82	-13.58	91.31	148.24	91.31	148.24	10
Testa	(4+5)-V-1(+)	-206.93	9.81	-29.90	91.31	148.24	91.31	148.24	7.4
Testa	(4+5)-V-1(-)	-206.93	9.00	-26.69	91.31	148.24	91.31	148.24	8.1
Testa	(4+5)-XI-3(+)	-206.93	9.81	13.56	91.31	148.24	91.31	148.24	10
Testa	(4+5)-XI-3(-)	-206.93	9.00	12.07	91.31	148.24	91.31	148.24	11
Testa	(4+5)-XI-1(-)	-206.93	9.00	-29.30	91.31	148.24	91.31	148.24	7.7
Testa	(4+5)-XI-1(+)	-206.93	9.81	-32.82	91.31	148.24	91.31	148.24	7.0
Testa	(4+5)-V-3(-)	-206.93	9.00	9.46	91.31	148.24	91.31	148.24	12
Testa	(4+5)-V-3(+)	-206.93	9.81	10.64	91.31	148.24	91.31	148.24	11
Testa	(4+5)-I-1(-)	-197.68	-1.39	-57.66	90.36	146.67	90.36	146.67	4.1
Testa	(4+5)-I-1(+)	-197.68	-1.40	-64.68	90.36	146.67	90.36	146.67	3.4
Testa	(4+5)-VII-3(-)	-197.68	-1.39	71.52	90.36	146.67	90.36	146.67	2.8
Testa	(4+5)-VII-3(+)	-197.68	-1.40	80.19	90.36	146.67	90.36	146.67	2.4

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 80 di 103

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
Testa	(4+5)-III-1(+)	-197.68	-1.40	-17.39	90.36	146.67	90.36	146.67	12
Testa	(4+5)-III-1(-)	-197.68	-1.39	-15.49	90.36	146.67	90.36	146.67	13
Testa	(4+5)-IX-3(-)	-197.68	-1.39	23.26	90.36	146.67	90.36	146.67	11
Testa	(4+5)-IX-3(+)	-197.68	-1.40	26.07	90.36	146.67	90.36	146.67	9.9
Testa	(4+5)-IX-1(-)	-197.68	-1.39	-18.11	90.36	146.67	90.36	146.67	12
Testa	(4+5)-IX-1(+)	-197.68	-1.40	-20.31	90.36	146.67	90.36	146.67	11
Testa	(4+5)-III-3(+)	-197.68	-1.40	23.15	90.36	146.67	90.36	146.67	11
Testa	(4+5)-III-3(-)	-197.68	-1.39	20.65	90.36	146.67	90.36	146.67	11
Testa	(4+5)-VII-1(+)	-197.68	-1.40	-74.42	90.36	146.67	90.36	146.67	2.7
Testa	(4+5)-VII-1(-)	-197.68	-1.39	-66.37	90.36	146.67	90.36	146.67	3.2
Testa	(4+5)-I-3(-)	-197.68	-1.39	62.82	90.36	146.67	90.36	146.67	3.5
Testa	(4+5)-I-3(+)	-197.68	-1.40	70.45	90.36	146.67	90.36	146.67	2.9
Testa	(4+5)-X-3(-)	-197.68	-1.40	66.36	90.36	146.67	90.36	146.67	3.2
Testa	(4+5)-X-3(+)	-197.68	-1.40	74.42	90.36	146.67	90.36	146.67	2.7
Testa	(4+5)-IV-1(+)	-197.68	-1.40	-70.45	90.36	146.67	90.36	146.67	2.9
Testa	(4+5)-IV-1(-)	-197.68	-1.40	-62.82	90.36	146.67	90.36	146.67	3.5
Testa	(4+5)-XII-3(+)	-197.68	-1.40	20.30	90.36	146.67	90.36	146.67	12
Testa	(4+5)-XII-3(-)	-197.68	-1.40	18.10	90.36	146.67	90.36	146.67	12
Testa	(4+5)-VI-1(+)	-197.68	-1.40	-23.16	90.36	146.67	90.36	146.67	11
Testa	(4+5)-VI-1(-)	-197.68	-1.40	-20.66	90.36	146.67	90.36	146.67	11
Testa	(4+5)-XII-1(-)	-197.68	-1.40	-23.27	90.36	146.67	90.36	146.67	11
Testa	(4+5)-XII-1(+)	-197.68	-1.40	-26.08	90.36	146.67	90.36	146.67	9.9
Testa	(4+5)-VI-3(-)	-197.68	-1.40	15.49	90.36	146.67	90.36	146.67	13
Testa	(4+5)-VI-3(+)	-197.68	-1.40	17.38	90.36	146.67	90.36	146.67	12
Testa	(4+5)-IV-3(+)	-197.68	-1.40	64.68	90.36	146.67	90.36	146.67	3.4
Testa	(4+5)-IV-3(-)	-197.68	-1.40	57.66	90.36	146.67	90.36	146.67	4.1
Testa	(4+5)-X-1(+)	-197.68	-1.40	-80.19	90.36	146.67	90.36	146.67	2.4
Testa	(4+5)-X-1(-)	-197.68	-1.40	-71.53	90.36	146.67	90.36	146.67	2.8
Testa	(4+5)-X-4(-)	-189.76	-10.31	71.53	89.54	145.32	89.54	145.32	2.4
Testa	(4+5)-X-4(+)	-189.76	-11.01	80.19	89.54	145.32	89.54	145.32	2.0
Testa	(4+5)-IV-2(+)	-189.76	-11.01	-64.68	89.54	145.32	89.54	145.32	2.8
Testa	(4+5)-IV-2(-)	-189.76	-10.31	-57.66	89.54	145.32	89.54	145.32	3.3
Testa	(4+5)-VI-2(+)	-189.76	-11.01	-17.38	89.54	145.32	89.54	145.32	9.4
Testa	(4+5)-VI-2(-)	-189.76	-10.31	-15.49	89.54	145.32	89.54	145.32	10
Testa	(4+5)-XII-4(-)	-189.76	-10.31	23.27	89.54	145.32	89.54	145.32	8.5
Testa	(4+5)-XII-4(+)	-189.76	-11.01	26.08	89.54	145.32	89.54	145.32	7.8
Testa	(4+5)-VI-4(+)	-189.76	-11.01	23.16	89.54	145.32	89.54	145.32	8.3
Testa	(4+5)-VI-4(-)	-189.76	-10.31	20.66	89.54	145.32	89.54	145.32	9.0
Testa	(4+5)-XII-2(+)	-189.76	-11.01	-20.30	89.54	145.32	89.54	145.32	8.9
Testa	(4+5)-XII-2(-)	-189.76	-10.31	-18.10	89.54	145.32	89.54	145.32	9.6
Testa	(4+5)-IV-4(+)	-189.76	-11.01	70.45	89.54	145.32	89.54	145.32	2.5
Testa	(4+5)-IV-4(-)	-189.76	-10.31	62.82	89.54	145.32	89.54	145.32	2.9
Testa	(4+5)-X-2(-)	-189.76	-10.31	-66.36	89.54	145.32	89.54	145.32	2.7
Testa	(4+5)-X-2(+)	-189.76	-11.01	-74.42	89.54	145.32	89.54	145.32	2.3
Testa	(4+5)-I-2(+)	-189.75	-11.01	-70.45	89.54	145.32	89.54	145.32	2.5
Testa	(4+5)-I-2(-)	-189.75	-10.31	-62.82	89.54	145.32	89.54	145.32	2.9
Testa	(4+5)-VII-4(-)	-189.75	-10.31	66.37	89.54	145.32	89.54	145.32	2.7
Testa	(4+5)-VII-4(+)	-189.75	-11.01	74.42	89.54	145.32	89.54	145.32	2.3
Testa	(4+5)-III-2(-)	-189.75	-10.31	-20.65	89.54	145.32	89.54	145.32	9.0
Testa	(4+5)-III-2(+)	-189.75	-11.01	-23.15	89.54	145.32	89.54	145.32	8.3
Testa	(4+5)-IX-4(-)	-189.75	-10.31	18.11	89.54	145.32	89.54	145.32	9.6
Testa	(4+5)-IX-4(+)	-189.75	-11.01	20.31	89.54	145.32	89.54	145.32	8.9
Testa	(4+5)-IX-2(-)	-189.75	-10.31	-23.26	89.54	145.32	89.54	145.32	8.5
Testa	(4+5)-IX-2(+)	-189.75	-11.01	-26.07	89.54	145.32	89.54	145.32	7.8
Testa	(4+5)-III-4(-)	-189.75	-10.31	15.49	89.54	145.32	89.54	145.32	10
Testa	(4+5)-III-4(+)	-189.75	-11.01	17.39	89.54	145.32	89.54	145.32	9.4
Testa	(4+5)-VII-2(-)	-189.75	-10.31	-71.52	89.54	145.32	89.54	145.32	2.4
Testa	(4+5)-VII-2(+)	-189.75	-11.01	-80.19	89.54	145.32	89.54	145.32	2.0
Testa	(4+5)-I-4(+)	-189.75	-11.01	64.68	89.54	145.32	89.54	145.32	2.8
Testa	(4+5)-I-4(-)	-189.75	-10.31	57.66	89.54	145.32	89.54	145.32	3.3
Testa	(4+5)-V-2(+)	-180.51	-22.22	-10.64	88.58	143.75	88.58	143.75	6.7
Testa	(4+5)-V-2(-)	-180.51	-20.71	-9.46	88.58	143.75	88.58	143.75	7.4
Testa	(4+5)-XI-4(+)	-180.51	-22.22	32.82	88.58	143.75	88.58	143.75	4.2
Testa	(4+5)-XI-4(-)	-180.51	-20.71	29.30	88.58	143.75	88.58	143.75	4.8
Testa	(4+5)-XI-2(-)	-180.51	-20.71	-12.07	88.58	143.75	88.58	143.75	7.0
Testa	(4+5)-XI-2(+)	-180.51	-22.22	-13.56	88.58	143.75	88.58	143.75	6.3
Testa	(4+5)-V-4(+)	-180.51	-22.22	29.90	88.58	143.75	88.58	143.75	4.4
Testa	(4+5)-V-4(-)	-180.51	-20.71	26.69	88.58	143.75	88.58	143.75	5.1
Testa	(4+5)-VIII-4(+)	-180.50	-22.23	13.58	88.58	143.74	88.58	143.74	6.3
Testa	(4+5)-VIII-4(-)	-180.50	-20.71	12.09	88.58	143.74	88.58	143.74	7.0
Testa	(4+5)-II-2(-)	-180.50	-20.71	-26.67	88.58	143.74	88.58	143.74	5.1
Testa	(4+5)-II-2(+)	-180.50	-22.23	-29.88	88.58	143.74	88.58	143.74	4.4
Testa	(4+5)-VIII-2(-)	-180.50	-20.71	-29.28	88.58	143.74	88.58	143.74	4.8
Testa	(4+5)-VIII-2(+)	-180.50	-22.23	-32.80	88.58	143.74	88.58	143.74	4.2
Testa	(4+5)-II-4(+)	-180.50	-22.23	10.66	88.58	143.74	88.58	143.74	6.7
Testa	(4+5)-II-4(-)	-180.50	-20.71	9.48	88.58	143.74	88.58	143.74	7.4

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 81 di 103

Zona	C.	N	MyCal	ΔMy	MzCal	ΔMz	Mry+	Mry-	Mrz+	Mrz-
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m
Piede	2 (+)	-310.75	9.28	-0.54	7.77	-0.02	101.78	101.78	165.47	165.47
Piede	2 (-)	-310.75	9.28	0.00	7.77	0.00	101.78	101.78	165.47	165.47
Piede	3 (+)	-306.31	9.29	-0.55	7.66	-0.02	101.34	101.34	164.75	164.75
Piede	3 (-)	-306.31	9.29	0.00	7.66	0.00	101.34	101.34	164.75	164.75
Piede	1 (-)	-282.87	8.40	0.00	7.07	0.00	99.01	99.01	160.91	160.91
Piede	1 (+)	-282.87	8.40	-0.48	7.07	-0.02	99.01	99.01	160.91	160.91
Piede	(4+5)-II-1 (+)	-221.94	-18.63	0.81	12.54	-1.19	92.85	92.85	150.77	150.77
Piede	(4+5)-II-1 (-)	-221.94	-18.63	0.00	12.54	0.00	92.85	92.85	150.77	150.77
Piede	(4+5)-VIII-3 (+)	-221.94	-18.63	0.81	-36.13	3.52	92.85	92.85	150.77	150.77
Piede	(4+5)-VIII-3 (-)	-221.94	-18.63	0.00	-36.13	0.00	92.85	92.85	150.77	150.77
Piede	(4+5)-II-3 (-)	-221.94	-18.63	0.00	-32.97	0.00	92.85	92.85	150.77	150.77
Piede	(4+5)-II-3 (+)	-221.94	-18.63	0.81	-32.97	3.21	92.85	92.85	150.77	150.77
Piede	(4+5)-VIII-1 (-)	-221.94	-18.63	0.00	15.70	0.00	92.85	92.85	150.77	150.77
Piede	(4+5)-VIII-1 (+)	-221.94	-18.63	0.81	15.70	-1.50	92.85	92.85	150.77	150.77
Piede	(4+5)-V-1 (+)	-221.93	-18.63	0.81	33.00	-3.21	92.85	92.85	150.77	150.77
Piede	(4+5)-V-1 (-)	-221.93	-18.63	0.00	33.00	0.00	92.85	92.85	150.77	150.77
Piede	(4+5)-XI-3 (+)	-221.93	-18.63	0.81	-15.68	1.49	92.85	92.85	150.77	150.77
Piede	(4+5)-XI-3 (-)	-221.93	-18.63	0.00	-15.68	0.00	92.85	92.85	150.77	150.77
Piede	(4+5)-XI-1 (-)	-221.93	-18.63	0.00	36.15	0.00	92.85	92.85	150.77	150.77
Piede	(4+5)-XI-1 (+)	-221.93	-18.63	0.81	36.15	-3.52	92.85	92.85	150.77	150.77
Piede	(4+5)-V-3 (-)	-221.93	-18.63	0.00	-12.52	0.00	92.85	92.85	150.77	150.77
Piede	(4+5)-V-3 (+)	-221.93	-18.63	0.81	-12.52	1.18	92.85	92.85	150.77	150.77
Piede	(4+5)-I-1 (-)	-212.68	-1.36	0.00	72.80	0.00	91.90	91.90	149.21	149.21
Piede	(4+5)-I-1 (+)	-212.68	-1.36	-0.00	72.80	-7.02	91.90	91.90	149.21	149.21
Piede	(4+5)-VII-3 (-)	-212.68	-1.36	0.00	-89.44	0.00	91.90	91.90	149.21	149.21
Piede	(4+5)-VII-3 (+)	-212.68	-1.36	-0.00	-89.44	8.66	91.90	91.90	149.21	149.21
Piede	(4+5)-III-1 (+)	-212.68	-1.36	-0.00	19.69	-1.89	91.90	91.90	149.21	149.21
Piede	(4+5)-III-1 (-)	-212.68	-1.36	0.00	19.69	0.00	91.90	91.90	149.21	149.21
Piede	(4+5)-IX-3 (-)	-212.68	-1.36	0.00	-28.98	0.00	91.90	91.90	149.21	149.21
Piede	(4+5)-IX-3 (+)	-212.68	-1.36	-0.00	-28.98	2.81	91.90	91.90	149.21	149.21
Piede	(4+5)-IX-1 (-)	-212.68	-1.36	0.00	22.85	0.00	91.90	91.90	149.21	149.21
Piede	(4+5)-IX-1 (+)	-212.68	-1.36	-0.00	22.85	-2.20	91.90	91.90	149.21	149.21
Piede	(4+5)-III-3 (+)	-212.68	-1.36	-0.00	-25.82	2.50	91.90	91.90	149.21	149.21
Piede	(4+5)-III-3 (-)	-212.68	-1.36	0.00	-25.82	0.00	91.90	91.90	149.21	149.21
Piede	(4+5)-VII-1 (+)	-212.68	-1.36	-0.00	83.31	-8.06	91.90	91.90	149.21	149.21
Piede	(4+5)-VII-1 (-)	-212.68	-1.36	0.00	83.31	0.00	91.90	91.90	149.21	149.21
Piede	(4+5)-I-3 (-)	-212.68	-1.36	0.00	-78.93	0.00	91.90	91.90	149.21	149.21
Piede	(4+5)-I-3 (+)	-212.68	-1.36	-0.00	-78.93	7.63	91.90	91.90	149.21	149.21
Piede	(4+5)-X-3 (-)	-212.68	-1.36	0.00	-83.31	0.00	91.90	91.90	149.21	149.21
Piede	(4+5)-X-3 (+)	-212.68	-1.36	-0.00	-83.31	8.06	91.90	91.90	149.21	149.21
Piede	(4+5)-IV-1 (+)	-212.68	-1.36	-0.00	78.94	-7.63	91.90	91.90	149.21	149.21
Piede	(4+5)-IV-1 (-)	-212.68	-1.36	0.00	78.94	0.00	91.90	91.90	149.21	149.21
Piede	(4+5)-XII-3 (+)	-212.68	-1.36	-0.00	-22.84	2.20	91.90	91.90	149.21	149.21
Piede	(4+5)-XII-3 (-)	-212.68	-1.36	0.00	-22.84	0.00	91.90	91.90	149.21	149.21
Piede	(4+5)-VI-1 (+)	-212.68	-1.36	-0.00	25.83	-2.50	91.90	91.90	149.21	149.21
Piede	(4+5)-VI-1 (-)	-212.68	-1.36	0.00	25.83	0.00	91.90	91.90	149.21	149.21
Piede	(4+5)-XII-1 (-)	-212.68	-1.36	0.00	28.98	0.00	91.90	91.90	149.21	149.21
Piede	(4+5)-XII-1 (+)	-212.68	-1.36	-0.00	28.98	-2.81	91.90	91.90	149.21	149.21
Piede	(4+5)-VI-3 (-)	-212.68	-1.36	0.00	-19.69	0.00	91.90	91.90	149.21	149.21
Piede	(4+5)-VI-3 (+)	-212.68	-1.36	-0.00	-19.69	1.89	91.90	91.90	149.21	149.21
Piede	(4+5)-IV-3 (+)	-212.68	-1.36	-0.00	-72.79	7.02	91.90	91.90	149.21	149.21
Piede	(4+5)-IV-3 (-)	-212.68	-1.36	0.00	-72.79	0.00	91.90	91.90	149.21	149.21
Piede	(4+5)-X-1 (+)	-212.68	-1.36	-0.00	89.45	-8.66	91.90	91.90	149.21	149.21
Piede	(4+5)-X-1 (-)	-212.68	-1.36	0.00	89.45	0.00	91.90	91.90	149.21	149.21
Piede	(4+5)-X-4 (-)	-204.76	13.45	0.00	-89.45	0.00	91.08	91.08	147.87	147.87
Piede	(4+5)-X-4 (+)	-204.76	13.45	-0.70	-89.45	8.66	91.08	91.08	147.87	147.87
Piede	(4+5)-IV-2 (+)	-204.76	13.44	-0.70	72.79	-7.02	91.08	91.08	147.87	147.87
Piede	(4+5)-IV-2 (-)	-204.76	13.44	0.00	72.79	0.00	91.08	91.08	147.87	147.87
Piede	(4+5)-VI-2 (+)	-204.76	13.45	-0.70	19.69	-1.89	91.08	91.08	147.87	147.87
Piede	(4+5)-VI-2 (-)	-204.76	13.45	0.00	19.69	0.00	91.08	91.08	147.87	147.87
Piede	(4+5)-XII-4 (-)	-204.76	13.45	0.00	-28.98	0.00	91.08	91.08	147.87	147.87
Piede	(4+5)-XII-4 (+)	-204.76	13.45	-0.70	-28.98	2.81	91.08	91.08	147.87	147.87
Piede	(4+5)-VI-4 (+)	-204.76	13.45	-0.70	-25.83	2.50	91.08	91.08	147.87	147.87
Piede	(4+5)-VI-4 (-)	-204.76	13.45	0.00	-25.83	0.00	91.08	91.08	147.87	147.87
Piede	(4+5)-XII-2 (+)	-204.76	13.45	-0.70	22.84	-2.20	91.08	91.08	147.87	147.87
Piede	(4+5)-XII-2 (-)	-204.76	13.45	0.00	22.84	0.00	91.08	91.08	147.87	147.87
Piede	(4+5)-IV-4 (+)	-204.76	13.45	-0.70	-78.94	7.63	91.08	91.08	147.87	147.87
Piede	(4+5)-IV-4 (-)	-204.76	13.45	0.00	-78.94	0.00	91.08	91.08	147.87	147.87
Piede	(4+5)-X-2 (-)	-204.76	13.45	0.00	83.31	0.00	91.08	91.08	147.87	147.87
Piede	(4+5)-X-2 (+)	-204.76	13.45	-0.70	83.31	-8.06	91.08	91.08	147.87	147.87
Piede	(4+5)-I-2 (+)	-204.75	13.45	-0.70	78.93	-7.63	91.08	91.08	147.87	147.87
Piede	(4+5)-I-2 (-)	-204.75	13.45	0.00	78.93	0.00	91.08	91.08	147.87	147.87
Piede	(4+5)-VII-4 (-)	-204.75	13.45	0.00	-83.31	0.00	91.08	91.08	147.87	147.87

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 82 di 103

Zona	C.	N	MyCal	ΔMy	MzCal	ΔMz	Mry+	Mry-	Mrz+	Mrz-
Piede	(4+5)-VII-4 (+)	-204.75	13.45	-0.70	-83.31	8.06	91.08	91.08	147.87	147.87
Piede	(4+5)-III-2 (-)	-204.75	13.45	0.00	25.82	0.00	91.08	91.08	147.87	147.87
Piede	(4+5)-III-2 (+)	-204.75	13.45	-0.70	25.82	-2.50	91.08	91.08	147.87	147.87
Piede	(4+5)-IX-4 (-)	-204.75	13.45	0.00	-22.85	0.00	91.08	91.08	147.87	147.87
Piede	(4+5)-IX-4 (+)	-204.75	13.45	-0.70	-22.85	2.20	91.08	91.08	147.87	147.87
Piede	(4+5)-IX-2 (-)	-204.75	13.45	0.00	28.98	0.00	91.08	91.08	147.87	147.87
Piede	(4+5)-IX-2 (+)	-204.75	13.45	-0.70	28.98	-2.81	91.08	91.08	147.87	147.87
Piede	(4+5)-III-4 (-)	-204.75	13.45	0.00	-19.69	0.00	91.08	91.08	147.87	147.87
Piede	(4+5)-III-4 (+)	-204.75	13.45	-0.70	-19.69	1.89	91.08	91.08	147.87	147.87
Piede	(4+5)-VII-2 (-)	-204.75	13.45	0.00	89.44	0.00	91.08	91.08	147.87	147.87
Piede	(4+5)-VII-2 (+)	-204.75	13.45	-0.70	89.44	-8.66	91.08	91.08	147.87	147.87
Piede	(4+5)-I-4 (+)	-204.75	13.45	-0.70	-72.80	7.02	91.08	91.08	147.87	147.87
Piede	(4+5)-I-4 (-)	-204.75	13.45	0.00	-72.80	0.00	91.08	91.08	147.87	147.87
Piede	(4+5)-V-2 (+)	-195.51	30.71	-1.51	12.52	-1.18	90.13	90.13	146.30	146.30
Piede	(4+5)-V-2 (-)	-195.51	30.71	0.00	12.52	0.00	90.13	90.13	146.30	146.30
Piede	(4+5)-XI-4 (+)	-195.51	30.71	-1.51	-36.15	3.52	90.13	90.13	146.30	146.30
Piede	(4+5)-XI-4 (-)	-195.51	30.71	0.00	-36.15	0.00	90.13	90.13	146.30	146.30
Piede	(4+5)-XI-2 (-)	-195.51	30.71	0.00	15.68	0.00	90.13	90.13	146.30	146.30
Piede	(4+5)-XI-2 (+)	-195.51	30.71	-1.51	15.68	-1.49	90.13	90.13	146.30	146.30
Piede	(4+5)-V-4 (+)	-195.51	30.71	-1.51	-33.00	3.21	90.13	90.13	146.30	146.30
Piede	(4+5)-V-4 (-)	-195.51	30.71	0.00	-33.00	0.00	90.13	90.13	146.30	146.30
Piede	(4+5)-VIII-4 (+)	-195.50	30.72	-1.51	-15.70	1.50	90.13	90.13	146.30	146.30
Piede	(4+5)-VIII-4 (-)	-195.50	30.72	0.00	-15.70	0.00	90.13	90.13	146.30	146.30
Piede	(4+5)-II-2 (-)	-195.50	30.72	0.00	32.97	0.00	90.13	90.13	146.30	146.30
Piede	(4+5)-II-2 (+)	-195.50	30.72	-1.51	32.97	-3.21	90.13	90.13	146.30	146.30
Piede	(4+5)-VIII-2 (-)	-195.50	30.72	0.00	36.13	0.00	90.13	90.13	146.30	146.30
Piede	(4+5)-VIII-2 (+)	-195.50	30.72	-1.51	36.13	-3.52	90.13	90.13	146.30	146.30
Piede	(4+5)-II-4 (+)	-195.50	30.72	-1.51	-12.54	1.19	90.13	90.13	146.30	146.30
Piede	(4+5)-II-4 (-)	-195.50	30.72	0.00	-12.54	0.00	90.13	90.13	146.30	146.30
Testa	2 (+)	-291.25	-9.82	0.00	-7.28	0.02	99.85	99.85	162.29	162.29
Testa	2 (-)	-291.25	-9.82	0.55	-7.28	-0.02	99.85	99.85	162.29	162.29
Testa	3 (+)	-286.81	-9.94	0.00	-7.17	0.02	99.40	99.40	161.56	161.56
Testa	3 (-)	-286.81	-9.94	0.55	-7.17	-0.02	99.40	99.40	161.56	161.56
Testa	1 (-)	-263.37	-8.60	0.49	-6.58	-0.02	97.05	97.05	157.69	157.69
Testa	1 (+)	-263.37	-8.60	0.00	-6.58	0.02	97.05	97.05	157.69	157.69
Testa	(4+5)-II-1 (+)	-206.94	9.82	0.00	-10.66	0.00	91.31	91.31	148.24	148.24
Testa	(4+5)-II-1 (-)	-206.94	9.82	-0.81	-10.66	1.19	91.31	91.31	148.24	148.24
Testa	(4+5)-VIII-3 (+)	-206.94	9.82	0.00	32.80	0.00	91.31	91.31	148.24	148.24
Testa	(4+5)-VIII-3 (-)	-206.94	9.82	-0.81	32.80	-3.52	91.31	91.31	148.24	148.24
Testa	(4+5)-II-3 (-)	-206.94	9.82	-0.81	29.88	-3.21	91.31	91.31	148.24	148.24
Testa	(4+5)-II-3 (+)	-206.94	9.82	0.00	29.88	0.00	91.31	91.31	148.24	148.24
Testa	(4+5)-VIII-1 (-)	-206.94	9.82	-0.81	-13.58	1.50	91.31	91.31	148.24	148.24
Testa	(4+5)-VIII-1 (+)	-206.94	9.82	0.00	-13.58	0.00	91.31	91.31	148.24	148.24
Testa	(4+5)-V-1 (+)	-206.93	9.81	0.00	-29.90	0.00	91.31	91.31	148.24	148.24
Testa	(4+5)-V-1 (-)	-206.93	9.81	-0.81	-29.90	3.21	91.31	91.31	148.24	148.24
Testa	(4+5)-XI-3 (+)	-206.93	9.81	0.00	13.56	0.00	91.31	91.31	148.24	148.24
Testa	(4+5)-XI-3 (-)	-206.93	9.81	-0.81	13.56	-1.49	91.31	91.31	148.24	148.24
Testa	(4+5)-XI-1 (-)	-206.93	9.81	-0.81	-32.82	3.52	91.31	91.31	148.24	148.24
Testa	(4+5)-XI-1 (+)	-206.93	9.81	0.00	-32.82	0.00	91.31	91.31	148.24	148.24
Testa	(4+5)-V-3 (-)	-206.93	9.81	-0.81	10.64	-1.18	91.31	91.31	148.24	148.24
Testa	(4+5)-V-3 (+)	-206.93	9.81	0.00	10.64	0.00	91.31	91.31	148.24	148.24
Testa	(4+5)-I-1 (-)	-197.68	-1.40	0.00	-64.68	7.02	90.36	90.36	146.67	146.67
Testa	(4+5)-I-1 (+)	-197.68	-1.40	0.00	-64.68	0.00	90.36	90.36	146.67	146.67
Testa	(4+5)-VII-3 (-)	-197.68	-1.40	0.00	80.19	-8.66	90.36	90.36	146.67	146.67
Testa	(4+5)-VII-3 (+)	-197.68	-1.40	0.00	80.19	0.00	90.36	90.36	146.67	146.67
Testa	(4+5)-III-1 (+)	-197.68	-1.40	0.00	-17.39	0.00	90.36	90.36	146.67	146.67
Testa	(4+5)-III-1 (-)	-197.68	-1.40	0.00	-17.39	1.89	90.36	90.36	146.67	146.67
Testa	(4+5)-IX-3 (-)	-197.68	-1.40	0.00	26.07	-2.81	90.36	90.36	146.67	146.67
Testa	(4+5)-IX-3 (+)	-197.68	-1.40	0.00	26.07	0.00	90.36	90.36	146.67	146.67
Testa	(4+5)-IX-1 (-)	-197.68	-1.40	0.00	-20.31	2.20	90.36	90.36	146.67	146.67
Testa	(4+5)-IX-1 (+)	-197.68	-1.40	0.00	-20.31	0.00	90.36	90.36	146.67	146.67
Testa	(4+5)-III-3 (+)	-197.68	-1.40	0.00	23.15	0.00	90.36	90.36	146.67	146.67
Testa	(4+5)-III-3 (-)	-197.68	-1.40	0.00	23.15	-2.50	90.36	90.36	146.67	146.67
Testa	(4+5)-VII-1 (+)	-197.68	-1.40	0.00	-74.42	0.00	90.36	90.36	146.67	146.67
Testa	(4+5)-VII-1 (-)	-197.68	-1.40	0.00	-74.42	8.06	90.36	90.36	146.67	146.67
Testa	(4+5)-I-3 (-)	-197.68	-1.40	0.00	70.45	-7.63	90.36	90.36	146.67	146.67
Testa	(4+5)-I-3 (+)	-197.68	-1.40	0.00	70.45	0.00	90.36	90.36	146.67	146.67
Testa	(4+5)-X-3 (-)	-197.68	-1.40	0.00	74.42	-8.06	90.36	90.36	146.67	146.67
Testa	(4+5)-X-3 (+)	-197.68	-1.40	0.00	74.42	0.00	90.36	90.36	146.67	146.67
Testa	(4+5)-IV-1 (+)	-197.68	-1.40	0.00	-70.45	0.00	90.36	90.36	146.67	146.67
Testa	(4+5)-IV-1 (-)	-197.68	-1.40	0.00	-70.45	7.63	90.36	90.36	146.67	146.67
Testa	(4+5)-XII-3 (+)	-197.68	-1.40	0.00	20.30	0.00	90.36	90.36	146.67	146.67
Testa	(4+5)-XII-3 (-)	-197.68	-1.40	0.00	20.30	-2.20	90.36	90.36	146.67	146.67
Testa	(4+5)-VI-1 (+)	-197.68	-1.40	0.00	-23.16	0.00	90.36	90.36	146.67	146.67
Testa	(4+5)-VI-1 (-)	-197.68	-1.40	0.00	-23.16	2.50	90.36	90.36	146.67	146.67
Testa	(4+5)-XII-1 (-)	-197.68	-1.40	0.00	-26.08	2.81	90.36	90.36	146.67	146.67

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021
Pagina 83 di 103

Zona	C.	N	MyCal	ΔMy	MzCal	ΔMz	Mry+	Mry-	Mrz+	Mrz-
Testa	(4+5)-XII-1 (+)	-197.68	-1.40	0.00	-26.08	0.00	90.36	90.36	146.67	146.67
Testa	(4+5)-VI-3 (-)	-197.68	-1.40	0.00	17.38	-1.89	90.36	90.36	146.67	146.67
Testa	(4+5)-VI-3 (+)	-197.68	-1.40	0.00	17.38	0.00	90.36	90.36	146.67	146.67
Testa	(4+5)-IV-3 (+)	-197.68	-1.40	0.00	64.68	0.00	90.36	90.36	146.67	146.67
Testa	(4+5)-IV-3 (-)	-197.68	-1.40	0.00	64.68	-7.02	90.36	90.36	146.67	146.67
Testa	(4+5)-X-1 (+)	-197.68	-1.40	0.00	-80.19	0.00	90.36	90.36	146.67	146.67
Testa	(4+5)-X-1 (-)	-197.68	-1.40	0.00	-80.19	8.66	90.36	90.36	146.67	146.67
Testa	(4+5)-X-4 (-)	-189.76	-11.01	0.70	80.19	-8.66	89.54	89.54	145.32	145.32
Testa	(4+5)-X-4 (+)	-189.76	-11.01	0.00	80.19	0.00	89.54	89.54	145.32	145.32
Testa	(4+5)-IV-2 (+)	-189.76	-11.01	0.00	-64.68	0.00	89.54	89.54	145.32	145.32
Testa	(4+5)-IV-2 (-)	-189.76	-11.01	0.70	-64.68	7.02	89.54	89.54	145.32	145.32
Testa	(4+5)-VI-2 (+)	-189.76	-11.01	0.00	-17.38	0.00	89.54	89.54	145.32	145.32
Testa	(4+5)-VI-2 (-)	-189.76	-11.01	0.70	-17.38	1.89	89.54	89.54	145.32	145.32
Testa	(4+5)-XII-4 (-)	-189.76	-11.01	0.70	26.08	-2.81	89.54	89.54	145.32	145.32
Testa	(4+5)-XII-4 (+)	-189.76	-11.01	0.00	26.08	0.00	89.54	89.54	145.32	145.32
Testa	(4+5)-VI-4 (+)	-189.76	-11.01	0.00	23.16	0.00	89.54	89.54	145.32	145.32
Testa	(4+5)-VI-4 (-)	-189.76	-11.01	0.70	23.16	-2.50	89.54	89.54	145.32	145.32
Testa	(4+5)-XII-2 (+)	-189.76	-11.01	0.00	-20.30	0.00	89.54	89.54	145.32	145.32
Testa	(4+5)-XII-2 (-)	-189.76	-11.01	0.70	-20.30	2.20	89.54	89.54	145.32	145.32
Testa	(4+5)-IV-4 (+)	-189.76	-11.01	0.00	70.45	0.00	89.54	89.54	145.32	145.32
Testa	(4+5)-IV-4 (-)	-189.76	-11.01	0.70	70.45	-7.63	89.54	89.54	145.32	145.32
Testa	(4+5)-X-2 (-)	-189.76	-11.01	0.70	-74.42	8.06	89.54	89.54	145.32	145.32
Testa	(4+5)-X-2 (+)	-189.76	-11.01	0.00	-74.42	0.00	89.54	89.54	145.32	145.32
Testa	(4+5)-I-2 (+)	-189.75	-11.01	0.00	-70.45	0.00	89.54	89.54	145.32	145.32
Testa	(4+5)-I-2 (-)	-189.75	-11.01	0.70	-70.45	7.63	89.54	89.54	145.32	145.32
Testa	(4+5)-VII-4 (-)	-189.75	-11.01	0.70	74.42	-8.06	89.54	89.54	145.32	145.32
Testa	(4+5)-VII-4 (+)	-189.75	-11.01	0.00	74.42	0.00	89.54	89.54	145.32	145.32
Testa	(4+5)-III-2 (-)	-189.75	-11.01	0.70	-23.15	2.50	89.54	89.54	145.32	145.32
Testa	(4+5)-III-2 (+)	-189.75	-11.01	0.00	-23.15	0.00	89.54	89.54	145.32	145.32
Testa	(4+5)-IX-4 (-)	-189.75	-11.01	0.70	20.31	-2.20	89.54	89.54	145.32	145.32
Testa	(4+5)-IX-4 (+)	-189.75	-11.01	0.00	20.31	0.00	89.54	89.54	145.32	145.32
Testa	(4+5)-IX-2 (-)	-189.75	-11.01	0.70	-26.07	2.81	89.54	89.54	145.32	145.32
Testa	(4+5)-IX-2 (+)	-189.75	-11.01	0.00	-26.07	0.00	89.54	89.54	145.32	145.32
Testa	(4+5)-III-4 (-)	-189.75	-11.01	0.70	17.39	-1.89	89.54	89.54	145.32	145.32
Testa	(4+5)-III-4 (+)	-189.75	-11.01	0.00	17.39	0.00	89.54	89.54	145.32	145.32
Testa	(4+5)-VII-2 (-)	-189.75	-11.01	0.70	-80.19	8.66	89.54	89.54	145.32	145.32
Testa	(4+5)-VII-2 (+)	-189.75	-11.01	0.00	-80.19	0.00	89.54	89.54	145.32	145.32
Testa	(4+5)-I-4 (+)	-189.75	-11.01	0.00	64.68	0.00	89.54	89.54	145.32	145.32
Testa	(4+5)-I-4 (-)	-189.75	-11.01	0.70	64.68	-7.02	89.54	89.54	145.32	145.32
Testa	(4+5)-V-2 (+)	-180.51	-22.22	0.00	-10.64	0.00	88.58	88.58	143.75	143.75
Testa	(4+5)-V-2 (-)	-180.51	-22.22	1.51	-10.64	1.18	88.58	88.58	143.75	143.75
Testa	(4+5)-XI-4 (+)	-180.51	-22.22	0.00	32.82	0.00	88.58	88.58	143.75	143.75
Testa	(4+5)-XI-4 (-)	-180.51	-22.22	1.51	32.82	-3.52	88.58	88.58	143.75	143.75
Testa	(4+5)-XI-2 (-)	-180.51	-22.22	1.51	-13.56	1.49	88.58	88.58	143.75	143.75
Testa	(4+5)-XI-2 (+)	-180.51	-22.22	0.00	-13.56	0.00	88.58	88.58	143.75	143.75
Testa	(4+5)-V-4 (+)	-180.51	-22.22	0.00	29.90	0.00	88.58	88.58	143.75	143.75
Testa	(4+5)-V-4 (-)	-180.51	-22.22	1.51	29.90	-3.21	88.58	88.58	143.75	143.75
Testa	(4+5)-VIII-4 (+)	-180.50	-22.23	0.00	13.58	0.00	88.58	88.58	143.74	143.74
Testa	(4+5)-VIII-4 (-)	-180.50	-22.23	1.51	13.58	-1.50	88.58	88.58	143.74	143.74
Testa	(4+5)-II-2 (-)	-180.50	-22.23	1.51	-29.88	3.21	88.58	88.58	143.74	143.74
Testa	(4+5)-II-2 (+)	-180.50	-22.23	0.00	-29.88	0.00	88.58	88.58	143.74	143.74
Testa	(4+5)-VIII-2 (-)	-180.50	-22.23	1.51	-32.80	3.52	88.58	88.58	143.74	143.74
Testa	(4+5)-VIII-2 (+)	-180.50	-22.23	0.00	-32.80	0.00	88.58	88.58	143.74	143.74
Testa	(4+5)-II-4 (+)	-180.50	-22.23	0.00	10.66	0.00	88.58	88.58	143.74	143.74
Testa	(4+5)-II-4 (-)	-180.50	-22.23	1.51	10.66	-1.19	88.58	88.58	143.74	143.74

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot (θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(4+5)-X-1	--	--	42.41	--	477.28	373.73	373.73	9.35	2.500	8.8
Z	(4+5)-II-4	--	--	13.24	--	442.78	209.09	209.09	9.35	2.500	16

Pilastro: 6 [6,106] Sez. R: By=30.00 cm Bz=50.00 cm L=400.00 cm Ln=400.00 cm Criterio: CLS_Pilastri_ND - Verifica a presso-flessione deviata, $\zeta_E=1.320$ [(4+5)-VIII-2] : **Verificato**

Piede	AfSpigolo = 3.14	Afy = 0.00	Afz = 1.54
Testa	AfSpigolo = 3.14	Afy = 0.00	Afz = 1.54

$V_{max}=N/(fcd*A)=0.043 \leq 0.65$ [Comb. (4+5)-II-1(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	2 (+)	-158.93	9.08	2.10	140.04	86.33	140.04	86.33	17
Piede	2 (-)	-158.93	9.64	3.18	140.04	86.33	140.04	86.33	17

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 84 di 103

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
Piede	3(+)	-158.29	9.03	2.09	139.93	86.26	139.93	86.26	18
Piede	3(-)	-158.29	9.57	3.17	139.93	86.26	139.93	86.26	17
Piede	1(-)	-147.16	8.73	-2.95	138.01	85.09	138.01	85.09	18
Piede	1(+)	-147.16	8.25	-2.93	138.01	85.09	138.01	85.09	19
Piede	(4+5)-II-1(+)	-137.38	-64.58	0.21	136.31	84.06	136.31	84.06	2.7
Piede	(4+5)-II-1(-)	-137.38	-71.47	0.39	136.31	84.06	136.31	84.06	2.3
Piede	(4+5)-VIII-1(-)	-136.62	-66.16	1.69	136.18	83.98	136.18	83.98	2.6
Piede	(4+5)-VIII-1(+)	-136.62	-59.77	1.44	136.18	83.98	136.18	83.98	3.0
Piede	(4+5)-V-1(+)	-131.27	-42.29	5.76	135.24	83.41	135.24	83.41	4.6
Piede	(4+5)-V-1(-)	-131.27	-46.87	6.27	135.24	83.41	135.24	83.41	3.9
Piede	(4+5)-I-1(-)	-131.03	-23.37	26.08	135.20	83.39	135.20	83.39	3.5
Piede	(4+5)-I-1(+)	-131.03	-20.95	24.46	135.20	83.39	135.20	83.39	3.9
Piede	(4+5)-XI-1(-)	-130.51	-41.56	7.58	135.11	83.33	135.11	83.33	4.4
Piede	(4+5)-XI-1(+)	-130.51	-37.49	6.99	135.11	83.33	135.11	83.33	5.2
Piede	(4+5)-VIII-3(-)	-129.58	-72.54	-18.13	134.95	83.23	134.95	83.23	1.8
Piede	(4+5)-VIII-3(+)	-129.58	-65.54	-17.27	134.95	83.23	134.95	83.23	2.0
Piede	(4+5)-IV-1(-)	-129.20	-15.99	27.84	134.88	83.19	134.88	83.19	3.6
Piede	(4+5)-IV-1(+)	-129.20	-14.26	26.12	134.88	83.19	134.88	83.19	4.1
Piede	(4+5)-II-3(-)	-128.82	-67.23	-16.82	134.82	83.15	134.82	83.15	2.0
Piede	(4+5)-II-3(+)	-128.82	-60.73	-16.04	134.82	83.15	134.82	83.15	2.2
Piede	(4+5)-VIII-1(-)	-128.50	-5.68	30.43	134.76	83.12	134.76	83.12	3.7
Piede	(4+5)-VII-1(+)	-128.50	-4.92	28.57	134.76	83.12	134.76	83.12	4.2
Piede	(4+5)-X-1(-)	-126.67	1.70	32.19	134.44	82.93	134.44	82.93	3.6
Piede	(4+5)-X-1(+)	-126.67	1.76	30.23	134.44	82.93	134.44	82.93	4.0
Piede	(4+5)-XI-3(+)	-123.47	-43.25	-11.72	133.88	82.59	133.88	82.59	3.6
Piede	(4+5)-XI-3(-)	-123.47	-47.93	-12.24	133.88	82.59	133.88	82.59	3.1
Piede	(4+5)-V-3(+)	-122.71	-38.45	-10.49	133.75	82.51	133.75	82.51	4.3
Piede	(4+5)-V-3(-)	-122.71	-42.62	-10.94	133.75	82.51	133.75	82.51	3.7
Piede	(4+5)-III-1(-)	-121.04	-18.42	6.00	133.46	82.33	133.46	82.33	12
Piede	(4+5)-III-1(+)	-121.04	-16.46	5.50	133.46	82.33	133.46	82.33	13
Piede	(4+5)-IX-1(-)	-120.29	-13.11	7.31	133.32	82.25	133.32	82.25	14
Piede	(4+5)-IX-1(+)	-120.29	-11.65	6.74	133.32	82.25	133.32	82.25	15
Piede	(4+5)-VI-1(-)	-119.21	-11.04	7.77	133.14	82.13	133.14	82.13	14
Piede	(4+5)-VI-1(+)	-119.21	-9.77	7.17	133.14	82.13	133.14	82.13	15
Piede	(4+5)-IV-2(+)	-118.86	13.62	27.33	133.08	82.10	133.08	82.10	3.7
Piede	(4+5)-IV-2(-)	-118.86	14.72	29.12	133.08	82.10	133.08	82.10	3.3
Piede	(4+5)-XII-1(+)	-118.45	-4.97	8.40	133.00	82.05	133.00	82.05	16
Piede	(4+5)-XII-1(-)	-118.45	-5.73	9.07	133.00	82.05	133.00	82.05	15
Piede	(4+5)-I-2(-)	-117.03	22.10	30.89	132.75	81.90	132.75	81.90	2.8
Piede	(4+5)-I-2(+)	-117.03	20.30	29.00	132.75	81.90	132.75	81.90	3.1
Piede	(4+5)-X-2(+)	-116.33	29.64	31.44	132.63	81.83	132.63	81.83	2.5
Piede	(4+5)-X-2(-)	-116.33	32.41	33.48	132.63	81.83	132.63	81.83	2.2
Piede	(4+5)-VII-2(-)	-114.50	39.79	35.24	132.31	81.63	132.31	81.63	1.9
Piede	(4+5)-VII-2(+)	-114.50	36.32	33.11	132.31	81.63	132.31	81.63	2.1
Piede	(4+5)-IX-3(-)	-113.25	-19.49	-12.51	132.09	81.50	132.09	81.50	7.6
Piede	(4+5)-IX-3(+)	-113.25	-17.42	-11.97	132.09	81.50	132.09	81.50	8.5
Piede	(4+5)-III-3(+)	-112.49	-12.61	-10.74	131.96	81.42	131.96	81.42	11
Piede	(4+5)-III-3(-)	-112.49	-14.18	-11.21	131.96	81.42	131.96	81.42	10
Piede	(4+5)-XII-3(+)	-111.41	-10.73	-10.31	131.77	81.30	131.77	81.30	12
Piede	(4+5)-XII-3(-)	-111.41	-12.10	-10.75	131.77	81.30	131.77	81.30	11
Piede	(4+5)-VI-3(-)	-110.65	-6.80	-9.44	131.64	81.22	131.64	81.22	15
Piede	(4+5)-VI-3(+)	-110.65	-5.92	-9.08	131.64	81.22	131.64	81.22	16
Piede	(4+5)-VI-2(-)	-108.88	19.67	9.05	131.32	81.03	131.32	81.03	9.2
Piede	(4+5)-VI-2(+)	-108.88	18.10	8.38	131.32	81.03	131.32	81.03	10
Piede	(4+5)-XII-2(-)	-108.12	24.98	10.35	131.19	80.95	131.19	80.95	6.7
Piede	(4+5)-XII-2(+)	-108.12	22.91	9.61	131.19	80.95	131.19	80.95	7.7
Piede	(4+5)-III-2(+)	-107.04	24.79	10.05	131.00	80.84	131.00	80.84	6.8
Piede	(4+5)-III-2(-)	-107.04	27.05	10.81	131.00	80.84	131.00	80.84	6.0
Piede	(4+5)-IX-2(-)	-106.28	32.36	12.12	130.87	80.76	130.87	80.76	4.6
Piede	(4+5)-IX-2(+)	-106.28	29.60	11.28	130.87	80.76	130.87	80.76	5.3
Piede	(4+5)-VII-3(-)	-105.03	-26.92	-35.63	130.65	80.62	130.65	80.62	2.1
Piede	(4+5)-VII-3(+)	-105.03	-24.14	-33.80	130.65	80.62	130.65	80.62	2.3
Piede	(4+5)-X-3(-)	-103.20	-19.54	-33.87	130.32	80.43	130.32	80.43	2.5
Piede	(4+5)-X-3(+)	-103.20	-17.46	-32.14	130.32	80.43	130.32	80.43	2.7
Piede	(4+5)-I-3(-)	-102.50	-9.23	-31.28	130.20	80.35	130.20	80.35	3.1
Piede	(4+5)-I-3(+)	-102.50	-8.12	-29.70	130.20	80.35	130.20	80.35	3.3
Piede	(4+5)-XII-4(-)	-101.08	18.60	-9.46	129.95	80.20	129.95	80.20	9.1
Piede	(4+5)-XII-4(+)	-101.08	17.15	-9.10	129.95	80.20	129.95	80.20	9.9
Piede	(4+5)-IV-3(-)	-100.67	-1.84	-29.52	129.88	80.16	129.88	80.16	3.6
Piede	(4+5)-IV-3(+)	-100.67	-1.44	-28.03	129.88	80.16	129.88	80.16	3.9
Piede	(4+5)-VI-4(+)	-100.32	21.95	-7.87	129.82	80.12	129.82	80.12	8.6
Piede	(4+5)-VI-4(-)	-100.32	23.91	-8.16	129.82	80.12	129.82	80.12	7.6
Piede	(4+5)-IX-4(+)	-99.24	23.83	-7.43	129.63	80.00	129.63	80.00	7.9
Piede	(4+5)-IX-4(-)	-99.24	25.99	-7.70	129.63	80.00	129.63	80.00	7.0
Piede	(4+5)-III-4(+)	-98.48	28.64	-6.20	129.49	79.92	129.49	79.92	6.5
Piede	(4+5)-III-4(-)	-98.48	31.29	-6.39	129.49	79.92	129.49	79.92	5.7

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 85 di 103

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
Piede	(4+5)-V-2 (-)	-96.82	55.50	10.54	129.20	79.74	129.20	79.74	2.5
Piede	(4+5)-V-2 (+)	-96.82	50.63	9.79	129.20	79.74	129.20	79.74	2.8
Piede	(4+5)-XI-2 (+)	-96.06	55.43	11.02	129.06	79.66	129.06	79.66	2.4
Piede	(4+5)-XI-2 (-)	-96.06	60.80	11.85	129.06	79.66	129.06	79.66	2.2
Piede	(4+5)-X-4 (+)	-92.86	10.42	-30.93	128.50	79.32	128.50	79.32	2.9
Piede	(4+5)-X-4 (-)	-92.86	11.17	-32.59	128.50	79.32	128.50	79.32	2.7
Piede	(4+5)-VII-4 (+)	-91.03	17.10	-29.26	128.17	79.12	128.17	79.12	2.8
Piede	(4+5)-VII-4 (-)	-91.03	18.55	-30.82	128.17	79.12	128.17	79.12	2.6
Piede	(4+5)-II-2 (-)	-90.71	80.10	16.43	128.12	79.09	128.12	79.09	1.5
Piede	(4+5)-II-2 (+)	-90.71	72.91	15.35	128.12	79.09	128.12	79.09	1.7
Piede	(4+5)-IV-4 (-)	-90.33	28.86	-28.23	128.05	79.05	128.05	79.05	2.5
Piede	(4+5)-IV-4 (+)	-90.33	26.44	-26.82	128.05	79.05	128.05	79.05	2.7
Piede	(4+5)-VIII-2 (-)	-89.95	85.41	17.73	127.98	79.01	127.98	79.01	1.4
Piede	(4+5)-VIII-2 (+)	-89.95	77.72	16.58	127.98	79.01	127.98	79.01	1.5
Piede	(4+5)-XI-4 (+)	-89.02	49.67	-7.69	127.82	78.91	127.82	78.91	2.9
Piede	(4+5)-XI-4 (-)	-89.02	54.43	-7.97	127.82	78.91	127.82	78.91	2.6
Piede	(4+5)-I-4 (+)	-88.50	33.13	-25.15	127.73	78.85	127.73	78.85	2.6
Piede	(4+5)-I-4 (-)	-88.50	36.25	-26.47	127.73	78.85	127.73	78.85	2.4
Piede	(4+5)-V-4 (+)	-88.26	54.47	-6.46	127.68	78.82	127.68	78.82	2.6
Piede	(4+5)-V-4 (-)	-88.26	59.74	-6.66	127.68	78.82	127.68	78.82	2.3
Piede	(4+5)-VIII-4 (+)	-82.91	71.95	-2.13	126.73	78.25	126.73	78.25	1.9
Piede	(4+5)-VIII-4 (-)	-82.91	79.04	-2.08	126.73	78.25	126.73	78.25	1.7
Piede	(4+5)-II-4 (-)	-82.15	84.34	-0.78	126.60	78.17	126.60	78.17	1.6
Piede	(4+5)-II-4 (+)	-82.15	76.76	-0.90	126.60	78.17	126.60	78.17	1.8
Testa	2 (+)	-139.43	-3.49	-9.03	136.66	84.28	136.66	84.28	15
Testa	2 (-)	-139.43	-1.32	-8.76	136.66	84.28	136.66	84.28	16
Testa	3 (+)	-138.79	-3.47	-8.62	136.55	84.21	136.55	84.21	16
Testa	3 (-)	-138.79	-1.32	-8.37	136.55	84.21	136.55	84.21	17
Testa	1 (-)	-127.66	-1.21	-7.38	134.61	83.03	134.61	83.03	18
Testa	1 (+)	-127.66	-3.19	-7.59	134.61	83.03	134.61	83.03	18
Testa	(4+5)-II-1 (+)	-122.38	63.46	-5.96	133.69	82.47	133.69	82.47	2.5
Testa	(4+5)-II-1 (-)	-122.38	56.57	-5.78	133.69	82.47	133.69	82.47	2.9
Testa	(4+5)-VIII-1 (-)	-121.62	52.56	-6.98	133.56	82.39	133.56	82.39	3.1
Testa	(4+5)-VIII-1 (+)	-121.62	58.95	-7.23	133.56	82.39	133.56	82.39	2.6
Testa	(4+5)-V-1 (+)	-116.27	42.66	-11.64	132.62	81.82	132.62	81.82	3.5
Testa	(4+5)-V-1 (-)	-116.27	38.09	-11.13	132.62	81.82	132.62	81.82	4.1
Testa	(4+5)-I-1 (-)	-116.03	21.73	-28.92	132.58	81.80	132.58	81.80	3.0
Testa	(4+5)-I-1 (+)	-116.03	24.16	-30.54	132.58	81.80	132.58	81.80	2.7
Testa	(4+5)-XI-1 (-)	-115.51	34.07	-12.33	132.49	81.74	132.49	81.74	4.5
Testa	(4+5)-XI-1 (+)	-115.51	38.14	-12.92	132.49	81.74	132.49	81.74	3.9
Testa	(4+5)-VIII-3 (-)	-114.58	57.45	10.87	132.32	81.64	132.32	81.64	2.5
Testa	(4+5)-VIII-3 (+)	-114.58	64.44	11.73	132.32	81.64	132.32	81.64	2.1
Testa	(4+5)-IV-1 (-)	-114.20	16.18	-30.53	132.26	81.60	132.26	81.60	3.0
Testa	(4+5)-IV-1 (+)	-114.20	17.91	-32.24	132.26	81.60	132.26	81.60	2.8
Testa	(4+5)-II-3 (-)	-113.82	53.43	9.68	132.19	81.56	132.19	81.56	2.8
Testa	(4+5)-II-3 (+)	-113.82	59.93	10.46	132.19	81.56	132.19	81.56	2.4
Testa	(4+5)-VII-1 (-)	-113.50	8.35	-32.92	132.14	81.53	132.14	81.53	3.0
Testa	(4+5)-VII-1 (+)	-113.50	9.10	-34.78	132.14	81.53	132.14	81.53	2.8
Testa	(4+5)-X-1 (-)	-111.67	2.80	-34.52	131.81	81.33	131.81	81.33	3.0
Testa	(4+5)-X-1 (+)	-111.67	2.86	-36.48	131.81	81.33	131.81	81.33	2.8
Testa	(4+5)-XI-3 (+)	-108.47	43.64	6.05	131.25	80.99	131.25	80.99	3.9
Testa	(4+5)-XI-3 (-)	-108.47	38.96	5.52	131.25	80.99	131.25	80.99	4.6
Testa	(4+5)-V-3 (+)	-107.71	39.12	4.77	131.12	80.91	131.12	80.91	4.6
Testa	(4+5)-V-3 (-)	-107.71	34.95	4.33	131.12	80.91	131.12	80.91	5.6
Testa	(4+5)-III-1 (-)	-106.04	18.07	-10.89	130.82	80.73	130.82	80.73	8.6
Testa	(4+5)-III-1 (+)	-106.04	20.03	-11.39	130.82	80.73	130.82	80.73	7.7
Testa	(4+5)-IX-1 (-)	-105.29	14.05	-12.09	130.69	80.65	130.69	80.65	9.3
Testa	(4+5)-IX-1 (+)	-105.29	15.52	-12.66	130.69	80.65	130.69	80.65	8.4
Testa	(4+5)-VI-1 (-)	-104.21	12.52	-12.49	130.50	80.54	130.50	80.54	9.4
Testa	(4+5)-VI-1 (+)	-104.21	13.79	-13.09	130.50	80.54	130.50	80.54	8.6
Testa	(4+5)-IV-2 (+)	-103.86	-6.83	-33.48	130.44	80.50	130.44	80.50	2.9
Testa	(4+5)-IV-2 (-)	-103.86	-5.73	-31.70	130.44	80.50	130.44	80.50	3.2
Testa	(4+5)-XII-1 (+)	-103.45	9.28	-14.36	130.37	80.45	130.37	80.45	9.1
Testa	(4+5)-XII-1 (-)	-103.45	8.51	-13.69	130.37	80.45	130.37	80.45	9.9
Testa	(4+5)-I-2 (-)	-102.03	-11.27	-33.30	130.12	80.30	130.12	80.30	2.8
Testa	(4+5)-I-2 (+)	-102.03	-13.07	-35.19	130.12	80.30	130.12	80.30	2.5
Testa	(4+5)-X-2 (+)	-101.33	-21.88	-37.72	129.99	80.23	129.99	80.23	2.1
Testa	(4+5)-X-2 (-)	-101.33	-19.11	-35.69	129.99	80.23	129.99	80.23	2.3
Testa	(4+5)-VII-2 (-)	-99.50	-24.65	-37.30	129.67	80.03	129.67	80.03	2.1
Testa	(4+5)-VII-2 (+)	-99.50	-28.12	-39.43	129.67	80.03	129.67	80.03	1.9
Testa	(4+5)-IX-3 (-)	-98.25	18.94	5.77	129.45	79.90	129.45	79.90	11
Testa	(4+5)-IX-3 (+)	-98.25	21.01	6.30	129.45	79.90	129.45	79.90	9.8
Testa	(4+5)-III-3 (+)	-97.49	16.50	5.03	129.32	79.82	129.32	79.82	14
Testa	(4+5)-III-3 (-)	-97.49	14.93	4.57	129.32	79.82	129.32	79.82	15
Testa	(4+5)-XII-3 (+)	-96.41	14.77	4.60	129.13	79.70	129.13	79.70	15
Testa	(4+5)-XII-3 (-)	-96.41	13.40	4.16	129.13	79.70	129.13	79.70	17

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 86 di 103

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
Testa	(4+5)-VI-3 (-)	-95.65	9.39	2.96	128.99	79.62	128.99	79.62	22
Testa	(4+5)-VI-3 (+)	-95.65	10.26	3.33	128.99	79.62	128.99	79.62	20
Testa	(4+5)-VI-2 (-)	-93.88	-9.39	-13.66	128.68	79.43	128.68	79.43	9.0
Testa	(4+5)-VI-2 (+)	-93.88	-10.95	-14.33	128.68	79.43	128.68	79.43	8.0
Testa	(4+5)-VII-2 (-)	-93.12	-13.40	-14.86	128.54	79.35	128.54	79.35	7.0
Testa	(4+5)-VII-2 (+)	-93.12	-15.47	-15.60	128.54	79.35	128.54	79.35	6.2
Testa	(4+5)-III-2 (+)	-92.04	-17.19	-16.03	128.35	79.23	128.35	79.23	5.7
Testa	(4+5)-III-2 (-)	-92.04	-14.93	-15.27	128.35	79.23	128.35	79.23	6.4
Testa	(4+5)-IX-2 (-)	-91.28	-18.95	-16.47	128.22	79.15	128.22	79.15	5.2
Testa	(4+5)-IX-2 (+)	-91.28	-21.71	-17.31	128.22	79.15	128.22	79.15	4.6
Testa	(4+5)-VII-3 (-)	-90.03	24.65	26.60	128.00	79.01	128.00	79.01	2.8
Testa	(4+5)-VII-3 (+)	-90.03	27.42	28.43	128.00	79.01	128.00	79.01	2.5
Testa	(4+5)-X-3 (-)	-88.20	19.10	24.99	127.67	78.82	127.67	78.82	3.2
Testa	(4+5)-X-3 (+)	-88.20	21.18	26.72	127.67	78.82	127.67	78.82	2.9
Testa	(4+5)-I-3 (-)	-87.50	11.27	22.60	127.55	78.74	127.55	78.74	4.2
Testa	(4+5)-I-3 (+)	-87.50	12.37	24.19	127.55	78.74	127.55	78.74	3.8
Testa	(4+5)-XII-4 (-)	-86.08	-8.51	2.99	127.30	78.59	127.30	78.59	24
Testa	(4+5)-XII-4 (+)	-86.08	-9.97	3.36	127.30	78.59	127.30	78.59	21
Testa	(4+5)-IV-3 (-)	-85.67	5.72	21.00	127.22	78.55	127.22	78.55	5.1
Testa	(4+5)-IV-3 (+)	-85.67	6.13	22.48	127.22	78.55	127.22	78.55	4.6
Testa	(4+5)-VII-4 (+)	-85.32	-14.49	2.09	127.16	78.51	127.16	78.51	18
Testa	(4+5)-VI-4 (-)	-85.32	-12.53	1.80	127.16	78.51	127.16	78.51	21
Testa	(4+5)-IX-4 (+)	-84.24	-16.21	1.66	126.97	78.39	126.97	78.39	17
Testa	(4+5)-IX-4 (-)	-84.24	-14.06	1.39	126.97	78.39	126.97	78.39	19
Testa	(4+5)-III-4 (+)	-83.48	-20.73	0.38	126.84	78.31	126.84	78.31	13
Testa	(4+5)-III-4 (-)	-83.48	-18.07	0.19	126.84	78.31	126.84	78.31	16
Testa	(4+5)-V-2 (-)	-81.82	-34.95	-15.02	126.54	78.13	126.54	78.13	3.4
Testa	(4+5)-V-2 (+)	-81.82	-39.82	-15.78	126.54	78.13	126.54	78.13	2.9
Testa	(4+5)-XI-2 (+)	-81.06	-44.34	-17.05	126.41	78.05	126.41	78.05	2.6
Testa	(4+5)-XI-2 (-)	-81.06	-38.97	-16.22	126.41	78.05	126.41	78.05	2.9
Testa	(4+5)-X-4 (+)	-77.86	-3.56	25.48	125.84	77.70	125.84	77.70	3.9
Testa	(4+5)-X-4 (-)	-77.86	-2.81	23.82	125.84	77.70	125.84	77.70	4.3
Testa	(4+5)-VII-4 (+)	-76.03	-9.80	23.78	125.51	77.51	125.51	77.51	3.8
Testa	(4+5)-VII-4 (-)	-76.03	-8.35	22.22	125.51	77.51	125.51	77.51	4.3
Testa	(4+5)-II-2 (-)	-75.71	-53.44	-20.37	125.45	77.47	125.45	77.47	2.0
Testa	(4+5)-II-2 (+)	-75.71	-60.62	-21.46	125.45	77.47	125.45	77.47	1.7
Testa	(4+5)-IV-4 (-)	-75.33	-16.19	19.83	125.39	77.43	125.39	77.43	4.1
Testa	(4+5)-IV-4 (+)	-75.33	-18.61	21.24	125.39	77.43	125.39	77.43	3.7
Testa	(4+5)-VIII-2 (-)	-74.95	-57.45	-21.57	125.32	77.39	125.32	77.39	1.8
Testa	(4+5)-VIII-2 (+)	-74.95	-65.14	-22.73	125.32	77.39	125.32	77.39	1.6
Testa	(4+5)-VII-1 (+)	-74.02	-38.84	1.91	125.15	77.29	125.15	77.29	4.2
Testa	(4+5)-XI-4 (-)	-74.02	-34.08	1.63	125.15	77.29	125.15	77.29	5.1
Testa	(4+5)-I-4 (+)	-73.50	-24.85	19.54	125.06	77.23	125.06	77.23	3.5
Testa	(4+5)-I-4 (-)	-73.50	-21.73	18.22	125.06	77.23	125.06	77.23	3.9
Testa	(4+5)-V-4 (+)	-73.26	-43.36	0.64	125.02	77.21	125.02	77.21	3.6
Testa	(4+5)-V-4 (-)	-73.26	-38.09	0.43	125.02	77.21	125.02	77.21	4.4
Testa	(4+5)-VIII-4 (+)	-67.91	-59.64	-3.77	124.06	76.63	124.06	76.63	2.3
Testa	(4+5)-VIII-4 (-)	-67.91	-52.56	-3.72	124.06	76.63	124.06	76.63	2.6
Testa	(4+5)-II-4 (-)	-67.15	-56.57	-4.92	123.93	76.54	123.93	76.54	2.4
Testa	(4+5)-II-4 (+)	-67.15	-64.16	-5.04	123.93	76.54	123.93	76.54	2.0

Zona	C.	N	MyCal	ΔMy	MzCal	ΔMz	Mry+	Mry-	Mrz+	Mrz-
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m
Piede	2 (+)	-158.93	9.64	-0.55	3.18	-1.08	140.04	140.04	86.33	86.33
Piede	2 (-)	-158.93	9.64	0.00	3.18	0.00	140.04	140.04	86.33	86.33
Piede	3 (+)	-158.29	9.57	-0.55	3.17	-1.07	139.93	139.93	86.26	86.26
Piede	3 (-)	-158.29	9.57	0.00	3.17	0.00	139.93	139.93	86.26	86.26
Piede	1 (-)	-147.16	8.73	0.00	-2.94	-0.01	138.01	138.01	85.09	85.09
Piede	1 (+)	-147.16	8.73	-0.48	-2.94	0.01	138.01	138.01	85.09	85.09
Piede	(4+5)-II-1 (+)	-137.38	-71.47	6.89	0.39	-0.18	136.31	136.31	84.06	84.06
Piede	(4+5)-II-1 (-)	-137.38	-71.47	0.00	0.39	0.00	136.31	136.31	84.06	84.06
Piede	(4+5)-VIII-1 (-)	-136.62	-66.16	0.00	1.69	0.00	136.18	136.18	83.98	83.98
Piede	(4+5)-VIII-1 (+)	-136.62	-66.16	6.39	1.69	-0.26	136.18	136.18	83.98	83.98
Piede	(4+5)-V-1 (+)	-131.27	-46.87	4.57	6.27	-0.51	135.24	135.24	83.41	83.41
Piede	(4+5)-V-1 (-)	-131.27	-46.87	0.00	6.27	0.00	135.24	135.24	83.41	83.41
Piede	(4+5)-I-1 (-)	-131.03	-23.37	0.00	26.08	0.00	135.20	135.20	83.39	83.39
Piede	(4+5)-I-1 (+)	-131.03	-23.37	2.43	26.08	-1.62	135.20	135.20	83.39	83.39
Piede	(4+5)-XI-1 (-)	-130.51	-41.56	0.00	7.58	0.00	135.11	135.11	83.33	83.33
Piede	(4+5)-XI-1 (+)	-130.51	-41.56	4.07	7.58	-0.59	135.11	135.11	83.33	83.33
Piede	(4+5)-VIII-3 (-)	-129.58	-72.54	0.00	-18.13	0.00	134.95	134.95	83.23	83.23
Piede	(4+5)-VIII-3 (+)	-129.58	-72.54	7.00	-18.13	0.85	134.95	134.95	83.23	83.23
Piede	(4+5)-IV-1 (-)	-129.20	-15.99	0.00	27.84	0.00	134.88	134.88	83.19	83.19
Piede	(4+5)-IV-1 (+)	-129.20	-15.99	1.73	27.84	-1.72	134.88	134.88	83.19	83.19
Piede	(4+5)-II-3 (-)	-128.82	-67.23	0.00	-16.82	0.00	134.82	134.82	83.15	83.15
Piede	(4+5)-II-3 (+)	-128.82	-67.23	6.49	-16.82	0.78	134.82	134.82	83.15	83.15

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 87 di 103

Zona	C.	N	MyCal	ΔMy	MzCal	ΔMz	Mry+	Mry-	Mrz+	Mrz-
Piede	(4+5)-VII-1 (-)	-128.50	-5.68	0.00	30.43	0.00	134.76	134.76	83.12	83.12
Piede	(4+5)-VII-1 (+)	-128.50	-5.68	0.76	30.43	-1.86	134.76	134.76	83.12	83.12
Piede	(4+5)-X-1 (-)	-126.67	1.70	0.00	32.19	0.00	134.44	134.44	82.93	82.93
Piede	(4+5)-X-1 (+)	-126.67	1.70	0.06	32.19	-1.96	134.44	134.44	82.93	82.93
Piede	(4+5)-XI-3 (+)	-123.47	-47.93	4.68	-12.24	0.52	133.88	133.88	82.59	82.59
Piede	(4+5)-XI-3 (-)	-123.47	-47.93	0.00	-12.24	0.00	133.88	133.88	82.59	82.59
Piede	(4+5)-V-3 (+)	-122.71	-42.62	4.18	-10.94	0.45	133.75	133.75	82.51	82.51
Piede	(4+5)-V-3 (-)	-122.71	-42.62	0.00	-10.94	0.00	133.75	133.75	82.51	82.51
Piede	(4+5)-III-1 (-)	-121.04	-18.42	0.00	6.00	0.00	133.46	133.46	82.33	82.33
Piede	(4+5)-III-1 (+)	-121.04	-18.42	1.96	6.00	-0.50	133.46	133.46	82.33	82.33
Piede	(4+5)-IX-1 (-)	-120.29	-13.11	0.00	7.31	0.00	133.32	133.32	82.25	82.25
Piede	(4+5)-IX-1 (+)	-120.29	-13.11	1.46	7.31	-0.57	133.32	133.32	82.25	82.25
Piede	(4+5)-VI-1 (-)	-119.21	-11.04	0.00	7.77	0.00	133.14	133.14	82.13	82.13
Piede	(4+5)-VI-1 (+)	-119.21	-11.04	1.27	7.77	-0.60	133.14	133.14	82.13	82.13
Piede	(4+5)-IV-2 (+)	-118.86	14.72	-1.10	29.12	-1.79	133.08	133.08	82.10	82.10
Piede	(4+5)-IV-2 (-)	-118.86	14.72	0.00	29.12	0.00	133.08	133.08	82.10	82.10
Piede	(4+5)-XII-1 (+)	-118.45	-5.73	0.77	9.07	-0.67	133.00	133.00	82.05	82.05
Piede	(4+5)-XII-1 (-)	-118.45	-5.73	0.00	9.07	0.00	133.00	133.00	82.05	82.05
Piede	(4+5)-I-2 (-)	-117.03	22.10	0.00	30.89	0.00	132.75	132.75	81.90	81.90
Piede	(4+5)-I-2 (+)	-117.03	22.10	-1.80	30.89	-1.89	132.75	132.75	81.90	81.90
Piede	(4+5)-X-2 (+)	-116.33	32.41	-2.77	33.48	-2.03	132.63	132.63	81.83	81.83
Piede	(4+5)-X-2 (-)	-116.33	32.41	0.00	33.48	0.00	132.63	132.63	81.83	81.83
Piede	(4+5)-VII-2 (-)	-114.50	39.79	0.00	35.24	0.00	132.31	132.31	81.63	81.63
Piede	(4+5)-VII-2 (+)	-114.50	39.79	-3.47	35.24	-2.13	132.31	132.31	81.63	81.63
Piede	(4+5)-IX-3 (-)	-113.25	-19.49	0.00	-12.51	0.00	132.09	132.09	81.50	81.50
Piede	(4+5)-IX-3 (+)	-113.25	-19.49	2.07	-12.51	0.54	132.09	132.09	81.50	81.50
Piede	(4+5)-III-3 (+)	-112.49	-14.18	1.57	-11.21	0.46	131.96	131.96	81.42	81.42
Piede	(4+5)-III-3 (-)	-112.49	-14.18	0.00	-11.21	0.00	131.96	131.96	81.42	81.42
Piede	(4+5)-XII-3 (+)	-111.41	-12.10	1.37	-10.75	0.44	131.77	131.77	81.30	81.30
Piede	(4+5)-XII-3 (-)	-111.41	-12.10	0.00	-10.75	0.00	131.77	131.77	81.30	81.30
Piede	(4+5)-VI-3 (-)	-110.65	-6.80	0.00	-9.44	0.00	131.64	131.64	81.22	81.22
Piede	(4+5)-VI-3 (+)	-110.65	-6.80	0.87	-9.44	0.36	131.64	131.64	81.22	81.22
Piede	(4+5)-VI-2 (-)	-108.88	19.67	0.00	9.05	0.00	131.32	131.32	81.03	81.03
Piede	(4+5)-VI-2 (+)	-108.88	19.67	-1.56	9.05	-0.67	131.32	131.32	81.03	81.03
Piede	(4+5)-XII-2 (-)	-108.12	24.98	0.00	10.35	0.00	131.19	131.19	80.95	80.95
Piede	(4+5)-XII-2 (+)	-108.12	24.98	-2.07	10.35	-0.74	131.19	131.19	80.95	80.95
Piede	(4+5)-III-2 (+)	-107.04	27.05	-2.26	10.81	-0.77	131.00	131.00	80.84	80.84
Piede	(4+5)-III-2 (-)	-107.04	27.05	0.00	10.81	0.00	131.00	131.00	80.84	80.84
Piede	(4+5)-IX-2 (-)	-106.28	32.36	0.00	12.12	0.00	130.87	130.87	80.76	80.76
Piede	(4+5)-IX-2 (+)	-106.28	32.36	-2.76	12.12	-0.84	130.87	130.87	80.76	80.76
Piede	(4+5)-VII-3 (-)	-105.03	-26.92	0.00	-35.63	0.00	130.65	130.65	80.62	80.62
Piede	(4+5)-VII-3 (+)	-105.03	-26.92	2.78	-35.63	1.83	130.65	130.65	80.62	80.62
Piede	(4+5)-X-3 (-)	-103.20	-19.54	0.00	-33.87	0.00	130.32	130.32	80.43	80.43
Piede	(4+5)-X-3 (+)	-103.20	-19.54	2.08	-33.87	1.73	130.32	130.32	80.43	80.43
Piede	(4+5)-I-3 (-)	-102.50	-9.23	0.00	-31.28	0.00	130.20	130.20	80.35	80.35
Piede	(4+5)-I-3 (+)	-102.50	-9.23	1.10	-31.28	1.58	130.20	130.20	80.35	80.35
Piede	(4+5)-XII-4 (-)	-101.08	18.60	0.00	-9.46	0.00	129.95	129.95	80.20	80.20
Piede	(4+5)-XII-4 (+)	-101.08	18.60	-1.46	-9.46	0.37	129.95	129.95	80.20	80.20
Piede	(4+5)-IV-3 (-)	-100.67	-1.84	0.00	-29.52	0.00	129.88	129.88	80.16	80.16
Piede	(4+5)-IV-3 (+)	-100.67	-1.84	0.41	-29.52	1.49	129.88	129.88	80.16	80.16
Piede	(4+5)-VI-4 (+)	-100.32	23.91	-1.96	-8.16	0.29	129.82	129.82	80.12	80.12
Piede	(4+5)-VI-4 (-)	-100.32	23.91	0.00	-8.16	0.00	129.82	129.82	80.12	80.12
Piede	(4+5)-IX-4 (+)	-99.24	25.99	-2.16	-7.70	0.27	129.63	129.63	80.00	80.00
Piede	(4+5)-IX-4 (-)	-99.24	25.99	0.00	-7.70	0.00	129.63	129.63	80.00	80.00
Piede	(4+5)-III-4 (+)	-98.48	31.29	-2.66	-6.39	0.19	129.49	129.49	79.92	79.92
Piede	(4+5)-III-4 (-)	-98.48	31.29	0.00	-6.39	0.00	129.49	129.49	79.92	79.92
Piede	(4+5)-V-2 (-)	-96.82	55.50	0.00	10.54	0.00	129.20	129.20	79.74	79.74
Piede	(4+5)-V-2 (+)	-96.82	55.50	-4.87	10.54	-0.75	129.20	129.20	79.74	79.74
Piede	(4+5)-XI-2 (+)	-96.06	60.80	-5.37	11.85	-0.83	129.06	129.06	79.66	79.66
Piede	(4+5)-XI-2 (-)	-96.06	60.80	0.00	11.85	0.00	129.06	129.06	79.66	79.66
Piede	(4+5)-X-4 (+)	-92.86	11.17	-0.75	-32.59	1.66	128.50	128.50	79.32	79.32
Piede	(4+5)-X-4 (-)	-92.86	11.17	0.00	-32.59	0.00	128.50	128.50	79.32	79.32
Piede	(4+5)-VII-4 (+)	-91.03	18.55	-1.45	-30.82	1.56	128.17	128.17	79.12	79.12
Piede	(4+5)-VII-4 (-)	-91.03	18.55	0.00	-30.82	0.00	128.17	128.17	79.12	79.12
Piede	(4+5)-II-2 (-)	-90.71	80.10	0.00	16.43	0.00	128.12	128.12	79.09	79.09
Piede	(4+5)-II-2 (+)	-90.71	80.10	-7.19	16.43	-1.08	128.12	128.12	79.09	79.09
Piede	(4+5)-IV-4 (-)	-90.33	28.86	0.00	-28.23	0.00	128.05	128.05	79.05	79.05
Piede	(4+5)-IV-4 (+)	-90.33	28.86	-2.42	-28.23	1.41	128.05	128.05	79.05	79.05
Piede	(4+5)-VIII-2 (-)	-89.95	85.41	0.00	17.73	0.00	127.98	127.98	79.01	79.01
Piede	(4+5)-VIII-2 (+)	-89.95	85.41	-7.69	17.73	-1.16	127.98	127.98	79.01	79.01
Piede	(4+5)-XI-4 (+)	-89.02	54.43	-4.76	-7.97	0.28	127.82	127.82	78.91	78.91
Piede	(4+5)-XI-4 (-)	-89.02	54.43	0.00	-7.97	0.00	127.82	127.82	78.91	78.91
Piede	(4+5)-I-4 (+)	-88.50	36.25	-3.12	-26.47	1.31	127.73	127.73	78.85	78.85
Piede	(4+5)-I-4 (-)	-88.50	36.25	0.00	-26.47	0.00	127.73	127.73	78.85	78.85
Piede	(4+5)-V-4 (+)	-88.26	59.74	-5.27	-6.66	0.21	127.68	127.68	78.82	78.82
Piede	(4+5)-V-4 (-)	-88.26	59.74	0.00	-6.66	0.00	127.68	127.68	78.82	78.82

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 88 di 103

Zona	C.	N	MyCal	ΔMy	MzCal	ΔMz	Mry+	Mry-	Mrz+	Mrz-
Piede	(4+5)-VIII-4 (+)	-82.91	79.04	-7.08	-2.08	-0.05	126.73	126.73	78.25	78.25
Piede	(4+5)-VIII-4 (-)	-82.91	79.04	0.00	-2.08	0.00	126.73	126.73	78.25	78.25
Piede	(4+5)-II-4 (-)	-82.15	84.34	0.00	-0.78	0.00	126.60	126.60	78.17	78.17
Piede	(4+5)-II-4 (+)	-82.15	84.34	-7.58	-0.78	-0.12	126.60	126.60	78.17	78.17
Testa	2 (+)	-139.43	-3.49	0.00	-9.03	0.00	136.66	136.66	84.28	84.28
Testa	2 (-)	-139.43	-3.49	2.16	-9.03	0.27	136.66	136.66	84.28	84.28
Testa	3 (+)	-138.79	-3.47	0.00	-8.62	0.00	136.55	136.55	84.21	84.21
Testa	3 (-)	-138.79	-3.47	2.15	-8.62	0.25	136.55	136.55	84.21	84.21
Testa	1 (-)	-127.66	-3.19	1.98	-7.59	0.21	134.61	134.61	83.03	83.03
Testa	1 (+)	-127.66	-3.19	0.00	-7.59	0.00	134.61	134.61	83.03	83.03
Testa	(4+5)-II-1 (+)	-122.38	63.46	0.00	-5.96	0.00	133.69	133.69	82.47	82.47
Testa	(4+5)-II-1 (-)	-122.38	63.46	-6.89	-5.96	0.18	133.69	133.69	82.47	82.47
Testa	(4+5)-VIII-1 (-)	-121.62	58.95	-6.39	-7.23	0.26	133.56	133.56	82.39	82.39
Testa	(4+5)-VIII-1 (+)	-121.62	58.95	0.00	-7.23	0.00	133.56	133.56	82.39	82.39
Testa	(4+5)-V-1 (+)	-116.27	42.66	0.00	-11.64	0.00	132.62	132.62	81.82	81.82
Testa	(4+5)-V-1 (-)	-116.27	42.66	-4.57	-11.64	0.51	132.62	132.62	81.82	81.82
Testa	(4+5)-I-1 (-)	-116.03	24.16	-2.43	-30.54	1.62	132.58	132.58	81.80	81.80
Testa	(4+5)-I-1 (+)	-116.03	24.16	0.00	-30.54	0.00	132.58	132.58	81.80	81.80
Testa	(4+5)-XI-1 (-)	-115.51	38.14	-4.07	-12.92	0.59	132.49	132.49	81.74	81.74
Testa	(4+5)-XI-1 (+)	-115.51	38.14	0.00	-12.92	0.00	132.49	132.49	81.74	81.74
Testa	(4+5)-VIII-3 (-)	-114.58	64.44	-7.00	11.73	-0.85	132.32	132.32	81.64	81.64
Testa	(4+5)-VIII-3 (+)	-114.58	64.44	0.00	11.73	0.00	132.32	132.32	81.64	81.64
Testa	(4+5)-IV-1 (-)	-114.20	17.91	-1.73	-32.24	1.72	132.26	132.26	81.60	81.60
Testa	(4+5)-IV-1 (+)	-114.20	17.91	0.00	-32.24	0.00	132.26	132.26	81.60	81.60
Testa	(4+5)-I-3 (-)	-113.82	59.93	-6.49	10.46	-0.78	132.19	132.19	81.56	81.56
Testa	(4+5)-I-3 (+)	-113.82	59.93	0.00	10.46	0.00	132.19	132.19	81.56	81.56
Testa	(4+5)-VII-1 (-)	-113.50	9.10	-0.76	-34.78	1.86	132.14	132.14	81.53	81.53
Testa	(4+5)-VII-1 (+)	-113.50	9.10	0.00	-34.78	0.00	132.14	132.14	81.53	81.53
Testa	(4+5)-X-1 (-)	-111.67	2.86	-0.06	-36.48	1.96	131.81	131.81	81.33	81.33
Testa	(4+5)-X-1 (+)	-111.67	2.86	0.00	-36.48	0.00	131.81	131.81	81.33	81.33
Testa	(4+5)-XI-3 (+)	-108.47	43.64	0.00	6.05	0.00	131.25	131.25	80.99	80.99
Testa	(4+5)-XI-3 (-)	-108.47	43.64	-4.68	6.05	-0.52	131.25	131.25	80.99	80.99
Testa	(4+5)-V-3 (+)	-107.71	39.12	0.00	4.77	0.00	131.12	131.12	80.91	80.91
Testa	(4+5)-V-3 (-)	-107.71	39.12	-4.18	4.77	-0.45	131.12	131.12	80.91	80.91
Testa	(4+5)-III-1 (-)	-106.04	20.03	-1.96	-11.39	0.50	130.82	130.82	80.73	80.73
Testa	(4+5)-III-1 (+)	-106.04	20.03	0.00	-11.39	0.00	130.82	130.82	80.73	80.73
Testa	(4+5)-IX-1 (-)	-105.29	15.52	-1.46	-12.66	0.57	130.69	130.69	80.65	80.65
Testa	(4+5)-IX-1 (+)	-105.29	15.52	0.00	-12.66	0.00	130.69	130.69	80.65	80.65
Testa	(4+5)-VI-1 (-)	-104.21	13.79	-1.27	-13.09	0.60	130.50	130.50	80.54	80.54
Testa	(4+5)-VI-1 (+)	-104.21	13.79	0.00	-13.09	0.00	130.50	130.50	80.54	80.54
Testa	(4+5)-IV-2 (+)	-103.86	-6.83	0.00	-33.48	0.00	130.44	130.44	80.50	80.50
Testa	(4+5)-IV-2 (-)	-103.86	-6.83	1.10	-33.48	1.79	130.44	130.44	80.50	80.50
Testa	(4+5)-XII-1 (+)	-103.45	9.28	0.00	-14.36	0.00	130.37	130.37	80.45	80.45
Testa	(4+5)-XII-1 (-)	-103.45	9.28	-0.77	-14.36	0.67	130.37	130.37	80.45	80.45
Testa	(4+5)-I-2 (-)	-102.03	-13.07	1.80	-35.19	1.89	130.12	130.12	80.30	80.30
Testa	(4+5)-I-2 (+)	-102.03	-13.07	0.00	-35.19	0.00	130.12	130.12	80.30	80.30
Testa	(4+5)-X-2 (+)	-101.33	-21.88	0.00	-37.72	0.00	129.99	129.99	80.23	80.23
Testa	(4+5)-X-2 (-)	-101.33	-21.88	2.77	-37.72	2.03	129.99	129.99	80.23	80.23
Testa	(4+5)-VII-2 (-)	-99.50	-28.12	3.47	-39.43	2.13	129.67	129.67	80.03	80.03
Testa	(4+5)-VII-2 (+)	-99.50	-28.12	0.00	-39.43	0.00	129.67	129.67	80.03	80.03
Testa	(4+5)-IX-3 (-)	-98.25	21.01	-2.07	6.30	-0.54	129.45	129.45	79.90	79.90
Testa	(4+5)-IX-3 (+)	-98.25	21.01	0.00	6.30	0.00	129.45	129.45	79.90	79.90
Testa	(4+5)-III-3 (+)	-97.49	16.50	0.00	5.03	0.00	129.32	129.32	79.82	79.82
Testa	(4+5)-III-3 (-)	-97.49	16.50	-1.57	5.03	-0.46	129.32	129.32	79.82	79.82
Testa	(4+5)-XII-3 (+)	-96.41	14.77	0.00	4.60	0.00	129.13	129.13	79.70	79.70
Testa	(4+5)-XII-3 (-)	-96.41	14.77	-1.37	4.60	-0.44	129.13	129.13	79.70	79.70
Testa	(4+5)-VI-3 (-)	-95.65	10.26	-0.87	3.33	-0.36	128.99	128.99	79.62	79.62
Testa	(4+5)-VI-3 (+)	-95.65	10.26	0.00	3.33	0.00	128.99	128.99	79.62	79.62
Testa	(4+5)-VI-2 (-)	-93.88	-10.95	1.56	-14.33	0.67	128.68	128.68	79.43	79.43
Testa	(4+5)-VI-2 (+)	-93.88	-10.95	0.00	-14.33	0.00	128.68	128.68	79.43	79.43
Testa	(4+5)-XII-2 (-)	-93.12	-15.47	2.07	-15.60	0.74	128.54	128.54	79.35	79.35
Testa	(4+5)-XII-2 (+)	-93.12	-15.47	0.00	-15.60	0.00	128.54	128.54	79.35	79.35
Testa	(4+5)-III-2 (+)	-92.04	-17.19	0.00	-16.03	0.00	128.35	128.35	79.23	79.23
Testa	(4+5)-III-2 (-)	-92.04	-17.19	2.26	-16.03	0.77	128.35	128.35	79.23	79.23
Testa	(4+5)-IX-2 (-)	-91.28	-21.71	2.76	-17.31	0.84	128.22	128.22	79.15	79.15
Testa	(4+5)-IX-2 (+)	-91.28	-21.71	0.00	-17.31	0.00	128.22	128.22	79.15	79.15
Testa	(4+5)-VII-3 (-)	-90.03	27.42	-2.78	28.43	-1.83	128.00	128.00	79.01	79.01
Testa	(4+5)-VII-3 (+)	-90.03	27.42	0.00	28.43	0.00	128.00	128.00	79.01	79.01
Testa	(4+5)-X-3 (-)	-88.20	21.18	-2.08	26.72	-1.73	127.67	127.67	78.82	78.82
Testa	(4+5)-X-3 (+)	-88.20	21.18	0.00	26.72	0.00	127.67	127.67	78.82	78.82
Testa	(4+5)-I-3 (-)	-87.50	12.37	-1.10	24.19	-1.58	127.55	127.55	78.74	78.74
Testa	(4+5)-I-3 (+)	-87.50	12.37	0.00	24.19	0.00	127.55	127.55	78.74	78.74
Testa	(4+5)-XII-4 (-)	-86.08	-9.97	1.46	3.36	-0.37	127.30	127.30	78.59	78.59
Testa	(4+5)-XII-4 (+)	-86.08	-9.97	0.00	3.36	0.00	127.30	127.30	78.59	78.59
Testa	(4+5)-IV-3 (-)	-85.67	6.13	-0.41	22.48	-1.49	127.22	127.22	78.55	78.55
Testa	(4+5)-IV-3 (+)	-85.67	6.13	0.00	22.48	0.00	127.22	127.22	78.55	78.55

Zona	C.	N	MyCal	ΔMy	MzCal	ΔMz	Mry+	Mry-	Mrz+	Mrz-
Testa	(4+5)-VI-4 (+)	-85.32	-14.49	0.00	2.09	0.00	127.16	127.16	78.51	78.51
Testa	(4+5)-VI-4 (-)	-85.32	-14.49	1.96	2.09	-0.29	127.16	127.16	78.51	78.51
Testa	(4+5)-IX-4 (+)	-84.24	-16.21	0.00	1.66	0.00	126.97	126.97	78.39	78.39
Testa	(4+5)-IX-4 (-)	-84.24	-16.21	2.16	1.66	-0.27	126.97	126.97	78.39	78.39
Testa	(4+5)-III-4 (+)	-83.48	-20.73	0.00	0.38	0.00	126.84	126.84	78.31	78.31
Testa	(4+5)-III-4 (-)	-83.48	-20.73	2.66	0.38	-0.19	126.84	126.84	78.31	78.31
Testa	(4+5)-V-2 (-)	-81.82	-39.82	4.87	-15.78	0.75	126.54	126.54	78.13	78.13
Testa	(4+5)-V-2 (+)	-81.82	-39.82	0.00	-15.78	0.00	126.54	126.54	78.13	78.13
Testa	(4+5)-XI-2 (+)	-81.06	-44.34	0.00	-17.05	0.00	126.41	126.41	78.05	78.05
Testa	(4+5)-XI-2 (-)	-81.06	-44.34	5.37	-17.05	0.83	126.41	126.41	78.05	78.05
Testa	(4+5)-X-4 (+)	-77.86	-3.56	0.00	25.48	0.00	125.84	125.84	77.70	77.70
Testa	(4+5)-X-4 (-)	-77.86	-3.56	0.75	25.48	-1.66	125.84	125.84	77.70	77.70
Testa	(4+5)-VII-4 (+)	-76.03	-9.80	0.00	23.78	0.00	125.51	125.51	77.51	77.51
Testa	(4+5)-VII-4 (-)	-76.03	-9.80	1.45	23.78	-1.56	125.51	125.51	77.51	77.51
Testa	(4+5)-II-2 (-)	-75.71	-60.62	7.19	-21.46	1.08	125.45	125.45	77.47	77.47
Testa	(4+5)-II-2 (+)	-75.71	-60.62	0.00	-21.46	0.00	125.45	125.45	77.47	77.47
Testa	(4+5)-IV-4 (-)	-75.33	-18.61	2.42	21.24	-1.41	125.39	125.39	77.43	77.43
Testa	(4+5)-IV-4 (+)	-75.33	-18.61	0.00	21.24	0.00	125.39	125.39	77.43	77.43
Testa	(4+5)-VIII-2 (-)	-74.95	-65.14	7.69	-22.73	1.16	125.32	125.32	77.39	77.39
Testa	(4+5)-VIII-2 (+)	-74.95	-65.14	0.00	-22.73	0.00	125.32	125.32	77.39	77.39
Testa	(4+5)-XI-4 (+)	-74.02	-38.84	0.00	1.91	0.00	125.15	125.15	77.29	77.29
Testa	(4+5)-XI-4 (-)	-74.02	-38.84	4.76	1.91	-0.28	125.15	125.15	77.29	77.29
Testa	(4+5)-I-4 (+)	-73.50	-24.85	0.00	19.54	0.00	125.06	125.06	77.23	77.23
Testa	(4+5)-I-4 (-)	-73.50	-24.85	3.12	19.54	-1.31	125.06	125.06	77.23	77.23
Testa	(4+5)-V-4 (+)	-73.26	-43.36	0.00	0.64	0.00	125.02	125.02	77.21	77.21
Testa	(4+5)-V-4 (-)	-73.26	-43.36	5.27	0.64	-0.21	125.02	125.02	77.21	77.21
Testa	(4+5)-VIII-4 (+)	-67.91	-59.64	0.00	-3.77	0.00	124.06	124.06	76.63	76.63
Testa	(4+5)-VIII-4 (-)	-67.91	-59.64	7.08	-3.77	0.05	124.06	124.06	76.63	76.63
Testa	(4+5)-II-4 (-)	-67.15	-64.16	7.58	-5.04	0.12	123.93	123.93	76.54	76.54
Testa	(4+5)-II-4 (+)	-67.15	-64.16	0.00	-5.04	0.00	123.93	123.93	76.54	76.54

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrzd	Vrsd	Vrd	Ast/m	cot (θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(4+5)-VII-2	--	--	18.67	--	432.14	209.09	209.09	9.35	2.500	11
Z	(4+5)-VIII-2	--	--	37.64	--	459.98	373.73	373.73	9.35	2.500	9.9

Verifica dei Muri in calcestruzzo

Scenario di calcolo: **ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO**

Simbologia:

Muro Indice del muro in verifica
Nodi [n1-n2-n3-n4...] Indici dei nodi di attacco del muro
Pann.X Numero di pannelli in direzione locale X del muro(per muri a pannelli)
Pann.Y Numero di pannelli in direzione locale Y del muro(per muri a pannelli)
Pann Numero totale di pannelli (per muri a mesh)
Spess [cm] Spessore del muro
Criterio Criterio di verifica adottato per la verifica
Pannello Indice del pannello
Nx [kN] Sforzo in direzione x locale per metro lineare (Nx=xxx*spessore)
Ny [kN] Sforzo in direzione y locale per metro lineare (Ny=syy*spessore)
Nxy [kN] Sforzo tagliante locale per metro lineare (Nxy=sxy*spessore)
Mx [kN*m] Momento in direzione x locale per metro lineare
My [kN*m] Momento in direzione y locale per metro lineare
Mxy [kN*m] Momento torcente locale per metro lineare
Ax [m^2] Armatura totale pannello in direzione x locale (1)
Ay [m^2] Armatura totale pannello in direzione y locale (1)
εc Deformazione nel cls (2)
εf Deformazione nell'acciaio (2)
Massimi Armature massime riscontrate nel muro
Massimo massima sigma ideale riscontrata nel muro
σid+,σid- [MPa] $(\sigma_x^2 + \sigma_y^2 - \sigma_x \sigma_y + 3 \tau_{xy}^2)^{1/2}$ Tensioni ideali ai lembi della lastra (Acciaio)
σid+,σid- [MPa] $(\sigma_x^2 + \sigma_y^2 - \sigma_x \sigma_y + 3 \tau_{xy}^2)^{1/2}$ Tensioni ideali ai lembi della lastra (Legno)
Fatt.Ampl.Sisma Fattore moltiplicativo di gruppo per le azioni sismiche (solo se diverso da 1.0)
Cs Coefficiente di sicurezza definito dal rapporto |Mr(N)|/|Md| (Mr(N)=Momento resistente corrispondente allo sforzo normale N,Md=momento agente), quando richiesto dal criterio di verifica
ξs Livello di sicurezza sismico definito come rapporto tra l'accelerazione sopportabile e l'accelerazione di progetto, quando richiesto dal criterio di verifica

Note Verifica muri:

(1): Le armature Ax ed Ay vanno intese come a metro lineare di pannello.

(2):Le deformazioni sono stampate a meno del fattore 10⁻³; esse si riferiscono alla verifica considerando quali sollecitazioni di progetto Mx,d=Mx +/- |Mxy|,My,d=My +/- |Mxy| scegliendo il segno in modo tale da rendere massimo in

valore assoluto il relativo momento flettente, le sollecitazioni stampate si riferiscono alle sollecitazioni in una data combinazione riferite al sistema locale del pannello

Muro : 1 - Nodi: [110-111-211-210] Pann=12 Spess.=15 cm, Terreno=--, Criterio=CLS_Muri_ND, Materiale=C35/45, $\zeta_E=2.687$
[(4+5)-I-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kN	kN	kN	kN*m	kN*m	kN*m	cmq	cmq		
12	296.53	57.89	33.90	-0.64	-0.23	0.72	10.47	7.85	2	2.5
1	-18.11	-2.78	-29.50	-0.17	-1.27	0.36	10.47	7.85	(4+5)-V-3	9.8

Muro : 2 - Nodi: [111-112-212-211] Pann=12 Spess.=15 cm, Terreno=--, Criterio=CLS_Muri_ND, Materiale=C35/45, $\zeta_E=2.687$
[(4+5)-IV-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kN	kN	kN	kN*m	kN*m	kN*m	cmq	cmq		
2	296.53	57.89	-33.90	-0.64	-0.23	-0.72	10.47	7.85	2	2.5
1	21.98	-22.40	-65.43	-0.60	-1.00	-0.94	10.47	7.85	2	8.8

Muro : 3 - Nodi: [109-108-208-209] Pann=12 Spess.=15 cm, Terreno=--, Criterio=CLS_Muri_ND, Materiale=C35/45, $\zeta_E=2.857$
[(4+5)-X-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kN	kN	kN	kN*m	kN*m	kN*m	cmq	cmq		
12	284.69	56.64	33.60	-0.64	-0.23	0.72	10.47	7.85	2	3.0
1	-17.84	-3.24	-28.90	-0.17	-1.29	0.37	10.47	7.85	(4+5)-VIII-2	9.7

Muro : 4 - Nodi: [108-107-207-208] Pann=12 Spess.=15 cm, Terreno=--, Criterio=CLS_Muri_ND, Materiale=C35/45, $\zeta_E=2.857$
[(4+5)-VII-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kN	kN	kN	kN*m	kN*m	kN*m	cmq	cmq		
2	284.69	56.64	-33.60	-0.64	-0.23	-0.72	10.47	7.85	2	3.0
1	18.69	-22.23	-64.82	-0.59	-1.00	-0.93	10.47	7.85	2	8.9

Muro : 5 - Nodi: [107-110-210-207] Pann=12 Spess.=15 cm, Terreno=--, Criterio=CLS_Muri_ND, Materiale=C35/45, $\zeta_E=2.852$
[(4+5)-XI-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kN	kN	kN	kN*m	kN*m	kN*m	cmq	cmq		
1	3.26	-34.90	30.84	-0.06	-0.77	0.50	10.47	7.85	(4+5)-XI-4	14

Muro : 6 - Nodi: [209-212-112-109] Pann=12 Spess.=15 cm, Terreno=--, Criterio=CLS_Muri_ND, Materiale=C35/45, $\zeta_E=2.853$
[(4+5)-VIII-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kN	kN	kN	kN*m	kN*m	kN*m	cmq	cmq		
2	3.26	-34.90	-30.85	-0.06	-0.77	-0.50	10.47	7.85	(4+5)-VIII-2	14

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
1	118.87	32.25	-22.55	0.08	-0.50	-0.48	10.47	7.85	(4+5)-VIII-2	14

Muro : 7 - Nodi: [105-111-110-104], Pann.X=6, Pann.Y=6Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=1.495$ [(4+5)-VII-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kN	kN	kN	kN*m	kN*m	kN*m	cmq	cmq		
4	13.64	265.21	-5.78	-3.77	-11.31	-0.76	7.85	11.00	2	1.1
25	69.17	-344.52	-4.20	0.06	11.60	-6.39	9.00	7.85	2	3.5
3	32.66	209.47	14.79	-3.36	-8.96	-2.69	7.85	11.00	2	1.6

Muro : 8 - Nodi: [106-112-111-105], Pann.X=6, Pann.Y=6Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=1.710$ [(4+5)-X-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kN	kN	kN	kN*m	kN*m	kN*m	cmq	cmq		
8	59.27	129.40	-79.97	-1.98	-7.01	3.48	7.85	7.85	2	1.5
3	133.65	145.20	-125.79	-8.30	-6.79	3.77	9.00	9.00	2	1.6

Muro : 9 - Nodi: [109-112-106-103], Pann.X=6, Pann.Y=6Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=1.141$ [(4+5)-II-4] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kN	kN	kN	kN*m	kN*m	kN*m	cmq	cmq		
36	192.47	-20.58	42.94	-7.75	0.88	-6.92	11.00	7.85	(4+5)-II-4	1.4
4	143.81	1.61	-16.93	-4.26	0.78	3.28	11.00	7.85	(4+5)-VIII-3	3.5
1	92.75	36.18	5.43	-2.28	-0.03	2.88	7.85	7.85	(4+5)-VIII-3	3.9

Muro : 10 - Nodi: [108-109-103-102], Pann.X=6, Pann.Y=6Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=1.487$ [(4+5)-IV-3] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kN	kN	kN	kN*m	kN*m	kN*m	cmq	cmq		
24	266.14	13.37	5.88	-11.35	-3.77	0.74	11.00	7.85	2	1.1
13	258.00	-116.27	31.00	-7.78	0.57	4.06	11.00	7.85	2	1.2
1	-346.63	178.51	18.78	9.97	-2.51	6.38	7.85	9.00	2	1.7

Muro : 11 - Nodi: [107-108-102-101], Pann.X=6, Pann.Y=6Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=1.487$ [(4+5)-I-1] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kN	kN	kN	kN*m	kN*m	kN*m	cmq	cmq		
18	266.14	13.37	-5.88	-11.35	-3.77	-0.74	11.00	7.85	2	1.1
7	174.34	-76.72	11.21	-5.64	0.50	3.27	11.00	7.85	(4+5)-I-1	2.6
31	-346.63	178.51	-18.78	9.97	-2.51	-6.38	7.85	9.00	2	1.7

Muro : 12 - Nodi: [107-101-104-110], Pann.X=6, Pann.Y=6Spess.=25 cm, Terreno=--,Criterio=CLS_Muri_ND,
Materiale=C35/45, $\zeta_e=1.153$ [(4+5)-V-2] : **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kN	kN	kN	kN*m	kN*m	kN*m	cmq	cmq		
36	128.86	43.27	106.54	-10.51	3.50	-4.30	9.00	7.85	(4+5)-V-2	1.4
30	95.24	30.22	101.46	-7.40	2.12	-3.32	9.00	7.85	(4+5)-V-2	2.2
25	29.53	93.94	100.38	2.02	-7.15	-3.30	7.85	9.00	(4+5)-XI-1	2.3

Verifiche stato limite di esercizio

Verifica delle travi (Stati limite esercizio)

Scenario di calcolo: **ScenarioNT_2018 A2_SLV_SLD_STR_GEO**

Simbologia

Terreno	Nome della stratigrafia per travi Winkler
L [cm]	Lunghezza teorica elemento (distanza tra i nodi)
Ln [cm]	Lunghezza netta elemento (tiene conto dei conci rigidi)
L2,L3 [cm]	Lunghezze libere di inflessione
Sez. R: Sezione Rettangolare	
	By[cm]: Larghezza (asse locale y)
	Bz[cm]: Larghezza (asse locale z)
Sez. T: Sezione a T (rovescia e non)	
	Ba[cm]: Larghezza base inferiore
	Ha[cm]: Altezza inferiore
	Bs[cm]: Larghezza superiore
	Hs[cm]: Altezza superiore
Sez. L: Sezione ad L (rovescia e non)	
	Ba[cm]: Larghezza base inferiore
	Ha[cm]: Altezza inferiore
	Bs[cm]: Larghezza superiore
	Hs[cm]: Altezza superiore
Sez. C: Sezione circolare	
	R[cm]: Raggio
Sez. G: Sezione generica	
	B[cm]: Larghezza
	H[cm]: Altezza
X [cm]	Punto di verifica
σ_{ca} [MPa]	Tensione ammissibile nel cls
σ_{fa} [MPa]	Tensione ammissibile nell'acciaio
σ_{cta} [MPa]	Tensione ammissibile a trazione (quando richiesto dalla verifica)
M- [kN*m]	Momento negativo massimo di calcolo
M+ [kN*m]	Momento positivo massimo di calcolo
M [kN*m]	Momento di calcolo (travi a flessione, pilastri circolari)
My [kN*m]	Momento calcolo per verifiche a pressoflessione
Mz [kN*m]	Momento calcolo per verifiche a pressoflessione (Sez. L,Pilastri)
N [kN]	Sforzo normale corrispondente ad My (e Mz per Sez. L,Pilastri)
Afsup [cmq]	Area di ferro superiore
Afinf [cmq]	Area di ferro inferiore
Afsin [cmq]	Area di ferro sinistra (Sez. L)
Afdes [cmq]	Area di ferro destra (Sez. L)
σ_{c-} [MPa]	Tensione nel cls compresso per effetto di M-
σ_{cy} [MPa]	Tensione nel cls compresso per effetto di (N,My) in caso di pressoflessione retta
σ_{cz} [MPa]	Tensione nel cls compresso per effetto di (N,Mz) in caso di pressoflessione retta
σ_{c+} [MPa]	Tensione nel cls compresso per effetto di M+
σ_{ct-} [MPa]	Tensione nel cls teso per effetto di M-
σ_{ct+} [MPa]	Tensione nel cls teso per effetto di M+
σ_{f-} [MPa]	Tensione nell'acciaio per effetto di M-
σ_{f+} [MPa]	Tensione nell'acciaio per effetto di M+
σ_{fy} [MPa]	Tensione nel acciaio per effetto di (N,My) in caso di pressoflessione retta
σ_{fz} [MPa]	Tensione nel acciaio per effetto di (N,Mz) in caso di pressoflessione retta
Cb-	Combinazione di carico generatore di M-
Cb+	Combinazione di carico generatore di M+
σ_c [MPa]	Tensione nel cls per effetto di N My
σ_f [MPa]	Tensione nell'acciaio per effetto di N My
Cb	Combinazione di carico generatore di N My
Act [m^2]	Area di calcestruzzo teso
Aft [cmq]	Area di acciaio teso
pAft [cm]	Perimetro area di acciaio teso
$s_{r,max}$ [cm]	Distanza massima delle fessure

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 93 di 103

σ_{fmed} [MPa] Tensione media dell'acciaio
 W_d [mm] Apertura delle fessure
 W_k [mm] Apertura caratteristica delle fessure
 W_{amm_Freq} [mm] Apertura ammissibile delle fessure per combinazione Frequente
 W_{amm_Qp} [mm] Apertura ammissibile delle fessure per combinazione Quasi Permanente
 W_{amm_Rara} [mm] Apertura ammissibile delle fessure per combinazione Rara
 C_s Coefficiente di sicurezza definito come minimo di σ_{amm}/σ tra acciaio e calcestruzzo oppure W_{amm}/W_k

Trave: 101 [101,104], Pilastrate [1,4] Sez. R: By=30.00 cm Bz=50.00 cm L=600.00 cm Ln=600.00 cm Criterio:
CLS_TraviAlte_ND

Combinazione Rara: σ_{ca} [MPa]=22.41 σ_{fa} [MPa]=360.00

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	9.38	8.04	8.04	--	--	-0.81	28.54	6	6	Si	13
60.00	--	3.23	8.04	8.04	--	--	-0.28	9.83	6	6	Si	37
300.00	5.80	--	8.04	8.04	-0.50	17.64	--	--	6	6	Si	20
540.00	--	3.14	8.04	8.04	--	--	-0.27	9.56	6	6	Si	38
600.00	--	9.32	8.04	8.04	--	--	-0.81	28.38	6	6	Si	13

Combinazione QP: σ_{ca} [MPa]=16.81 σ_{fa} [MPa]=360.00

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	10.13	8.04	8.04	--	--	-0.88	30.81	8	8	Si	12
60.00	--	3.55	8.04	8.04	--	--	-0.31	10.79	8	8	Si	33
300.00	6.12	--	8.04	8.04	-0.53	18.64	--	--	8	8	Si	19
540.00	--	3.46	8.04	8.04	--	--	-0.30	10.52	8	8	Si	34
600.00	--	10.07	8.04	8.04	--	--	-0.87	30.65	8	8	Si	12

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	W_d	W_k	Cb	Ver.	Cs
cm	kN*m	m ²	cmq	cm	cm	MPa	mm	mm			
0.00	10.19	0.03	8.04	20.11	21.87	31.00	0.019	0.019	7 (Fr)	Si	15
0.00	10.13	0.03	8.04	20.11	21.87	30.81	0.019	0.019	8 (Qp)	Si	10
60.00	3.55	0.03	8.04	20.11	21.87	10.79	0.007	0.007	8 (Qp)	Si	30
60.00	3.58	0.03	8.04	20.11	21.87	10.90	0.007	0.007	7 (Fr)	Si	44
300.00	-6.12	0.03	8.04	20.11	21.87	18.64	0.012	0.012	8 (Qp)	Si	17
300.00	-6.15	0.03	8.04	20.11	21.87	18.72	0.012	0.012	7 (Fr)	Si	26
540.00	3.46	0.03	8.04	20.11	21.87	10.52	0.007	0.007	8 (Qp)	Si	30
540.00	3.49	0.03	8.04	20.11	21.87	10.62	0.007	0.007	7 (Fr)	Si	45
600.00	10.07	0.03	8.04	20.11	21.87	30.65	0.019	0.019	8 (Qp)	Si	10
600.00	10.13	0.03	8.04	20.11	21.87	30.84	0.019	0.019	7 (Fr)	Si	16

Trave: 102 [104,105], Pilastrate [4,5] Sez. R: By=30.00 cm Bz=50.00 cm L=600.00 cm Ln=600.00 cm Criterio:
CLS_TraviAlte_ND

Combinazione Rara: σ_{ca} [MPa]=22.41 σ_{fa} [MPa]=360.00

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	17.46	8.04	8.04	--	--	-1.51	53.13	6	6	Si	6.8
60.00	1.95	--	8.04	8.04	-0.17	5.93	--	--	6	6	Si	61
300.00	18.36	--	8.04	8.04	-1.59	55.89	--	--	6	6	Si	6.4
540.00	--	18.32	8.04	8.04	--	--	-1.58	55.75	6	6	Si	6.5
600.00	--	45.74	8.04	8.04	--	--	-3.95	139.19	6	6	Si	2.6

Combinazione QP: σ_{ca} [MPa]=16.81 σ_{fa} [MPa]=360.00

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	16.21	8.04	8.04	--	--	-1.40	49.33	8	8	Si	7.3
60.00	1.49	--	8.04	8.04	-0.13	4.53	--	--	8	8	Si	80
300.00	17.08	--	8.04	8.04	-1.48	51.97	--	--	8	8	Si	6.9
540.00	--	17.40	8.04	8.04	--	--	-1.50	52.94	8	8	Si	6.8
600.00	--	42.75	8.04	8.04	--	--	-3.70	130.11	8	8	Si	2.8

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	W_d	W_k	Cb	Ver.	Cs
cm	kN*m	m ²	cmq	cm	cm	MPa	mm	mm			
0.00	16.48	0.03	8.04	20.11	21.87	50.14	0.031	0.031	7 (Fr)	Si	9.6
0.00	16.21	0.03	8.04	20.11	21.87	49.33	0.031	0.031	8 (Qp)	Si	6.5
60.00	-1.49	0.03	8.04	20.11	21.87	4.53	0.003	0.003	8 (Qp)	Si	71
60.00	-1.52	0.03	8.04	20.11	21.87	4.63	0.003	0.003	7 (Fr)	Si	>100
300.00	-17.08	0.03	8.04	20.11	21.87	51.97	0.032	0.032	8 (Qp)	Si	6.2

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 94 di 103

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
300.00	-17.37	0.03	8.04	20.11	21.87	52.85	0.033	0.033	7 (Fr)	Si	9.1
540.00	17.40	0.03	8.04	20.11	21.87	52.94	0.033	0.033	8 (Qp)	Si	6.0
540.00	17.64	0.03	8.04	20.11	21.87	53.69	0.034	0.034	7 (Fr)	Si	8.9
600.00	42.75	0.03	8.04	20.11	21.87	130.11	0.081	0.081	8 (Qp)	Si	2.5
600.00	43.42	0.03	8.04	20.11	21.87	132.14	0.083	0.083	7 (Fr)	Si	3.6

Trave: 102 [105,106], Pilastrate [5,6] Sez. R: By=30.00 cm Bz=50.00 cm L=600.00 cm Ln=600.00 cm Criterio:
CLS_TraviAlte_ND

Combinazione Rara: σ_{ca} [MPa]=22.41 σ_{fa} [MPa]=360.00

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	45.74	8.04	8.04	--	--	-3.95	139.19	6	6	Si	2.6
60.00	--	18.32	8.04	8.04	--	--	-1.58	55.75	6	6	Si	6.5
300.00	16.77	--	8.04	8.04	-1.45	51.04	--	--	6	6	Si	7.1
540.00	1.95	--	8.04	8.04	-0.17	5.93	--	--	6	6	Si	61
600.00	--	17.46	8.04	8.04	--	--	-1.51	53.13	6	6	Si	6.8

Combinazione QP: σ_{ca} [MPa]=16.81 σ_{fa} [MPa]=360.00

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	42.75	8.04	8.04	--	--	-3.70	130.11	8	8	Si	2.8
60.00	--	17.40	8.04	8.04	--	--	-1.50	52.94	8	8	Si	6.8
300.00	15.39	--	8.04	8.04	-1.33	46.84	--	--	8	8	Si	7.7
540.00	1.49	--	8.04	8.04	-0.13	4.53	--	--	8	8	Si	80
600.00	--	16.21	8.04	8.04	--	--	-1.40	49.33	8	8	Si	7.3

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kN*m	m ²	cmq	cm	cm	MPa	mm	mm			
0.00	43.42	0.03	8.04	20.11	21.87	132.14	0.083	0.083	7 (Fr)	Si	3.6
0.00	42.75	0.03	8.04	20.11	21.87	130.11	0.081	0.081	8 (Qp)	Si	2.5
60.00	17.40	0.03	8.04	20.11	21.87	52.94	0.033	0.033	8 (Qp)	Si	6.0
60.00	17.64	0.03	8.04	20.11	21.87	53.69	0.034	0.034	7 (Fr)	Si	8.9
300.00	-15.39	0.03	8.04	20.11	21.87	46.84	0.029	0.029	8 (Qp)	Si	6.8
300.00	-15.65	0.03	8.04	20.11	21.87	47.63	0.030	0.030	7 (Fr)	Si	10
540.00	-1.49	0.03	8.04	20.11	21.87	4.53	0.003	0.003	8 (Qp)	Si	71
540.00	-1.52	0.03	8.04	20.11	21.87	4.63	0.003	0.003	7 (Fr)	Si	>100
600.00	16.21	0.03	8.04	20.11	21.87	49.33	0.031	0.031	8 (Qp)	Si	6.5
600.00	16.48	0.03	8.04	20.11	21.87	50.14	0.031	0.031	7 (Fr)	Si	9.6

Trave: 103 [105,102], Pilastrate [5,2] Sez. R: By=70.00 cm Bz=25.00 cm L=600.00 cm Ln=600.00 cm Criterio:
CLS_TraviSpessore_ND

Combinazione Rara: σ_{ca} [MPa]=22.41 σ_{fa} [MPa]=360.00

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	14.45	14.07	14.07	--	--	-2.37	59.15	6	6	Si	6.1
60.00	--	7.31	14.07	14.07	--	--	-1.20	29.92	6	6	Si	12
300.00	5.51	--	14.07	14.07	-0.90	22.57	--	--	6	6	Si	16
540.00	--	6.86	14.07	14.07	--	--	-1.12	28.09	6	6	Si	13
600.00	--	13.89	14.07	14.07	--	--	-2.27	56.87	6	6	Si	6.3

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kN*m	m ²	cmq	cm	cm	MPa	mm	mm			
0.00	14.60	0.04	14.07	35.19	18.02	59.74	0.031	0.031	7 (Fr)	Si	9.8
0.00	14.57	0.04	14.07	35.19	18.02	59.61	0.031	0.031	8 (Qp)	Si	6.5
60.00	7.42	0.04	14.07	35.19	18.02	30.38	0.016	0.016	8 (Qp)	Si	13
60.00	7.45	0.04	14.07	35.19	18.02	30.50	0.016	0.016	7 (Fr)	Si	19
300.00	-5.40	0.04	14.07	35.19	18.02	22.10	0.011	0.011	8 (Qp)	Si	18
300.00	-5.37	0.04	14.07	35.19	18.02	21.99	0.011	0.011	7 (Fr)	Si	26
540.00	6.98	0.04	14.07	35.19	18.02	28.56	0.015	0.015	8 (Qp)	Si	14
540.00	7.00	0.04	14.07	35.19	18.02	28.66	0.015	0.015	7 (Fr)	Si	20
600.00	14.01	0.04	14.07	35.19	18.02	57.34	0.030	0.030	8 (Qp)	Si	6.8
600.00	14.03	0.04	14.07	35.19	18.02	57.44	0.030	0.030	7 (Fr)	Si	10

Trave: 104 [102,101], Pilastrate [2,1] Sez. R: By=30.00 cm Bz=50.00 cm L=600.00 cm Ln=600.00 cm Criterio:
CLS_TraviAlte_ND

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 95 di 103

Combinazione Rara: $\sigma_{ca}[MPa]=22.41$ $\sigma_{fa}[MPa]=360.00$

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	45.10	8.04	8.04	--	--	-3.90	137.25	6	6	Si	2.6
60.00	--	17.79	8.04	8.04	--	--	-1.54	54.15	6	6	Si	6.6
300.00	16.93	--	8.04	8.04	-1.46	51.53	--	--	6	6	Si	7.0
540.00	1.65	--	8.04	8.04	-0.14	5.02	--	--	6	6	Si	72
600.00	--	17.97	8.04	8.04	--	--	-1.55	54.69	6	6	Si	6.6

Combinazione QP: $\sigma_{ca}[MPa]=16.81$ $\sigma_{fa}[MPa]=360.00$

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	42.12	8.04	8.04	--	--	-3.64	128.18	8	8	Si	2.8
60.00	--	16.88	8.04	8.04	--	--	-1.46	51.36	8	8	Si	7.0
300.00	15.55	--	8.04	8.04	-1.34	47.31	--	--	8	8	Si	7.6
540.00	1.19	--	8.04	8.04	-0.10	3.63	--	--	8	8	Si	99
600.00	--	16.72	8.04	8.04	--	--	-1.45	50.88	8	8	Si	7.1

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	42.78	0.03	8.04	20.11	21.87	130.19	0.081	0.081	7 (Fr)	Si	3.7
0.00	42.12	0.03	8.04	20.11	21.87	128.18	0.080	0.080	8 (Qp)	Si	2.5
60.00	16.88	0.03	8.04	20.11	21.87	51.36	0.032	0.032	8 (Qp)	Si	6.2
60.00	17.12	0.03	8.04	20.11	21.87	52.09	0.033	0.033	7 (Fr)	Si	9.2
300.00	-15.55	0.03	8.04	20.11	21.87	47.31	0.030	0.030	8 (Qp)	Si	6.8
300.00	-15.81	0.03	8.04	20.11	21.87	48.11	0.030	0.030	7 (Fr)	Si	10.0
540.00	-1.19	0.03	8.04	20.11	21.87	3.63	0.002	0.002	8 (Qp)	Si	88
540.00	-1.22	0.03	8.04	20.11	21.87	3.72	0.002	0.002	7 (Fr)	Si	>100
600.00	16.72	0.03	8.04	20.11	21.87	50.88	0.032	0.032	8 (Qp)	Si	6.3
600.00	16.99	0.03	8.04	20.11	21.87	51.71	0.032	0.032	7 (Fr)	Si	9.3

Trave: 104 [103,102], Pilastrate [3,2] Sez. R: By=30.00 cm Bz=50.00 cm L=600.00 cm Ln=600.00 cm Criterio:
CLS_TraviAlte_ND

Combinazione Rara: $\sigma_{ca}[MPa]=22.41$ $\sigma_{fa}[MPa]=360.00$

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	17.97	8.04	8.04	--	--	-1.55	54.69	6	6	Si	6.6
60.00	1.65	--	8.04	8.04	-0.14	5.02	--	--	6	6	Si	72
300.00	18.51	--	8.04	8.04	-1.60	56.32	--	--	6	6	Si	6.4
540.00	--	17.79	8.04	8.04	--	--	-1.54	54.15	6	6	Si	6.6
600.00	--	45.10	8.04	8.04	--	--	-3.90	137.25	6	6	Si	2.6

Combinazione QP: $\sigma_{ca}[MPa]=16.81$ $\sigma_{fa}[MPa]=360.00$

X	M+	M-	Afsup	Afinf	σ_c+	σ_f+	σ_c-	σ_f-	Cb+	Cb-	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	16.72	8.04	8.04	--	--	-1.45	50.88	8	8	Si	7.1
60.00	1.19	--	8.04	8.04	-0.10	3.63	--	--	8	8	Si	99
300.00	17.22	--	8.04	8.04	-1.49	52.40	--	--	8	8	Si	6.9
540.00	--	16.88	8.04	8.04	--	--	-1.46	51.36	8	8	Si	7.0
600.00	--	42.12	8.04	8.04	--	--	-3.64	128.18	8	8	Si	2.8

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	16.99	0.03	8.04	20.11	21.87	51.71	0.032	0.032	7 (Fr)	Si	9.3
0.00	16.72	0.03	8.04	20.11	21.87	50.88	0.032	0.032	8 (Qp)	Si	6.3
60.00	-1.19	0.03	8.04	20.11	21.87	3.63	0.002	0.002	8 (Qp)	Si	88
60.00	-1.22	0.03	8.04	20.11	21.87	3.72	0.002	0.002	7 (Fr)	Si	>100
300.00	-17.22	0.03	8.04	20.11	21.87	52.40	0.033	0.033	8 (Qp)	Si	6.1
300.00	-17.51	0.03	8.04	20.11	21.87	53.28	0.033	0.033	7 (Fr)	Si	9.0
540.00	16.88	0.03	8.04	20.11	21.87	51.36	0.032	0.032	8 (Qp)	Si	6.2
540.00	17.12	0.03	8.04	20.11	21.87	52.09	0.033	0.033	7 (Fr)	Si	9.2
600.00	42.12	0.03	8.04	20.11	21.87	128.18	0.080	0.080	8 (Qp)	Si	2.5
600.00	42.78	0.03	8.04	20.11	21.87	130.19	0.081	0.081	7 (Fr)	Si	3.7

Trave: 105 [106,103], Pilastrate [6,3] Sez. R: By=30.00 cm Bz=50.00 cm L=600.00 cm Ln=600.00 cm Criterio:
CLS_TraviAlte_ND

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 96 di 103

Combinazione Rara: σ_{ca} [MPa]=22.41 σ_{fa} [MPa]=360.00

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	9.32	8.04	8.04	--	--	-0.81	28.38	6	6	Si	13
60.00	--	3.14	8.04	8.04	--	--	-0.27	9.56	6	6	Si	38
300.00	5.72	--	8.04	8.04	-0.49	17.41	--	--	6	6	Si	21
540.00	--	3.23	8.04	8.04	--	--	-0.28	9.83	6	6	Si	37
600.00	--	9.38	8.04	8.04	--	--	-0.81	28.54	6	6	Si	13

Combinazione QP: σ_{ca} [MPa]=16.81 σ_{fa} [MPa]=360.00

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	10.07	8.04	8.04	--	--	-0.87	30.65	8	8	Si	12
60.00	--	3.46	8.04	8.04	--	--	-0.30	10.52	8	8	Si	34
300.00	6.05	--	8.04	8.04	-0.52	18.41	--	--	8	8	Si	20
540.00	--	3.55	8.04	8.04	--	--	-0.31	10.79	8	8	Si	33
600.00	--	10.13	8.04	8.04	--	--	-0.88	30.81	8	8	Si	12

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kN*m	m ²	cmq	cm	cm	MPa	mm	mm			
0.00	10.13	0.03	8.04	20.11	21.87	30.84	0.019	0.019	7 (Fr)	Si	16
0.00	10.07	0.03	8.04	20.11	21.87	30.65	0.019	0.019	8 (Qp)	Si	10
60.00	3.46	0.03	8.04	20.11	21.87	10.52	0.007	0.007	8 (Qp)	Si	30
60.00	3.49	0.03	8.04	20.11	21.87	10.62	0.007	0.007	7 (Fr)	Si	45
300.00	-6.05	0.03	8.04	20.11	21.87	18.41	0.012	0.012	8 (Qp)	Si	17
300.00	-6.07	0.03	8.04	20.11	21.87	18.49	0.012	0.012	7 (Fr)	Si	26
540.00	3.55	0.03	8.04	20.11	21.87	10.79	0.007	0.007	8 (Qp)	Si	30
540.00	3.58	0.03	8.04	20.11	21.87	10.90	0.007	0.007	7 (Fr)	Si	44
600.00	10.13	0.03	8.04	20.11	21.87	30.81	0.019	0.019	8 (Qp)	Si	10
600.00	10.19	0.03	8.04	20.11	21.87	31.00	0.019	0.019	7 (Fr)	Si	15

Trave di fondazione: 9001 [1,4], Pilastrate [1,4] Sez. T: Ba=100.00 cm Ha=40.00 cm Bs=30.00cm Hs=60.00 cm L=600.00 cm Ln=550.00 cm Terreno=Terreno1 Criterio: CLS_TraviFondazione_Rett_ND

Combinazione Rara: σ_{ca} [MPa]=22.41 σ_{fa} [MPa]=360.00

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	24.65	--	6.16	12.32	-0.59	22.96	--	--	6	6	Si	16
55.00	--	6.33	6.16	12.32	--	--	-0.10	11.23	6	6	Si	32
275.00	--	66.05	6.16	12.32	--	--	-1.06	117.28	6	6	Si	3.1
495.00	--	28.33	6.16	12.32	--	--	-0.46	50.30	6	6	Si	7.2
550.00	--	2.17	6.16	12.32	--	--	-0.03	3.86	6	6	Si	93

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kN*m	m ²	cmq	cm	cm	MPa	mm	mm			
0.00	-24.63	0.12	12.32	35.19	32.42	22.93	0.021	0.021	7 (Fr)	Si	14
0.00	-24.34	0.12	12.32	35.19	32.42	22.66	0.021	0.021	8 (Qp)	Si	9.5
55.00	6.12	0.03	6.16	17.59	23.53	10.86	0.007	0.007	8 (Qp)	Si	27
55.00	6.16	0.03	6.16	17.59	23.53	10.94	0.007	0.007	7 (Fr)	Si	41
275.00	64.83	0.03	6.16	17.59	23.53	115.11	0.077	0.077	8 (Qp)	Si	2.6
275.00	65.52	0.03	6.16	17.59	23.53	116.32	0.078	0.078	7 (Fr)	Si	3.8
495.00	27.73	0.03	6.16	17.59	23.53	49.24	0.033	0.033	8 (Qp)	Si	6.0
495.00	28.01	0.03	6.16	17.59	23.53	49.74	0.033	0.033	7 (Fr)	Si	9.0
550.00	2.02	0.03	6.16	17.59	23.53	3.58	0.002	0.002	8 (Qp)	Si	83
550.00	2.01	0.03	6.16	17.59	23.53	3.58	0.002	0.002	7 (Fr)	Si	>100

Trave di fondazione: 9002 [4,5], Pilastrate [4,5] Sez. T: Ba=100.00 cm Ha=40.00 cm Bs=30.00cm Hs=60.00 cm L=600.00 cm Ln=600.00 cm Terreno=Terreno1 Criterio: CLS_TraviFondazione_Rett_ND

Combinazione Rara: σ_{ca} [MPa]=22.41 σ_{fa} [MPa]=360.00

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	9.81	--	6.16	12.32	-0.24	9.14	--	--	6	6	Si	39
60.00	--	19.78	6.16	12.32	--	--	-0.32	35.11	6	6	Si	10
300.00	--	54.40	6.16	12.32	--	--	-0.87	96.58	6	6	Si	3.7
540.00	30.80	--	6.16	12.32	-0.74	28.68	--	--	6	6	Si	13
600.00	71.21	--	6.16	12.32	-1.71	66.31	--	--	6	6	Si	5.4

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 97 di 103

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kN*m	m ²	cmq	cm	cm	MPa	mm	mm			
0.00	-10.40	0.12	12.32	35.19	32.42	9.69	0.009	0.009	7 (Fr)	Si	33
0.00	-10.35	0.12	12.32	35.19	32.42	9.64	0.009	0.009	8 (Qp)	Si	22
60.00	18.84	0.03	6.16	17.59	23.53	33.45	0.022	0.022	8 (Qp)	Si	8.9
60.00	19.09	0.03	6.16	17.59	23.53	33.90	0.023	0.023	7 (Fr)	Si	13
300.00	53.98	0.03	6.16	17.59	23.53	95.84	0.064	0.064	8 (Qp)	Si	3.1
300.00	54.52	0.03	6.16	17.59	23.53	96.79	0.065	0.065	7 (Fr)	Si	4.6
540.00	-25.68	0.12	12.32	35.19	32.42	23.91	0.022	0.022	8 (Qp)	Si	9.0
540.00	-26.37	0.12	12.32	35.19	32.42	24.56	0.023	0.023	7 (Fr)	Si	13
600.00	-63.65	0.12	12.32	35.19	32.42	59.27	0.055	0.055	8 (Qp)	Si	3.6
600.00	-64.92	0.12	12.32	35.19	32.42	60.45	0.056	0.056	7 (Fr)	Si	5.4

Trave di fondazione: 9002 [5,6], Pilastrate [5,6] Sez. T: Ba=100.00 cm Ha=40.00 cm Bs=30.00cm Hs=60.00 cm L=600.00 cm Ln=600.00 cm Terreno=Terrenol Criterio: CLS_TraviFondazione_Rett_ND

Combinazione Rara: σ_{ca} [MPa]=22.41 σ_{fa} [MPa]=360.00

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	71.21	--	12.32	12.32	-1.54	65.58	--	--	6	6	Si	5.5
60.00	30.80	--	12.32	12.32	-0.67	28.36	--	--	6	6	Si	13
300.00	--	54.40	12.32	12.32	--	--	-0.65	48.97	6	6	Si	7.4
540.00	--	19.78	12.32	12.32	--	--	-0.24	17.80	6	6	Si	20
600.00	9.81	--	12.32	12.32	-0.21	9.04	--	--	6	6	Si	40

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kN*m	m ²	cmq	cm	cm	MPa	mm	mm			
0.00	-64.92	0.12	12.32	35.19	32.42	59.79	0.055	0.055	7 (Fr)	Si	5.4
0.00	-63.65	0.12	12.32	35.19	32.42	58.62	0.054	0.054	8 (Qp)	Si	3.7
60.00	-25.68	0.12	12.32	35.19	32.42	23.65	0.022	0.022	8 (Qp)	Si	9.1
60.00	-26.37	0.12	12.32	35.19	32.42	24.29	0.023	0.023	7 (Fr)	Si	13
300.00	53.98	0.03	12.32	35.19	16.87	48.59	0.023	0.023	8 (Qp)	Si	8.5
300.00	54.52	0.03	12.32	35.19	16.87	49.07	0.024	0.024	7 (Fr)	Si	13
540.00	18.84	0.03	12.32	35.19	16.87	16.96	0.008	0.008	8 (Qp)	Si	24
540.00	19.09	0.03	12.32	35.19	16.87	17.19	0.008	0.008	7 (Fr)	Si	36
600.00	-10.35	0.12	12.32	35.19	32.42	9.53	0.009	0.009	8 (Qp)	Si	23
600.00	-10.40	0.12	12.32	35.19	32.42	9.58	0.009	0.009	7 (Fr)	Si	34

Trave di fondazione: 9003 [5,2], Pilastrate [5,2] Sez. T: Ba=100.00 cm Ha=40.00 cm Bs=30.00cm Hs=60.00 cm L=600.00 cm Ln=570.00 cm Terreno=Terrenol Criterio: CLS_TraviFondazione_Rett_ND

Combinazione Rara: σ_{ca} [MPa]=22.41 σ_{fa} [MPa]=360.00

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	0.31	--	6.16	12.32	-0.01	0.29	--	--	6	6	Si	>100
57.00	--	36.00	6.16	12.32	--	--	-0.58	63.91	6	6	Si	5.6
285.00	--	91.55	6.16	12.32	--	--	-1.47	162.54	6	6	Si	2.2
513.00	--	15.82	6.16	12.32	--	--	-0.25	28.09	6	6	Si	13
570.00	25.41	--	6.16	12.32	-0.61	23.66	--	--	6	6	Si	15

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kN*m	m ²	cmq	cm	cm	MPa	mm	mm			
0.00	-0.34	0.12	12.32	35.19	32.42	0.31	0.000	0.000	7 (Fr)	Si	>100
0.00	-0.31	0.12	12.32	35.19	32.42	0.29	0.000	0.000	8 (Qp)	Si	>100
57.00	34.52	0.03	6.16	17.59	23.53	61.28	0.041	0.041	8 (Qp)	Si	4.9
57.00	34.85	0.03	6.16	17.59	23.53	61.87	0.042	0.042	7 (Fr)	Si	7.2
285.00	87.78	0.03	6.16	17.59	23.53	155.86	0.105	0.105	8 (Qp)	Si	1.9
285.00	88.65	0.03	6.16	17.59	23.53	157.40	0.106	0.106	7 (Fr)	Si	2.8
513.00	15.07	0.03	6.16	17.59	23.53	26.76	0.018	0.018	8 (Qp)	Si	11
513.00	15.20	0.03	6.16	17.59	23.53	26.99	0.018	0.018	7 (Fr)	Si	17
570.00	-24.50	0.12	12.32	35.19	32.42	22.82	0.021	0.021	8 (Qp)	Si	9.5
570.00	-24.77	0.12	12.32	35.19	32.42	23.07	0.021	0.021	7 (Fr)	Si	14

Trave di fondazione: 9004 [2,1], Pilastrate [2,1] Sez. T: Ba=100.00 cm Ha=40.00 cm Bs=30.00cm Hs=60.00 cm L=600.00 cm Ln=600.00 cm Terreno=Terrenol Criterio: CLS_TraviFondazione_Rett_ND

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 98 di 103

Combinazione Rara: σ_{ca} [MPa]=22.41 σ_{fa} [MPa]=360.00

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	70.71	--	6.16	12.32	-1.70	65.84	--	--	6	6	Si	5.5
60.00	32.92	--	6.16	12.32	-0.79	30.66	--	--	6	6	Si	12
300.00	--	47.69	6.16	12.32	--	--	-0.77	84.67	6	6	Si	4.3
540.00	--	19.78	6.16	12.32	--	--	-0.32	35.13	6	6	Si	10
600.00	5.75	--	6.16	12.32	-0.14	5.35	--	--	6	6	Si	67

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kN*m	m ²	cmq	cm	cm	MPa	mm	mm			
0.00	-64.57	0.12	12.32	35.19	32.42	60.13	0.056	0.056	7 (Fr)	Si	5.4
0.00	-63.30	0.12	12.32	35.19	32.42	58.95	0.055	0.055	8 (Qp)	Si	3.7
60.00	-27.87	0.12	12.32	35.19	32.42	25.95	0.024	0.024	8 (Qp)	Si	8.3
60.00	-28.59	0.12	12.32	35.19	32.42	26.63	0.025	0.025	7 (Fr)	Si	12
300.00	47.39	0.03	6.16	17.59	23.53	84.13	0.057	0.057	8 (Qp)	Si	3.5
300.00	47.85	0.03	6.16	17.59	23.53	84.96	0.057	0.057	7 (Fr)	Si	5.3
540.00	18.87	0.03	6.16	17.59	23.53	33.50	0.023	0.023	8 (Qp)	Si	8.9
540.00	19.12	0.03	6.16	17.59	23.53	33.95	0.023	0.023	7 (Fr)	Si	13
600.00	-6.34	0.12	12.32	35.19	32.42	5.91	0.005	0.005	8 (Qp)	Si	37
600.00	-6.35	0.12	12.32	35.19	32.42	5.91	0.005	0.005	7 (Fr)	Si	55

Trave di fondazione: 9004 [3,2], Pilastrate [3,2] Sez. T: Ba=100.00 cm Ha=40.00 cm Bs=30.00cm Hs=60.00 cm L=600.00 cm Ln=600.00 cm Terreno=Terrenol Criterio: CLS_TraviFondazione_Rett_ND

Combinazione Rara: σ_{ca} [MPa]=22.41 σ_{fa} [MPa]=360.00

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	5.75	--	12.32	12.32	-0.12	5.29	--	--	6	6	Si	68
60.00	--	19.78	12.32	12.32	--	--	-0.24	17.81	6	6	Si	20
300.00	--	47.69	12.32	12.32	--	--	-0.57	42.93	6	6	Si	8.4
540.00	32.92	--	12.32	12.32	-0.71	30.32	--	--	6	6	Si	12
600.00	70.71	--	12.32	12.32	-1.53	65.12	--	--	6	6	Si	5.5

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kN*m	m ²	cmq	cm	cm	MPa	mm	mm			
0.00	-6.35	0.12	12.32	35.19	32.42	5.85	0.005	0.005	7 (Fr)	Si	55
0.00	-6.34	0.12	12.32	35.19	32.42	5.84	0.005	0.005	8 (Qp)	Si	37
60.00	18.87	0.03	12.32	35.19	16.87	16.98	0.008	0.008	8 (Qp)	Si	24
60.00	19.12	0.03	12.32	35.19	16.87	17.21	0.008	0.008	7 (Fr)	Si	36
300.00	47.39	0.03	12.32	35.19	16.87	42.66	0.021	0.021	8 (Qp)	Si	9.7
300.00	47.85	0.03	12.32	35.19	16.87	43.08	0.021	0.021	7 (Fr)	Si	14
540.00	-27.87	0.12	12.32	35.19	32.42	25.67	0.024	0.024	8 (Qp)	Si	8.4
540.00	-28.59	0.12	12.32	35.19	32.42	26.33	0.024	0.024	7 (Fr)	Si	12
600.00	-63.30	0.12	12.32	35.19	32.42	58.30	0.054	0.054	8 (Qp)	Si	3.7
600.00	-64.57	0.12	12.32	35.19	32.42	59.47	0.055	0.055	7 (Fr)	Si	5.4

Trave di fondazione: 9005 [6,3], Pilastrate [6,3] Sez. T: Ba=100.00 cm Ha=40.00 cm Bs=30.00cm Hs=60.00 cm L=600.00 cm Ln=550.00 cm Terreno=Terrenol Criterio: CLS_TraviFondazione_Rett_ND

Combinazione Rara: σ_{ca} [MPa]=22.41 σ_{fa} [MPa]=360.00

X	M+	M-	Afsup	Afinf	σ_{c+}	σ_{f+}	σ_{c-}	σ_{f-}	Cb+	Cb-	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	2.17	12.32	12.32	--	--	-0.03	1.96	6	6	Si	>100
55.00	--	28.33	12.32	12.32	--	--	-0.34	25.50	6	6	Si	14
275.00	--	66.05	12.32	12.32	--	--	-0.79	59.46	6	6	Si	6.1
495.00	--	6.33	12.32	12.32	--	--	-0.08	5.69	6	6	Si	63
550.00	24.65	--	12.32	12.32	-0.53	22.70	--	--	6	6	Si	16

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
cm	kN*m	m ²	cmq	cm	cm	MPa	mm	mm			
0.00	2.01	0.03	12.32	35.19	16.87	1.81	0.001	0.001	7 (Fr)	Si	>100
0.00	2.02	0.03	12.32	35.19	16.87	1.81	0.001	0.001	8 (Qp)	Si	>100
55.00	27.73	0.03	12.32	35.19	16.87	24.97	0.012	0.012	8 (Qp)	Si	17
55.00	28.01	0.03	12.32	35.19	16.87	25.22	0.012	0.012	7 (Fr)	Si	25
275.00	64.83	0.03	12.32	35.19	16.87	58.36	0.028	0.028	8 (Qp)	Si	7.1
275.00	65.52	0.03	12.32	35.19	16.87	58.98	0.028	0.028	7 (Fr)	Si	11

X	M	Act	Aft	pAft	$S_{r,max}$	σ_{fmed}	Wd	Wk	Cb	Ver.	Cs
495.00	6.12	0.03	12.32	35.19	16.87	5.51	0.003	0.003	8 (Qp)	Si	75
495.00	6.16	0.03	12.32	35.19	16.87	5.55	0.003	0.003	7 (Fr)	Si	>100
550.00	-24.34	0.12	12.32	35.19	32.42	22.41	0.021	0.021	8 (Qp)	Si	9.6
550.00	-24.63	0.12	12.32	35.19	32.42	22.68	0.021	0.021	7 (Fr)	Si	14

Verifica dei pilastri (Stati limite esercizio)

Scenario di calcolo: **ScenarioNT_ 2018 A2_SLV_SLD_STR_GEO**

Simbologia

Terreno	Nome della stratigrafia per travi Winkler
L [cm]	Lunghezza teorica elemento (distanza tra i nodi)
Ln [cm]	Lunghezza netta elemento (tiene conto dei conci rigidi)
L2,L3 [cm]	Lunghezze libere di inflessione
Sez. R: Sezione Rettangolare	
	By[cm]: Larghezza (asse locale y)
	Bz[cm]: Larghezza (asse locale z)
Sez. T: Sezione a T (rovescia e non)	
	Ba[cm]: Larghezza base inferiore
	Ha[cm]: Altezza inferiore
	Bs[cm]: Larghezza superiore
	Hs[cm]: Altezza superiore
Sez. L: Sezione ad L (rovescia e non)	
	Ba[cm]: Larghezza base inferiore
	Ha[cm]: Altezza inferiore
	Bs[cm]: Larghezza superiore
	Hs[cm]: Altezza superiore
Sez. C: Sezione circolare	
	R[cm]: Raggio
Sez. G: Sezione generica	
	B[cm]: Larghezza
	H[cm]: Altezza
X [cm]	Punto di verifica
σ_{ca} [MPa]	Tensione ammissibile nel cls
σ_{fa} [MPa]	Tensione ammissibile nell'acciaio
σ_{cta} [MPa]	Tensione ammissibile a trazione (quando richiesto dalla verifica)
M- [kN*m]	Momento negativo massimo di calcolo
M+ [kN*m]	Momento positivo massimo di calcolo
M [kN*m]	Momento di calcolo (travi a flessione, pilastri circolari)
My [kN*m]	Momento calcolo per verifiche a pressoflessione
Mz [kN*m]	Momento calcolo per verifiche a pressoflessione (Sez. L,Pilastri)
N [kN]	Sforzo normale corrispondente ad My (e Mz per Sez. L,Pilastri)
Afsup [cmq]	Area di ferro superiore
Afinf [cmq]	Area di ferro inferiore
Afsin [cmq]	Area di ferro sinistra (Sez. L)
Afdes [cmq]	Area di ferro destra (Sez. L)
σ_{c-} [MPa]	Tensione nel cls compresso per effetto di M-
σ_{cy} [MPa]	Tensione nel cls compresso per effetto di (N,My) in caso di pressoflessione retta
σ_{cz} [MPa]	Tensione nel cls compresso per effetto di (N,Mz) in caso di pressoflessione retta
σ_{c+} [MPa]	Tensione nel cls compresso per effetto di M+
σ_{ct-} [MPa]	Tensione nel cls teso per effetto di M-
σ_{ct+} [MPa]	Tensione nel cls teso per effetto di M+
σ_{f-} [MPa]	Tensione nell'acciaio per effetto di M-
σ_{f+} [MPa]	Tensione nell'acciaio per effetto di M+
σ_{fy} [MPa]	Tensione nel acciaio per effetto di (N,My) in caso di pressoflessione retta
σ_{fz} [MPa]	Tensione nel acciaio per effetto di (N,Mz) in caso di pressoflessione retta
Cb-	Combinazione di carico generatore di M-
Cb+	Combinazione di carico generatore di M+
σ_c [MPa]	Tensione nel cls per effetto di N My
σ_f [MPa]	Tensione nell'acciaio per effetto di N My
Cb	Combinazione di carico generatore di N My
Act [m^2]	Area di calcestruzzo teso
Aft [cmq]	Area di acciaio teso
pAft [cm]	Perimetro area di acciaio teso
$S_{r,max}$ [cm]	Distanza massima delle fessure
σ_{fmed} [MPa]	Tensione media dell'acciaio
Wd [mm]	Apertura delle fessure
Wk [mm]	Apertura caratteristica delle fessure
Wamm_Freq [mm]	Apertura ammissibile delle fessure per combinazione Frequente
Wamm_Qp [mm]	Apertura ammissibile delle fessure per combinazione Quasi Permanente
Wamm_Rara [mm]	Apertura ammissibile delle fessure per combinazione Rara
Cs	Coefficiente di sicurezza definito come minimo di σ_{amm}/σ tra acciaio e calcestruzzo oppure Wamm/Wk

Pilastro: 1 [1,101] Sez. R: By=30.00 cm Bz=50.00 cm L=400.00 cm Ln=400.00 cm L2=400.00 cm L3=400.00 cm Criterio: CLS_Pilastri_ND

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 1.54
400.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 1.54

Verifica snellezza: fcd=21.16 [MPa] - **Verificato**

Cb	N	fcd*Ac	v	λmax	λlim
	kN	kN			
6	112.09	3174.75	0.035	46.188	133.050

Combinazione Rara: σca[MPa]=22.41 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-112.09	-6.26	-1.19	-1.18	-3.44	6	Si	19
400.00	-97.09	0.43	7.17	-1.41	1.10	6	Si	16

Combinazione QP: σca[MPa]=16.81 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-110.37	-6.09	-0.54	-1.08	-4.17	8	Si	15
400.00	-95.37	0.34	6.08	-1.24	-0.84	8	Si	14

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	N	My	Mz	Act	Aft	pAft	S _{F,max}	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m ²	cmq	cm	cm	MPa	mm	mm			
0.00	-111.55	-6.18	-0.60	0.00	0.00	0.00	0.00	0.00	0.000	0.000	7 (Fr)	Si	>100
0.00	-110.37	-6.09	-0.54	0.00	0.00	0.00	0.00	0.00	0.000	0.000	8 (Qp)	Si	>100
400.00	-95.37	0.34	6.08	0.00	0.00	0.00	0.00	0.00	0.000	0.000	8 (Qp)	Si	>100
400.00	-96.55	0.39	6.23	0.00	0.00	0.00	0.00	0.00	0.000	0.000	7 (Fr)	Si	>100

Pilastro: 2 [2,102] Sez. R: By=50.00 cm Bz=30.00 cm L=400.00 cm Ln=400.00 cm L2=400.00 cm L3=400.00 cm Criterio: CLS_Pilastrini_ND

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 3.14	Afy = 1.54	Afz = 0.00
400.00	AfSpigolo = 3.14	Afy = 1.54	Afz = 0.00

Verifica snellezza: fcd=21.16 [MPa] - **Verificato**

Cb	N	fcd*Ac	v	λmax	λlim
	kN	kN			
6	219.31	3174.75	0.069	46.188	95.118

Combinazione Rara: σca[MPa]=22.41 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-219.31	-6.49	0.00	-1.97	-11.62	6	Si	11
400.00	-204.31	6.11	-0.00	-1.84	-10.75	6	Si	12

Combinazione QP: σca[MPa]=16.81 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-207.48	-6.52	0.00	-1.91	-10.56	8	Si	8.8
400.00	-192.48	6.44	-0.00	-1.81	-9.36	8	Si	9.3

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	N	My	Mz	Act	Aft	pAft	S _{F,max}	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m ²	cmq	cm	cm	MPa	mm	mm			
0.00	-210.25	-6.61	0.00	0.00	0.00	0.00	0.00	0.00	0.000	0.000	7 (Fr)	Si	>100
0.00	-207.48	-6.52	0.00	0.00	0.00	0.00	0.00	0.00	0.000	0.000	8 (Qp)	Si	>100
400.00	-192.48	6.44	-0.00	0.00	0.00	0.00	0.00	0.00	0.000	0.000	8 (Qp)	Si	>100
400.00	-195.25	6.56	-0.00	0.00	0.00	0.00	0.00	0.00	0.000	0.000	7 (Fr)	Si	>100

Pilastro: 3 [3,103] Sez. R: By=30.00 cm Bz=50.00 cm L=400.00 cm Ln=400.00 cm L2=400.00 cm L3=400.00 cm Criterio: CLS_Pilastrini_ND

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 101 di 103

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 1.54
400.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 1.54

Verifica snellezza: fcd=21.16 [MPa] - **Verificato**

Cb	N	fcd*Ac	v	λmax	λlim
	kN	kN			
6	112.09	3174.75	0.035	46.188	133.050

Combinazione Rara: σca[MPa]=22.41 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-112.09	-6.26	1.19	-1.18	-3.44	6	Si	19
400.00	-97.09	0.43	-7.17	-1.41	1.10	6	Si	16

Combinazione QP: σca[MPa]=16.81 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-110.37	-6.09	0.54	-1.08	-4.17	8	Si	15
400.00	-95.37	0.34	-6.08	-1.24	-0.84	8	Si	14

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	N	My	Mz	Act	Aft	pAft	S _{r,max}	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-111.55	-6.18	0.60	0.00	0.00	0.00	0.00	0.00	0.000	0.000	7 (Fr)	Si	>100
0.00	-110.37	-6.09	0.54	0.00	0.00	0.00	0.00	0.00	0.000	0.000	8 (Qp)	Si	>100
400.00	-95.37	0.34	-6.08	0.00	0.00	0.00	0.00	0.00	0.000	0.000	8 (Qp)	Si	>100
400.00	-96.55	0.39	-6.23	0.00	0.00	0.00	0.00	0.00	0.000	0.000	7 (Fr)	Si	>100

Pilastro: 4 [4,104] Sez. R: By=30.00 cm Bz=50.00 cm L=400.00 cm Ln=400.00 cm L2=400.00 cm L3=400.00 cm Criterio: CLS_Pilastri_ND

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 1.54
400.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 1.54

Verifica snellezza: fcd=21.16 [MPa] - **Verificato**

Cb	N	fcd*Ac	v	λmax	λlim
	kN	kN			
6	111.48	3174.75	0.035	46.188	133.411

Combinazione Rara: σca[MPa]=22.41 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-111.48	6.60	-0.45	-1.11	-3.96	6	Si	20
400.00	-96.48	-0.44	6.59	-1.32	0.01	6	Si	17

Combinazione QP: σca[MPa]=16.81 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-109.76	6.44	0.20	-1.07	-4.23	8	Si	16
400.00	-94.76	-0.35	5.50	-1.17	-1.63	8	Si	14

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	N	My	Mz	Act	Aft	pAft	S _{r,max}	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-110.94	6.53	0.14	0.00	0.00	0.00	0.00	0.00	0.000	0.000	7 (Fr)	Si	>100
0.00	-109.76	6.44	0.20	0.00	0.00	0.00	0.00	0.00	0.000	0.000	8 (Qp)	Si	>100
400.00	-94.76	-0.35	5.50	0.00	0.00	0.00	0.00	0.00	0.000	0.000	8 (Qp)	Si	>100
400.00	-95.94	-0.40	5.64	0.00	0.00	0.00	0.00	0.00	0.000	0.000	7 (Fr)	Si	>100

Pilastro: 5 [5,105] Sez. R: By=50.00 cm Bz=30.00 cm L=400.00 cm Ln=400.00 cm L2=400.00 cm L3=400.00 cm Criterio: CLS_Pilastri_ND

Zona	Armature		
cm	cmq	cmq	cmq

**POTENZIAMENTO DELL'IMPIANTO DI DEPURAZIONE E
DEL RECAPITO FINALE DI SQUINZANO (LE)
PROGETTO DEFINITIVO
Tabulati di calcolo strutturale-Edificio Alloggio soffianti**

R.37.2

Maggio 2021

Pagina 102 di 103

Zona	Armature		
0.00	AfSpigolo = 3.14	Afy = 1.54	Afz = 0.00
400.00	AfSpigolo = 3.14	Afy = 1.54	Afz = 0.00

Verifica snellezza: fcd=21.16 [MPa] - **Verificato**

Cb	N	fcd*Ac	v	λmax	λlim
	kN	kN			
6	220.56	3174.75	0.069	46.188	94.848

Combinazione Rara: σca[MPa]=22.41 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-220.56	6.02	0.00	-1.93	-12.26	6	Si	12
400.00	-205.56	-5.88	-0.00	-1.82	-11.13	6	Si	12

Combinazione QP: σca[MPa]=16.81 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-208.72	6.04	0.00	-1.86	-11.21	8	Si	9.0
400.00	-193.72	-6.20	-0.00	-1.79	-9.73	8	Si	9.4

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	N	My	Mz	Act	Aft	pAft	Sr,max	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-211.51	6.13	0.00	0.00	0.00	0.00	0.00	0.00	0.000	0.000	7 (Fr)	Si	>100
0.00	-208.72	6.04	0.00	0.00	0.00	0.00	0.00	0.00	0.000	0.000	8 (Qp)	Si	>100
400.00	-193.72	-6.20	-0.00	0.00	0.00	0.00	0.00	0.00	0.000	0.000	8 (Qp)	Si	>100
400.00	-196.51	-6.32	-0.00	0.00	0.00	0.00	0.00	0.00	0.000	0.000	7 (Fr)	Si	>100

Pilastro: 6 [6,106] Sez. R: By=30.00 cm Bz=50.00 cm L=400.00 cm Ln=400.00 cm L2=400.00 cm L3=400.00 cm Criterio: CLS_Pilastri_ND

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 1.54
400.00	AfSpigolo = 3.14	Afy = 0.00	Afz = 1.54

Verifica snellezza: fcd=21.16 [MPa] - **Verificato**

Cb	N	fcd*Ac	v	λmax	λlim
	kN	kN			
6	111.48	3174.75	0.035	46.188	133.411

Combinazione Rara: σca[MPa]=22.41 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-111.48	6.60	0.45	-1.11	-3.96	6	Si	20
400.00	-96.48	-0.44	-6.59	-1.32	0.01	6	Si	17

Combinazione QP: σca[MPa]=16.81 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-109.76	6.44	-0.20	-1.07	-4.23	8	Si	16
400.00	-94.76	-0.35	-5.50	-1.17	-1.63	8	Si	14

Verifica aperture fessure:Wamm Freq[mm]=0.300 Wamm Qp[mm]=0.200

X	N	My	Mz	Act	Aft	pAft	Sr,max	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-110.94	6.53	-0.14	0.00	0.00	0.00	0.00	0.00	0.000	0.000	7 (Fr)	Si	>100
0.00	-109.76	6.44	-0.20	0.00	0.00	0.00	0.00	0.00	0.000	0.000	8 (Qp)	Si	>100
400.00	-94.76	-0.35	-5.50	0.00	0.00	0.00	0.00	0.00	0.000	0.000	8 (Qp)	Si	>100
400.00	-95.94	-0.40	-5.64	0.00	0.00	0.00	0.00	0.00	0.000	0.000	7 (Fr)	Si	>100

PROGETTO DEL SOLAIO MONOTRAVE A TRAVETTI IN CALCESTRUZZO PRECOMPRESSO H = 20+5 cm, interasse 50 cm

I solai saranno del tipo latero cementizio con travetti in calcestruzzo precompresso della larghezza di 12 cm. L'altezza sarà pari a 25 cm di cui 5 cm di soletta collaborante. L'interasse dei travetti sarà pari a 50 cm.

Luce netta massima 5,24 m con luce di calcolo 6,00 m

ANALISI DEI CARICHI SOLAIO:

Peso proprio	= 310 daN/m ²
Sovraccarichi permanenti	= 250 daN/m ²
Sovraccarico di esercizio	= 50 daN/m ²
Neve	= 60 daN/m ²

Si utilizzeranno i valori relativi allo stato limite di esercizio per le verifiche relative ai travetti ed alle armature aggiuntive per i momenti negativi, mentre si farà ricorso agli stati limite ultimi per le verifiche relative alle fasce piene e semipiene e per il calcolo dell'armatura inferiore sugli appoggi.

SLE: COMBINAZIONE RARA

Il carico totale massimo in combinazione rara è pari a $(310 \times 1 + 250 \times 1 + 110 \times 1)$ daN/m² = 670 daN/m².

I vincoli vengono considerati come semi appoggi, per cui il momento flettente positivo di servizio sollecitante una fascia di solaio larga 1,00 m è il seguente:

$$M_{dmax+} = q \times l^2 / 10 = 670 \times 6,00^2 / 10 = 2412 \text{ daNm}$$

Si utilizzerà un solaio con travetti in c.a.p. avente momento di servizio positivo minimo in combinazione rara maggiore di 2500 daNm/m.

Il momento negativo è pari a $M_{dmax-} = q \times l^2 / 10 = 670 \times 6,00^2 / 10 = 2412 \text{ daNm}$

$$M_{dmax-} / \text{travetto} = 2412 \text{ daNm} / 2 = 1210 \text{ daNm}$$

$$\text{Armatura a momento negativo: } A_a = M_{dmax-} / (0,88 \times s_f \times h) = 1210 / (0,88 \times 26 \times 21) = 2,51 \text{ cm}^2$$

Si utilizzano 2Φ16 a travetto = 4,02 cm²

SLU

Il carico totale è:

$$(310 \times 1,30 + 250 \times 1,50 + 110 \times 1,50) \text{ daN/m}^2 = 950 \text{ daN/m}^2$$

Verifica a flessione

I vincoli vengono considerati come semi appoggi, per cui il momento flettente positivo di servizio sollecitante una fascia di solaio larga 1,00 m è il seguente:

$$M_{dmax+} = q \times l^2 / 10 = 950 \times 6,00^2 / 10 = 3420 \text{ daNm}$$

Si utilizzerà un solaio con travetti in c.a.p. avente momento allo SLU positivo minimo pari a 3500 daNm.

Il momento negativo è pari a $M_{dmax-} = q \times l^2 / 10 = 950 \times 6,00^2 / 10 = 3420 \text{ daNm}$

$$M_{dmax-} / \text{travetto} = 3420 \text{ daNm} / 2 = 1710 \text{ daNm}$$

$$\text{Armatura a momento negativo: } A_a = M_{dmax-} / (0,88 \times s_f \times h) = 1710 / (0,88 \times 21 \times 39) = 2,37 \text{ cm}^2$$

Si utilizzano 2Φ16 a travetto = 4,02 cm²

Verifica a taglio

Il taglio massimo sollecitante una fascia di solaio della larghezza di 1 m è pari a

$$T_{max} = 950 \text{ daN/m} \times 6,00 \text{ m} / 2 = 2850 \text{ daN}$$

Per cui:

$$T_{max} \text{ travetto} = 2850 / 2 = 1425 \text{ daN}$$

Determinazione armatura inferiore appoggi

$$T_{max} \text{ travetto} / f_{yd} = 14250 \text{ N} / 391,3 \text{ N/mm}^2 = 37 \text{ mm}^2 = 0,37 \text{ cm}^2$$

Si adottano 2 Φ 10 a travetto per complessivi 1,60 cm²

L'armatura della soletta collaborante sarà costituita da una rete elettrosaldata Φ 6 passo 15x15 cm corrispondente ad un'area di armatura pari a 1,88 cm² in entrambe le direzioni (tale area risulta > del 20% dell'area dell'armatura longitudinale)